

## **Appendix 2. Project Description**

### **2.1. Civil Engineering Report**

BASELINE

AtkinsRéalis



# Civil Engineering Planning Report

Bord Gáis Energy

12 May 2025

PEK3-ATR-ZZ-ZZ-RP-CE-300001

# CASHLA PEAKER PLANT

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# 1. Introduction

## 1.1 Site Description

The greenfield site for the proposed Cashla Peaker Plant is approximately 11.54ha and is situated at Pollnagroagh and Rathmorrisy, Athenry. The site is situated approximately 14 kilometres east of Galway City and 2 kilometres west of Athenry. Covering an area of roughly 19.17 hectares, the wider project site lies between the northern and eastern arms of the M6/M18 interchange. Access to the Cashla Peaker Plant site will be provided through a newly proposed access road, measuring 1.15 kilometres in length, which will connect to the L3103. This connection point is located approximately 1 kilometre east of the M17 motorway.

## 1.2 Project Overview

The proposed development involves the construction of a gas-fired peaker plant, referred to as the Cashla Peaker Plant, and associated infrastructure. An overview of the proposed development is set out in Section 2.2. of this report.

## 1.3 Planning Application and Ancillary Infrastructure

The planning application for the open cycle gas turbine peaker power plant will be submitted as a Strategic Infrastructure Development (SID). It is important to note that the SID application covering the plant and access road will be separate from those relating to the cable route and substation.

## 1.4 Grid Connection and Infrastructure

A key feature of the site is the four-bay substation and 8.1km underground cable to Cashla Substation, constructed in accordance with EirGrid's 220kV standards to ensure compliance with national grid requirements. The substation will be supported by newly built access roads to facilitate movement within the site and connect the facility to the wider transport network. An ESB switchgear building will also be established as part of the plant's electrical infrastructure, contributing to the safe and reliable operation of the facility.

### 1.4.1 On-Site Infrastructure and Support Systems

To support the operation of the generator and turbine, the development will include dedicated fuel oil tanks and demineralised water tanks. A water treatment system will be installed to produce demineralised water required for plant operations. The site will also feature a steel stack, standing 30 metres high and 7 metres in diameter, designed for the safe discharge of exhaust gases from the turbine.

### 1.4.2 Ancillary Structures and Site Layout

Additional supporting structures will be constructed throughout the site, including pump houses, kiosks, internal roads, pipe racks and bridges, and an infiltration pond. The generator's support equipment will be housed in containerised units, allowing for straightforward installation and replacement as required.



### 1.4.3 Gas Supply Infrastructure

To the south of the site, a Gas Networks Ireland Above Ground Installation (GNI AGI) will be constructed. This facility will enable extraction of gas from the underground high-pressure transmission line passing through the site, ensuring a reliable fuel supply for the plant.

### 1.4.4 Operational Staffing and Control

The plant is designed for efficient operation, with a maximum of ten personnel required on-site at any one time. Remote control capabilities will be available, and a small security presence will be maintained as part of the operational plan.

### 1.4.5 Site Investigations and Environmental Considerations

Initial desktop studies have identified the site as being within a karst landscape, with early investigations revealing that bedrock is located close to the surface. There are no watercourses, streams, or culverts in the immediate vicinity of the site. Consequently, stormwater runoff will be managed by discharging to groundwater via infiltration in the proposed infiltration pond.

### 1.4.6 Wastewater Management

As the site is not served by a local foul sewer network, all wastewater streams must be collected and stored on-site before being transported off-site for appropriate treatment and disposal. These streams include domestic foul effluent, contaminated fire water runoff, chemicals from machine washdown, and rejection water from the demineralised water processing system.



## 2. Existing Site

### 2.1 Project Location

The greenfield site in Pollnagroagh and Rathmorrissy, Athenry is located approximately 14 kilometres east of Galway City and 2 kilometres west of Athenry. The project site with an area circa. 19.17 hectares (including the access road and cable route), is positioned between the northern and eastern arms of the M6/M18 interchange and stretches to Cashla Sub-Station. Access to the site will be provided via a newly proposed 1.15-kilometer-long access road connecting to the L3103, approximately 1 kilometre east of the M17 motorway. The location of the proposed site is presented in Figure 2-1.



Figure 2-1 - Project Location



**Figure 2-2 - Site area components of the project redline boundary**

The total site area is 19.17 ha. This is comprised of the main site area shown in red, the site access road shown in green, and the proposed HV cable route shown in blue. The proposed HV cable route (pink dashed line) is 8.1km to the site (Red area)

## 2.2 Overview of proposed Development

The following provides a summary description of the project assessed as part of the EIAR. The overall project is subject to two separate planning applications: one for the proposed Cashla Peaker Plant and one for the electricity transmission infrastructure. The project will function as a balancing asset, operating intermittently during periods of low renewable energy generation and high electricity demand. Notwithstanding the dual consenting approach, the developments constitute a single, integrated project, whereby the peaker plant will generate electricity for supply to the national grid. The submission of separate planning applications arises solely from planning legislation requirements, which necessitate distinct applications for Strategic Infrastructure Development.

Each application will seek a 10-year permission and detail on the relevant statutory development description is set out in the planning application form.

The proposed operational life is up to and including the 31<sup>st</sup> of December 2050, which is tied to Ireland's Climate Action Plan 2025.

The project site is approximately 19.17 hectares. This is broken down into the 'Cashla Peaker Plant Site' which is approximately 11.54 hectares and is located within the townlands of Pollnagroagh and Rathmorrissy, Athenry, Co. Galway. The balance, 7.63 hectares, relates to the grid connection and substation and is located across the townlands of Rathmorrissy, Pollnagroagh, Moanbaun, Castlelambert, Knocknacreeva, Caraunduff, Caherbriskaun, Lisheenkyle East, Barrettspark, Cashla, Athenry, Co. Galway. The grid connection route traverses approximately 8.1km including along the L7109, L71093, L7108 and L3103 roads.

The project comprises the following infrastructure:

- a. The construction of an open-cycle gas turbine (OCGT) and generator with ancillary equipment including a 30m high stack and emissions monitoring unit, fuel storage and supply systems, cooling and air systems, compressed air and gas handling skids, a grid step-up transformer within a bund, an auxiliary transformer, a generator circuit breaker and an emergency diesel generator. The construction of ten buildings on-site including one single-storey administration building (approximately 390sqm), one single storey ESB Substation building (approximately 32.5sqm), one single-storey workshop building (approximately 750.5sqm), one single storey water treatment plant building (approximately 104sqm), fuel forwarding and unloading area (approximately 104sqm), one single-storey electrical control building (approximately 243.5sqm), one single storey gas analyser kiosk (approximately 6.25sqm), one single-storey boiler house kiosk (approximately 37sqm), one single-storey ancillary pressure reduction kiosk (approximately 26sqm) and a single-storey electrical and instrumentation kiosk (approximately 19sqm). The installation of five above-ground tanks including two bunded fuel tanks (approximately 11.1m high), one fire and service water tank (approximately 13m high), one demineralised water tank (approximately 15.4m high) and one demineralised waste tank (approximately 5m high).
  
- b. The construction of a Gas Networks Ireland (GNI) above ground pressure regulating installation, known as an Above Ground Installation (AGI). The AGI (named Rathmorrissy AGI) will connect to the mains transmission gas network which exists within the site. The AGI infrastructure will occupy an enclosed area of approximately 2,500 sq.m. It encompasses five single-storey buildings: the gas analyser kiosk (approximately 6.25 sqm), the boiler house kiosk (approximately 37 sqm) including 10 no boiler flues approximately 5.67 m above ground level and emergency generator, two pressure reduction kiosks – main (approximately 72 sqm) including approximately 5.24 m high vents, and ancillary (approximately 21.7 sqm) including approximately 3.72 high vents – and the electrical and instrumentation kiosk (approximately 19 sqm). Ancillary infrastructure will include a gas meter, filters, heat exchangers, and above-ground pipework. The compound will include lighting, 3 no. parking spaces, internal access routes, concrete bases to support the infrastructure, and stone-chipped surfacing. It will be secured by an approximately 2.4 m high fence with an access gate.
  
  

*It is noted that the connection to the existing mains gas network (Mayo–Galway pipeline (BGE/85)) will be undertaken via a new transmission pipeline (named GNI146). The GNI146 gas pipeline is subject to Section 39A Consent under the Gas Act 1976, as amended.*
  
- c. Ancillary works including the provision of a new gated vehicular entrance off the L3103, the construction of an access road from the proposed Cashla Peaker Plant Site entrance to the new entrance off the L3103, the demolition of one farm outbuilding (in ruin), construction of internal access roads, hardstanding, security fencing (2.4m high), CCTV and gates, provision of a wastewater treatment system and associated underground wastewater storage tanks, drainage (foul and storm), soakaway retention pond, propane tank, construction of underground firewater retention tanks, provision of parking (12 no. spaces including mobility and EV Parking) and laydown area, 20 no. cycle parking spaces, landscaping and all ancillary on-site development works.
  
- d. The electricity transmission infrastructure comprises the construction of an ESB substation compound within the Cashla Peaker Plant site. The infrastructure will include a 4-bay 220 kV substation incorporating a single-storey Air-Insulated Switchgear (AIS) substation building (approximately 388sqm) and access road; a 36m high telecommunications mast; a shunt reactor, ancillary works including lighting, security fencing (2.4m high), internal tracks, and 4 no. carparking spaces. It also consists of the construction of approximately 8.1 kilometres of an underground grid connection route and laying of cable from the proposed ESB Substation in the Cashla Peaker Plant Site to the Cashla 220kV Substation. The construction methodology includes three horizontal directional drilling (HDD) operations beneath the M6 and M17 motorways to minimise surface disruption.

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The Cashla Peaker Plant involves an activity that will require an Industrial Emission Licence from the Environmental Protection Agency (EPA). This ensures that the project meets all necessary environmental standards related to emissions and other factors impacting the surrounding area. This does not apply to the electricity transmission infrastructure.

Additionally, the Cashla Peaker Plant includes the establishment of a facility where safety measures under the Major Accident Directive (Seveso) will apply. These regulations are designed to prevent and limit the consequences of potential industrial accidents, ensuring the project is both safe and compliant with industry best practices. This does not apply to the electricity transmission infrastructure.



## 2.3 Wayleaves

A desktop search of land direct revealed no existing registered wayleaves in the proposed site. Refer to Figure 2-3.

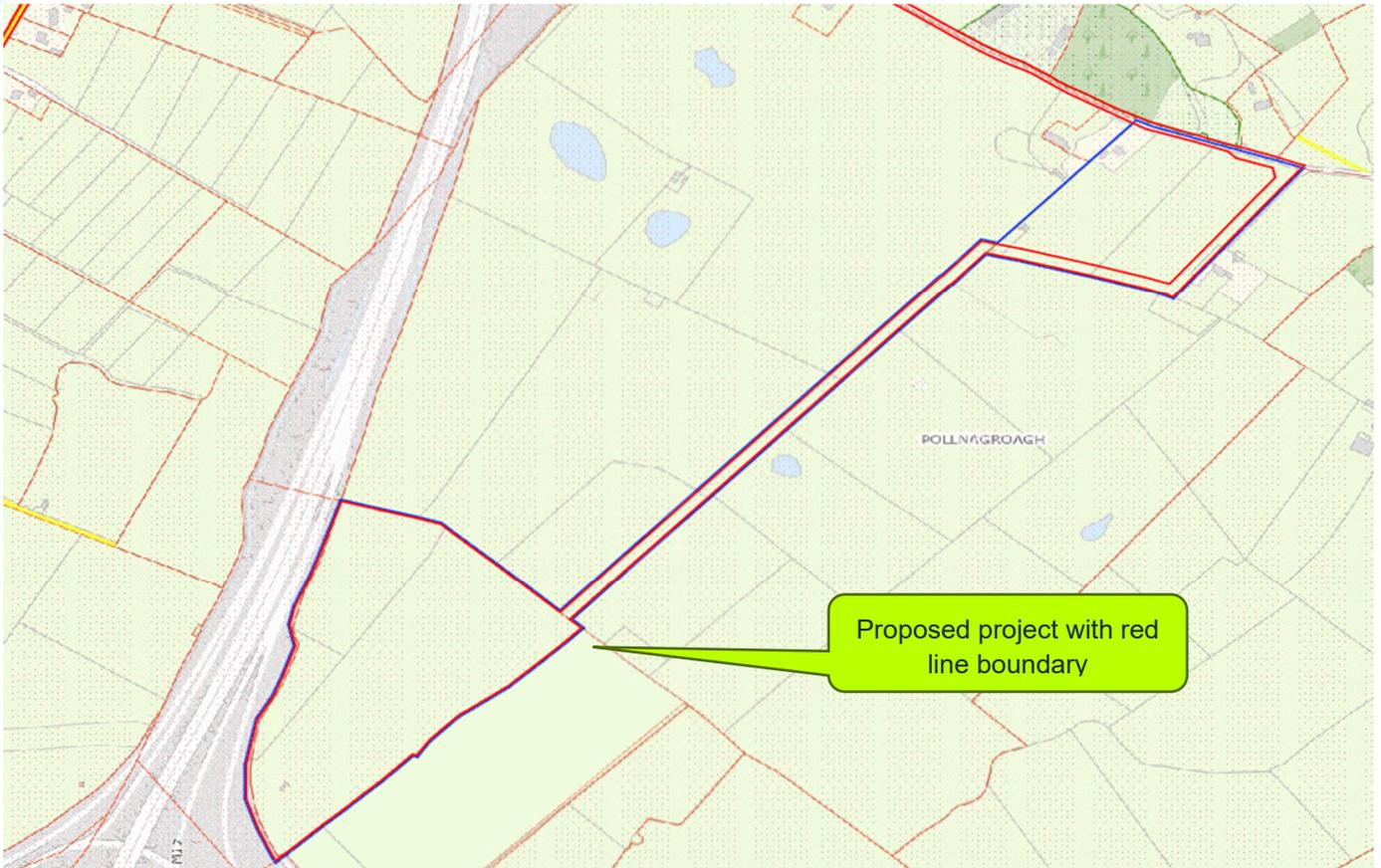


Figure 2-3 - Screenshot from Land Direct showing existing registered wayleaves.

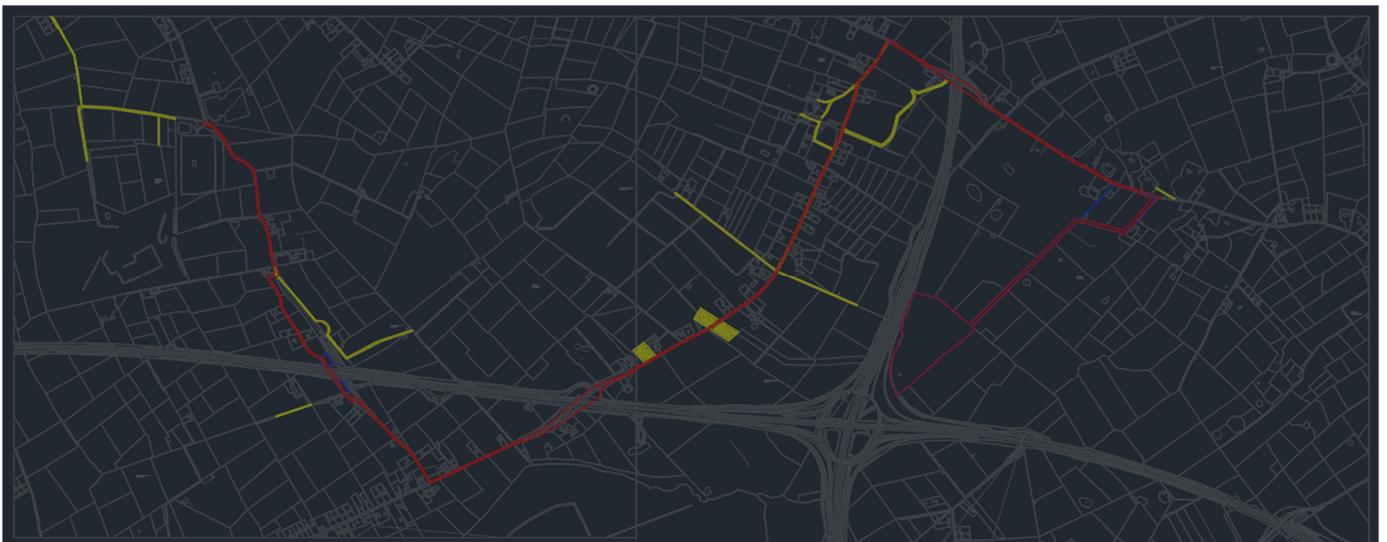


Figure 2-4 - Screenshot of all Land Direct wayleaves along proposed HV Cable Route

## 2.4 Topography

The topography of the site is undulating with a general low point of around 51.8 to the northeast of the site. The site rises as it heads south with an isolated high point to the southwest of 58.5 and general levels to the south of the site of around 57.0m AoD.

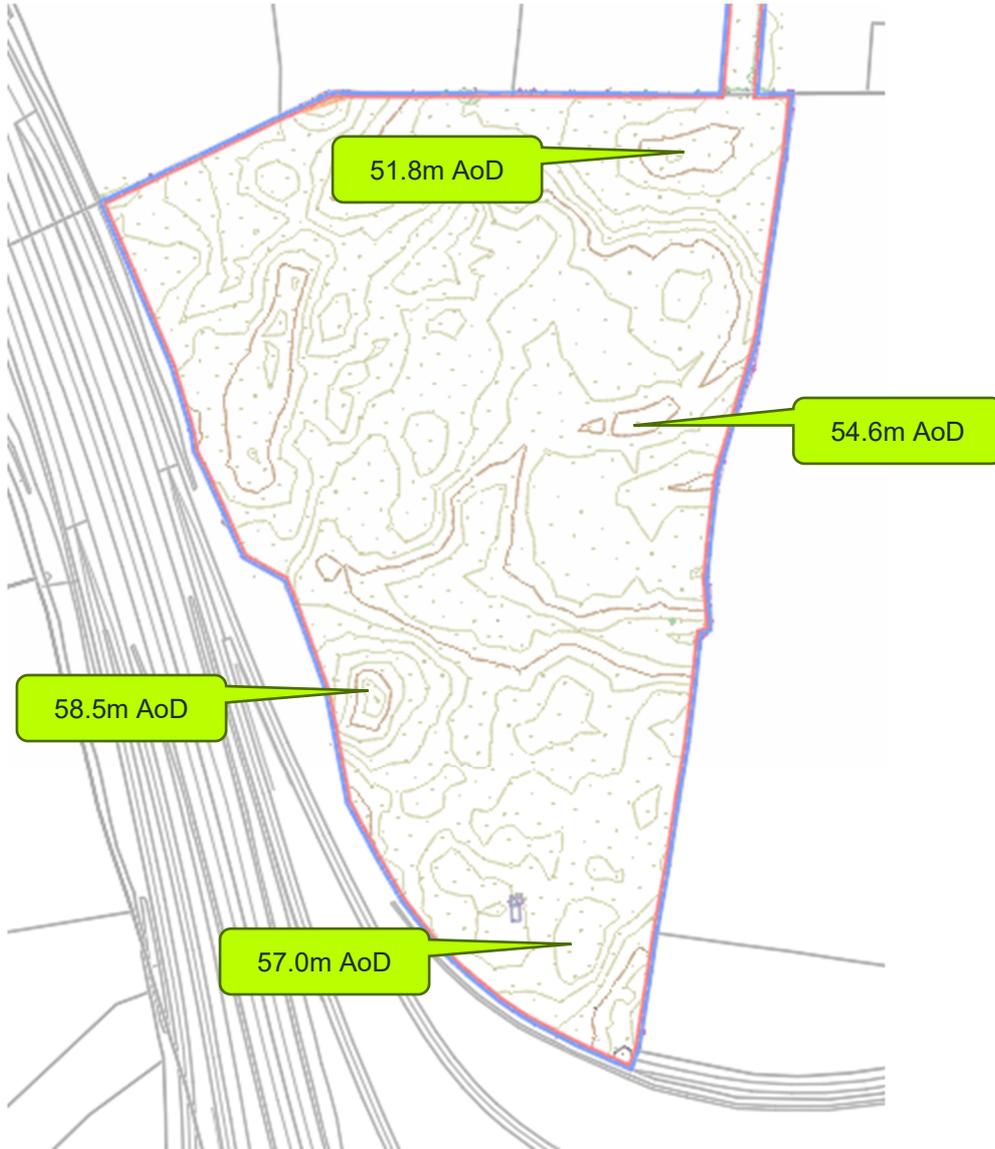


Figure 2-5 - Topographic survey of main site area

## 3. Exiting local infrastructure

A review of local infrastructure was undertaken through a desktop study. Record maps were obtained from the local authority, Uisce Éireann, ESB, telecommunications providers, and Bord Gáis Energy, and are included in Appendix A Utility Record Maps. Additional requests were made to Virgin Media and eNet; while no networks from these providers are present within the project boundary, some eNet networks are located along or near the route designated for Extraordinary Abnormal Loads.

### 3.1.1 Existing Gas Networks

#### 3.1.1.1 Transmission Line

There is a 650mm diameter high pressure gas transmission main which runs south to north through the existing site. The location of the transmission line is presented in the obtained utility records in Appendix A.

#### 3.1.1.2 Gas Wayleave and GNI consultation distances

There are wayleave distances associated with the gas transmission line that need to be observed for varying types of activity, a synopsis of these distances is shown in Table 3-1.

| Activity                   | Distance within which GNI shall be consulted                                     |
|----------------------------|--|
| Any excavation actions     | 10m  |
| Piling                     | 15m  |
| Surface mineral extraction | 100m   |
| Land filling               | 100m   |
| Demolition                 | 150m   |
| Blasting                   | 400m   |
| Wind farm                  | 2 times the turbine mast height from the nearest edge of a transmission pipeline |
| Trenchless techniques      | 10m  |
| Pressure testing           | 8m   |

Table 3-1 - Excerpt from GNI COP 'Working in the vicinity of the transmission network'.

### 3.1.2 Existing ESB Network

Existing ESB utility maps are included in Appendix A.



# 4. Proposed Infrastructure

## 4.1 Foul sewer

The onsite foul sewer has been designed and will be constructed in accordance with Uisce Éireann standards. It is proposed to install a small foul sewer network which will be partly gravity fed and partly pumped. The pumped section of the sewer will be to lift the effluent from the administration building to the proposed waste water treatment plant (WWTP). The proposed WWTP will be designed and installed in accordance with the current EPA Code of Practice Domestic Waste Water Treatment Systems. The foul sewer network will include a small package pump station. The rising main is approximately 35m in length and will discharge to a Uisce Éireann standard decompression manhole before discharging to the proposed WWTP.

The proposed peaker plant is proposed to be remotely controlled where possible and as such the staff on site will generally be 2-3 maintenance staff or security with an expected maximum population of 10 persons at any one time.

As such the proposed WWTP will be a package domestic plant such as a 10 Person ONE2CLEAN Wastewater Treatment System by Graf G50006 (or similar). This will discharge to underground storage tanks which will be emptied by tanker as required and taken to a municipal WWTP for disposal by a licensed contractor. The onsite WWTP is to prevent septicity occurring in the storage tanks between collection times.

The storage tanks will be sized as follows:

Maximum population on site = 10 persons.

Uisce Éireann allows 100 litres/person/day for onsite canteen

Storage for 7 days = 7 x 10 x 100 = 7000 litres.

As such it is proposed to install a 10cu.m underground GRP cesspool tank surrounded in concrete to contain the waste.

### 4.1.1 Foul sewer design parameters

| Sl. No. | Particulars                     | Value  |
|---------|---------------------------------|--|
| 1.      | Frequency of use (Kdu)          | 0  |
| 2.      | Flow per dwelling per day (l/s) | 0  |
| 3.      | Domestic flow (l/s/ha)          | 0  |
| 4.      | Industrial flow (l/s/ha)        | 0  |
| 5.      | Additional flow (%)             | 0  |
| 6.      | Minimum Velocity                | 0.75 m/s for pipes less than 300mm diameter<br>0.77 m/s for pipes 375mm and 450mm diameter |



BASELINE

|     |                                   |   |
|-----|-----------------------------------|---|
|     |                                   | (Page number 46, Wastewater-Code-of-Practice)   |
| 7.  | Maximum Velocity                  | 2.50 m/s (Page number 46, Wastewater-Code-of-Practice)  |
| 8.  | Minimum Pipe Diameter             | 150 mm (Clause 3.8 and Table: Sewer Size/Gradient for Multiple Properties, page number 45, Wastewater-Code-of-Practice)   |
| 9.  | Minimum cover depth of pipe       | <p>Areas without any possibility of vehicular access - depth not less than 0.5 m</p> <p>Driveways, footways, parking areas and yards with height restrictions to prevent entry by vehicles with a gross vehicle weight in excess of 7.5 tonnes - depth not less than 0.75 m</p> <p>Agricultural land and public open space - depth not less than 0.9 m</p> <p>Other roadways, highways and parking areas with unrestricted access to vehicles with a gross vehicle weight in excess of 7.5 tonnes – depth not less than 1.2 m.</p> <p>(Clause 3.9, Wastewater-Code-of-Practice)</p> |
| 10. | Chamber Diameter                  | <p>1200mm diameter chamber for pipes less than 375mm diameter</p> <p>1350mm diameter chamber for pipes of 375mm to 450 mm diameter</p> <p>(Clause 3.12.2, page number 56, Wastewater-Code-of-Practice)</p>  |
| 11. | Maximum distance between chambers | <p>90m for pipes of 225mm diameter and above</p> <p>75m for pipes of 150mm diameter</p> <p>(Clause 3.3.5.8. Wastewater-Code-of-Practice)</p>  |
| 12. | Flow rates                        | <p>100 l/day (Appendix C, Wastewater-Code-of-Practice)</p> <p>Considering 10 person/day on site, total flow is <math>10 \times 100 = 1000</math> l/day = 0.0116 l/s</p> <p>In the model, a minimum value of 0.1 l/s is required. So the same is considered at each outlet</p>   |



|     |                                   |  |
|-----|-----------------------------------|--|
| 13. | Septic tank                       | Tank is assumed to be emptied once a week. So, it's capacity is 10X100X7 = 7000 cubic meter.<br><br>Considering any delay in empty, a volume of 10000 cubic meter is considered  |
| 14. | Minimum rising main pipe diameter | The minimum size for a Rising Main should not be less than 80mm internal diameter. Rising Mains less than 80mm will only be considered with the use of appropriately sized/type pumps. (Clause 3.8, Wastewater-Code-of-Practice) |
| 15. | Velocity range of rising main     | 0.75 m/s to 1.8 m/s (Clause 3.2, Wastewater-Code-of-Practice)  |
| 16. | Pump                              | The flow rate is 1.8 l/s (6X0.3) as per clause 5.8 and 5.9.7, Wastewater-Code-of-Practice  |

**Table 4-1 - Foul Sewer design parameters**

The foul sewer design calculations are presented in Appendix D and the reader should refer to the engineering planning pack for the foul sewer layout drawings.

## 4.2 Storm Sewer

It is proposed to provide the site with a new storm sewer network which will include SuDS measures where practicable. There are no storm sewers or culverts in the immediate surroundings and as such it is proposed to discharge stormwater generated by the development by infiltration to ground.

The new network will be segregated into different sections to facilitate contaminated fire water collection and flow by gravity. The segregated areas will be controlled by actuator valves to control the flow path of these areas. The reader is referred to the submitted storm drainage drawings.

The site will require an IE License from the EPA and as such is limited in its discharge of stormwater to ground due to the possibility of contaminated firewater in the discharge. The proposed SuDS measures to be included are:

- Filter drains (external to the site)
- Infiltration pond with hydrocarbon interceptor.
- Sealed permeable paving (car parking areas)

The storm runoff will be collected through a series of gullies, linear drains and filter drains and will ultimately discharge to the infiltration pond to the north of the site via a class 1 full retention hydrocarbon separator. A BRE365 infiltration test has been carried out and is presented in Appendix F. The results of this test are the basis of design for the infiltration pond. The pond has been sized for the 100 year storm event + 20% climate change. A section through the pond including levels is include in the drainage drawings submitted as part of the planning drawings.

The storm drainage network has been designed with the following design criteria:

For collection and conveyance systems, the following storm events are to be considered with the associated surcharge requirements:



- 1 in 5 year + 20% climate change – Surcharge of the drainage system is allowed
- 1 in 30 year + 20% climate change – No flooding of the drainage system. For Swales this means 150 mm of freeboard should be achieved.
- 1 in 100 year + 20% climate change - Some short-term flooding managed such that it does not enter buildings or disrupt emergency access routes.

### 4.2.1 Design Parameters

| Sl. No.  | Particulars                 | Value   |          |       |       |       |       |       |       |       |       |    |     |     |        |     |     |     |     |     |     |     |     |     |      |      |         |     |     |     |     |     |     |     |      |      |      |      |         |     |     |     |     |     |     |      |      |      |      |      |         |     |     |     |      |      |      |      |      |      |      |      |         |     |      |      |      |      |      |      |      |      |      |      |         |      |      |      |      |      |      |      |      |      |      |      |         |      |      |      |      |      |      |      |      |      |      |      |         |      |      |      |      |      |      |      |      |      |      |      |         |      |      |      |      |      |      |      |      |      |      |      |         |      |      |      |      |      |      |      |      |      |      |      |          |      |      |      |      |      |      |      |      |      |      |      |          |      |      |      |      |      |      |      |      |      |      |      |          |      |      |      |      |      |      |      |      |      |      |      |        |      |      |      |      |      |      |      |      |      |      |      |        |      |      |      |      |      |      |      |      |      |       |       |        |      |      |      |      |      |      |      |      |       |       |       |        |      |      |      |      |      |      |       |       |       |       |       |        |      |      |      |      |       |       |       |       |       |       |       |         |      |      |       |       |       |       |       |       |       |       |       |         |      |       |       |       |       |       |       |       |       |       |       |         |       |       |       |       |       |       |       |       |       |       |       |         |       |       |       |       |       |       |       |       |       |       |       |         |       |       |       |       |       |       |       |       |       |       |       |
|----------|-----------------------------|---|----------|-------|-------|-------|-------|-------|-------|-------|-------|----|-----|-----|--------|-----|-----|-----|-----|-----|-----|-----|-----|-----|------|------|---------|-----|-----|-----|-----|-----|-----|-----|------|------|------|------|---------|-----|-----|-----|-----|-----|-----|------|------|------|------|------|---------|-----|-----|-----|------|------|------|------|------|------|------|------|---------|-----|------|------|------|------|------|------|------|------|------|------|---------|------|------|------|------|------|------|------|------|------|------|------|---------|------|------|------|------|------|------|------|------|------|------|------|---------|------|------|------|------|------|------|------|------|------|------|------|---------|------|------|------|------|------|------|------|------|------|------|------|---------|------|------|------|------|------|------|------|------|------|------|------|----------|------|------|------|------|------|------|------|------|------|------|------|----------|------|------|------|------|------|------|------|------|------|------|------|----------|------|------|------|------|------|------|------|------|------|------|------|--------|------|------|------|------|------|------|------|------|------|------|------|--------|------|------|------|------|------|------|------|------|------|-------|-------|--------|------|------|------|------|------|------|------|------|-------|-------|-------|--------|------|------|------|------|------|------|-------|-------|-------|-------|-------|--------|------|------|------|------|-------|-------|-------|-------|-------|-------|-------|---------|------|------|-------|-------|-------|-------|-------|-------|-------|-------|-------|---------|------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|---------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|---------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|---------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| 1.       | Rainfall Method             | Flood Studies Report (FSR)  |          |       |       |       |       |       |       |       |       |    |     |     |        |     |     |     |     |     |     |     |     |     |      |      |         |     |     |     |     |     |     |     |      |      |      |      |         |     |     |     |     |     |     |      |      |      |      |      |         |     |     |     |      |      |      |      |      |      |      |      |         |     |      |      |      |      |      |      |      |      |      |      |         |      |      |      |      |      |      |      |      |      |      |      |         |      |      |      |      |      |      |      |      |      |      |      |         |      |      |      |      |      |      |      |      |      |      |      |         |      |      |      |      |      |      |      |      |      |      |      |         |      |      |      |      |      |      |      |      |      |      |      |          |      |      |      |      |      |      |      |      |      |      |      |          |      |      |      |      |      |      |      |      |      |      |      |          |      |      |      |      |      |      |      |      |      |      |      |        |      |      |      |      |      |      |      |      |      |      |      |        |      |      |      |      |      |      |      |      |      |       |       |        |      |      |      |      |      |      |      |      |       |       |       |        |      |      |      |      |      |      |       |       |       |       |       |        |      |      |      |      |       |       |       |       |       |       |       |         |      |      |       |       |       |       |       |       |       |       |       |         |      |       |       |       |       |       |       |       |       |       |       |         |       |       |       |       |       |       |       |       |       |       |       |         |       |       |       |       |       |       |       |       |       |       |       |         |       |       |       |       |       |       |       |       |       |       |       |
| 2.       | Return period               | 5 years   |          |       |       |       |       |       |       |       |       |    |     |     |        |     |     |     |     |     |     |     |     |     |      |      |         |     |     |     |     |     |     |     |      |      |      |      |         |     |     |     |     |     |     |      |      |      |      |      |         |     |     |     |      |      |      |      |      |      |      |      |         |     |      |      |      |      |      |      |      |      |      |      |         |      |      |      |      |      |      |      |      |      |      |      |         |      |      |      |      |      |      |      |      |      |      |      |         |      |      |      |      |      |      |      |      |      |      |      |         |      |      |      |      |      |      |      |      |      |      |      |         |      |      |      |      |      |      |      |      |      |      |      |          |      |      |      |      |      |      |      |      |      |      |      |          |      |      |      |      |      |      |      |      |      |      |      |          |      |      |      |      |      |      |      |      |      |      |      |        |      |      |      |      |      |      |      |      |      |      |      |        |      |      |      |      |      |      |      |      |      |       |       |        |      |      |      |      |      |      |      |      |       |       |       |        |      |      |      |      |      |      |       |       |       |       |       |        |      |      |      |      |       |       |       |       |       |       |       |         |      |      |       |       |       |       |       |       |       |       |       |         |      |       |       |       |       |       |       |       |       |       |       |         |       |       |       |       |       |       |       |       |       |       |       |         |       |       |       |       |       |       |       |       |       |       |       |         |       |       |       |       |       |       |       |       |       |       |       |
| 3.       | M5-60                       | 15.6 mm (Easting=146600, Northing=228137)   |          |       |       |       |       |       |       |       |       |    |     |     |        |     |     |     |     |     |     |     |     |     |      |      |         |     |     |     |     |     |     |     |      |      |      |      |         |     |     |     |     |     |     |      |      |      |      |      |         |     |     |     |      |      |      |      |      |      |      |      |         |     |      |      |      |      |      |      |      |      |      |      |         |      |      |      |      |      |      |      |      |      |      |      |         |      |      |      |      |      |      |      |      |      |      |      |         |      |      |      |      |      |      |      |      |      |      |      |         |      |      |      |      |      |      |      |      |      |      |      |         |      |      |      |      |      |      |      |      |      |      |      |          |      |      |      |      |      |      |      |      |      |      |      |          |      |      |      |      |      |      |      |      |      |      |      |          |      |      |      |      |      |      |      |      |      |      |      |        |      |      |      |      |      |      |      |      |      |      |      |        |      |      |      |      |      |      |      |      |      |       |       |        |      |      |      |      |      |      |      |      |       |       |       |        |      |      |      |      |      |      |       |       |       |       |       |        |      |      |      |      |       |       |       |       |       |       |       |         |      |      |       |       |       |       |       |       |       |       |       |         |      |       |       |       |       |       |       |       |       |       |       |         |       |       |       |       |       |       |       |       |       |       |       |         |       |       |       |       |       |       |       |       |       |       |       |         |       |       |       |       |       |       |       |       |       |       |       |
| 4.       | Ratio R                     | 0.26 (15.6/59.8)  |          |       |       |       |       |       |       |       |       |    |     |     |        |     |     |     |     |     |     |     |     |     |      |      |         |     |     |     |     |     |     |     |      |      |      |      |         |     |     |     |     |     |     |      |      |      |      |      |         |     |     |     |      |      |      |      |      |      |      |      |         |     |      |      |      |      |      |      |      |      |      |      |         |      |      |      |      |      |      |      |      |      |      |      |         |      |      |      |      |      |      |      |      |      |      |      |         |      |      |      |      |      |      |      |      |      |      |      |         |      |      |      |      |      |      |      |      |      |      |      |         |      |      |      |      |      |      |      |      |      |      |      |          |      |      |      |      |      |      |      |      |      |      |      |          |      |      |      |      |      |      |      |      |      |      |      |          |      |      |      |      |      |      |      |      |      |      |      |        |      |      |      |      |      |      |      |      |      |      |      |        |      |      |      |      |      |      |      |      |      |       |       |        |      |      |      |      |      |      |      |      |       |       |       |        |      |      |      |      |      |      |       |       |       |       |       |        |      |      |      |      |       |       |       |       |       |       |       |         |      |      |       |       |       |       |       |       |       |       |       |         |      |       |       |       |       |       |       |       |       |       |       |         |       |       |       |       |       |       |       |       |       |       |       |         |       |       |       |       |       |       |       |       |       |       |       |         |       |       |       |       |       |       |       |       |       |       |       |
|          |                             | <p>Met Eireann<br/>Return Period Rainfall Depths for sliding Durations<br/>Irish Grid: Easting: 146600, Northing: 228137</p> <table border="1"> <thead> <tr> <th>Interval</th> <th>2</th> <th>3</th> <th>4</th> <th>5</th> <th>10</th> <th>20</th> <th>30</th> <th>50</th> <th>75</th> <th>100</th> <th>120</th> </tr> </thead> <tbody> <tr> <td>5 mins</td> <td>2.7</td> <td>3.7</td> <td>4.2</td> <td>4.9</td> <td>5.4</td> <td>5.8</td> <td>7.1</td> <td>8.4</td> <td>9.3</td> <td>10.5</td> <td>11.6</td> </tr> <tr> <td>10 mins</td> <td>3.8</td> <td>5.1</td> <td>5.8</td> <td>6.9</td> <td>7.6</td> <td>8.1</td> <td>9.8</td> <td>11.7</td> <td>13.0</td> <td>14.7</td> <td>16.2</td> </tr> <tr> <td>15 mins</td> <td>4.4</td> <td>6.0</td> <td>6.9</td> <td>8.1</td> <td>8.9</td> <td>9.5</td> <td>11.6</td> <td>13.8</td> <td>15.3</td> <td>17.3</td> <td>19.1</td> </tr> <tr> <td>30 mins</td> <td>5.9</td> <td>7.9</td> <td>8.9</td> <td>10.4</td> <td>11.4</td> <td>12.2</td> <td>14.7</td> <td>17.4</td> <td>19.1</td> <td>21.5</td> <td>23.6</td> </tr> <tr> <td>1 hours</td> <td>7.8</td> <td>10.3</td> <td>11.6</td> <td>13.4</td> <td>14.7</td> <td>15.6</td> <td>18.6</td> <td>21.8</td> <td>23.9</td> <td>26.8</td> <td>29.3</td> </tr> <tr> <td>2 hours</td> <td>10.3</td> <td>13.4</td> <td>15.0</td> <td>17.3</td> <td>18.8</td> <td>19.9</td> <td>23.6</td> <td>27.5</td> <td>30.0</td> <td>33.4</td> <td>36.4</td> </tr> <tr> <td>3 hours</td> <td>12.1</td> <td>15.6</td> <td>17.4</td> <td>20.0</td> <td>21.7</td> <td>23.0</td> <td>27.1</td> <td>31.4</td> <td>34.2</td> <td>38.0</td> <td>41.2</td> </tr> <tr> <td>4 hours</td> <td>13.6</td> <td>17.5</td> <td>19.4</td> <td>22.2</td> <td>24.1</td> <td>25.5</td> <td>29.9</td> <td>34.6</td> <td>37.5</td> <td>41.6</td> <td>45.1</td> </tr> <tr> <td>6 hours</td> <td>16.0</td> <td>20.4</td> <td>22.6</td> <td>25.8</td> <td>27.9</td> <td>29.4</td> <td>34.3</td> <td>39.5</td> <td>42.8</td> <td>47.3</td> <td>51.1</td> </tr> <tr> <td>9 hours</td> <td>18.8</td> <td>23.8</td> <td>26.3</td> <td>29.9</td> <td>32.2</td> <td>34.0</td> <td>39.4</td> <td>45.2</td> <td>48.8</td> <td>53.8</td> <td>58.0</td> </tr> <tr> <td>12 hours</td> <td>21.1</td> <td>26.6</td> <td>29.3</td> <td>33.2</td> <td>35.7</td> <td>37.6</td> <td>43.5</td> <td>49.7</td> <td>53.6</td> <td>58.9</td> <td>63.4</td> </tr> <tr> <td>18 hours</td> <td>24.9</td> <td>31.1</td> <td>34.2</td> <td>38.5</td> <td>41.3</td> <td>43.4</td> <td>49.9</td> <td>56.8</td> <td>61.1</td> <td>67.0</td> <td>71.9</td> </tr> <tr> <td>24 hours</td> <td>27.9</td> <td>34.7</td> <td>38.0</td> <td>42.8</td> <td>45.8</td> <td>48.1</td> <td>55.1</td> <td>62.5</td> <td>67.1</td> <td>73.3</td> <td>78.6</td> </tr> <tr> <td>2 days</td> <td>36.3</td> <td>44.4</td> <td>48.2</td> <td>53.7</td> <td>57.2</td> <td>60.0</td> <td>67.8</td> <td>76.1</td> <td>81.2</td> <td>88.1</td> <td>93.9</td> </tr> <tr> <td>3 days</td> <td>43.5</td> <td>52.5</td> <td>56.9</td> <td>62.9</td> <td>66.8</td> <td>69.6</td> <td>78.4</td> <td>87.5</td> <td>93.1</td> <td>100.5</td> <td>106.7</td> </tr> <tr> <td>4 days</td> <td>49.9</td> <td>59.8</td> <td>64.6</td> <td>71.2</td> <td>75.4</td> <td>78.5</td> <td>88.0</td> <td>97.7</td> <td>103.7</td> <td>111.6</td> <td>118.3</td> </tr> <tr> <td>6 days</td> <td>61.7</td> <td>73.1</td> <td>78.6</td> <td>86.1</td> <td>90.9</td> <td>94.4</td> <td>105.1</td> <td>116.0</td> <td>122.7</td> <td>131.5</td> <td>138.8</td> </tr> <tr> <td>8 days</td> <td>72.4</td> <td>85.2</td> <td>91.3</td> <td>99.7</td> <td>104.9</td> <td>108.8</td> <td>120.5</td> <td>132.5</td> <td>139.8</td> <td>149.3</td> <td>157.3</td> </tr> <tr> <td>10 days</td> <td>82.6</td> <td>96.6</td> <td>103.2</td> <td>112.3</td> <td>118.0</td> <td>122.3</td> <td>135.0</td> <td>147.8</td> <td>155.7</td> <td>165.9</td> <td>174.5</td> </tr> <tr> <td>12 days</td> <td>92.3</td> <td>107.5</td> <td>114.6</td> <td>124.4</td> <td>130.5</td> <td>135.0</td> <td>148.6</td> <td>162.4</td> <td>170.7</td> <td>181.6</td> <td>190.7</td> </tr> <tr> <td>16 days</td> <td>110.9</td> <td>128.1</td> <td>136.2</td> <td>147.3</td> <td>154.1</td> <td>159.2</td> <td>174.4</td> <td>189.7</td> <td>198.9</td> <td>211.0</td> <td>221.0</td> </tr> <tr> <td>20 days</td> <td>128.6</td> <td>147.8</td> <td>156.8</td> <td>168.9</td> <td>176.5</td> <td>182.0</td> <td>198.7</td> <td>215.4</td> <td>225.4</td> <td>238.5</td> <td>249.4</td> </tr> <tr> <td>25 days</td> <td>150.1</td> <td>171.5</td> <td>181.4</td> <td>194.9</td> <td>203.2</td> <td>209.3</td> <td>227.6</td> <td>245.9</td> <td>256.9</td> <td>271.2</td> <td>283.0</td> </tr> </tbody> </table> | Interval | 2     | 3     | 4     | 5     | 10    | 20    | 30    | 50    | 75 | 100 | 120 | 5 mins | 2.7 | 3.7 | 4.2 | 4.9 | 5.4 | 5.8 | 7.1 | 8.4 | 9.3 | 10.5 | 11.6 | 10 mins | 3.8 | 5.1 | 5.8 | 6.9 | 7.6 | 8.1 | 9.8 | 11.7 | 13.0 | 14.7 | 16.2 | 15 mins | 4.4 | 6.0 | 6.9 | 8.1 | 8.9 | 9.5 | 11.6 | 13.8 | 15.3 | 17.3 | 19.1 | 30 mins | 5.9 | 7.9 | 8.9 | 10.4 | 11.4 | 12.2 | 14.7 | 17.4 | 19.1 | 21.5 | 23.6 | 1 hours | 7.8 | 10.3 | 11.6 | 13.4 | 14.7 | 15.6 | 18.6 | 21.8 | 23.9 | 26.8 | 29.3 | 2 hours | 10.3 | 13.4 | 15.0 | 17.3 | 18.8 | 19.9 | 23.6 | 27.5 | 30.0 | 33.4 | 36.4 | 3 hours | 12.1 | 15.6 | 17.4 | 20.0 | 21.7 | 23.0 | 27.1 | 31.4 | 34.2 | 38.0 | 41.2 | 4 hours | 13.6 | 17.5 | 19.4 | 22.2 | 24.1 | 25.5 | 29.9 | 34.6 | 37.5 | 41.6 | 45.1 | 6 hours | 16.0 | 20.4 | 22.6 | 25.8 | 27.9 | 29.4 | 34.3 | 39.5 | 42.8 | 47.3 | 51.1 | 9 hours | 18.8 | 23.8 | 26.3 | 29.9 | 32.2 | 34.0 | 39.4 | 45.2 | 48.8 | 53.8 | 58.0 | 12 hours | 21.1 | 26.6 | 29.3 | 33.2 | 35.7 | 37.6 | 43.5 | 49.7 | 53.6 | 58.9 | 63.4 | 18 hours | 24.9 | 31.1 | 34.2 | 38.5 | 41.3 | 43.4 | 49.9 | 56.8 | 61.1 | 67.0 | 71.9 | 24 hours | 27.9 | 34.7 | 38.0 | 42.8 | 45.8 | 48.1 | 55.1 | 62.5 | 67.1 | 73.3 | 78.6 | 2 days | 36.3 | 44.4 | 48.2 | 53.7 | 57.2 | 60.0 | 67.8 | 76.1 | 81.2 | 88.1 | 93.9 | 3 days | 43.5 | 52.5 | 56.9 | 62.9 | 66.8 | 69.6 | 78.4 | 87.5 | 93.1 | 100.5 | 106.7 | 4 days | 49.9 | 59.8 | 64.6 | 71.2 | 75.4 | 78.5 | 88.0 | 97.7 | 103.7 | 111.6 | 118.3 | 6 days | 61.7 | 73.1 | 78.6 | 86.1 | 90.9 | 94.4 | 105.1 | 116.0 | 122.7 | 131.5 | 138.8 | 8 days | 72.4 | 85.2 | 91.3 | 99.7 | 104.9 | 108.8 | 120.5 | 132.5 | 139.8 | 149.3 | 157.3 | 10 days | 82.6 | 96.6 | 103.2 | 112.3 | 118.0 | 122.3 | 135.0 | 147.8 | 155.7 | 165.9 | 174.5 | 12 days | 92.3 | 107.5 | 114.6 | 124.4 | 130.5 | 135.0 | 148.6 | 162.4 | 170.7 | 181.6 | 190.7 | 16 days | 110.9 | 128.1 | 136.2 | 147.3 | 154.1 | 159.2 | 174.4 | 189.7 | 198.9 | 211.0 | 221.0 | 20 days | 128.6 | 147.8 | 156.8 | 168.9 | 176.5 | 182.0 | 198.7 | 215.4 | 225.4 | 238.5 | 249.4 | 25 days | 150.1 | 171.5 | 181.4 | 194.9 | 203.2 | 209.3 | 227.6 | 245.9 | 256.9 | 271.2 | 283.0 |
| Interval | 2                           | 3   | 4        | 5     | 10    | 20    | 30    | 50    | 75    | 100   | 120   |    |     |     |        |     |     |     |     |     |     |     |     |     |      |      |         |     |     |     |     |     |     |     |      |      |      |      |         |     |     |     |     |     |     |      |      |      |      |      |         |     |     |     |      |      |      |      |      |      |      |      |         |     |      |      |      |      |      |      |      |      |      |      |         |      |      |      |      |      |      |      |      |      |      |      |         |      |      |      |      |      |      |      |      |      |      |      |         |      |      |      |      |      |      |      |      |      |      |      |         |      |      |      |      |      |      |      |      |      |      |      |         |      |      |      |      |      |      |      |      |      |      |      |          |      |      |      |      |      |      |      |      |      |      |      |          |      |      |      |      |      |      |      |      |      |      |      |          |      |      |      |      |      |      |      |      |      |      |      |        |      |      |      |      |      |      |      |      |      |      |      |        |      |      |      |      |      |      |      |      |      |       |       |        |      |      |      |      |      |      |      |      |       |       |       |        |      |      |      |      |      |      |       |       |       |       |       |        |      |      |      |      |       |       |       |       |       |       |       |         |      |      |       |       |       |       |       |       |       |       |       |         |      |       |       |       |       |       |       |       |       |       |       |         |       |       |       |       |       |       |       |       |       |       |       |         |       |       |       |       |       |       |       |       |       |       |       |         |       |       |       |       |       |       |       |       |       |       |       |
| 5 mins   | 2.7                         | 3.7   | 4.2      | 4.9   | 5.4   | 5.8   | 7.1   | 8.4   | 9.3   | 10.5  | 11.6  |    |     |     |        |     |     |     |     |     |     |     |     |     |      |      |         |     |     |     |     |     |     |     |      |      |      |      |         |     |     |     |     |     |     |      |      |      |      |      |         |     |     |     |      |      |      |      |      |      |      |      |         |     |      |      |      |      |      |      |      |      |      |      |         |      |      |      |      |      |      |      |      |      |      |      |         |      |      |      |      |      |      |      |      |      |      |      |         |      |      |      |      |      |      |      |      |      |      |      |         |      |      |      |      |      |      |      |      |      |      |      |         |      |      |      |      |      |      |      |      |      |      |      |          |      |      |      |      |      |      |      |      |      |      |      |          |      |      |      |      |      |      |      |      |      |      |      |          |      |      |      |      |      |      |      |      |      |      |      |        |      |      |      |      |      |      |      |      |      |      |      |        |      |      |      |      |      |      |      |      |      |       |       |        |      |      |      |      |      |      |      |      |       |       |       |        |      |      |      |      |      |      |       |       |       |       |       |        |      |      |      |      |       |       |       |       |       |       |       |         |      |      |       |       |       |       |       |       |       |       |       |         |      |       |       |       |       |       |       |       |       |       |       |         |       |       |       |       |       |       |       |       |       |       |       |         |       |       |       |       |       |       |       |       |       |       |       |         |       |       |       |       |       |       |       |       |       |       |       |
| 10 mins  | 3.8                         | 5.1   | 5.8      | 6.9   | 7.6   | 8.1   | 9.8   | 11.7  | 13.0  | 14.7  | 16.2  |    |     |     |        |     |     |     |     |     |     |     |     |     |      |      |         |     |     |     |     |     |     |     |      |      |      |      |         |     |     |     |     |     |     |      |      |      |      |      |         |     |     |     |      |      |      |      |      |      |      |      |         |     |      |      |      |      |      |      |      |      |      |      |         |      |      |      |      |      |      |      |      |      |      |      |         |      |      |      |      |      |      |      |      |      |      |      |         |      |      |      |      |      |      |      |      |      |      |      |         |      |      |      |      |      |      |      |      |      |      |      |         |      |      |      |      |      |      |      |      |      |      |      |          |      |      |      |      |      |      |      |      |      |      |      |          |      |      |      |      |      |      |      |      |      |      |      |          |      |      |      |      |      |      |      |      |      |      |      |        |      |      |      |      |      |      |      |      |      |      |      |        |      |      |      |      |      |      |      |      |      |       |       |        |      |      |      |      |      |      |      |      |       |       |       |        |      |      |      |      |      |      |       |       |       |       |       |        |      |      |      |      |       |       |       |       |       |       |       |         |      |      |       |       |       |       |       |       |       |       |       |         |      |       |       |       |       |       |       |       |       |       |       |         |       |       |       |       |       |       |       |       |       |       |       |         |       |       |       |       |       |       |       |       |       |       |       |         |       |       |       |       |       |       |       |       |       |       |       |
| 15 mins  | 4.4                         | 6.0   | 6.9      | 8.1   | 8.9   | 9.5   | 11.6  | 13.8  | 15.3  | 17.3  | 19.1  |    |     |     |        |     |     |     |     |     |     |     |     |     |      |      |         |     |     |     |     |     |     |     |      |      |      |      |         |     |     |     |     |     |     |      |      |      |      |      |         |     |     |     |      |      |      |      |      |      |      |      |         |     |      |      |      |      |      |      |      |      |      |      |         |      |      |      |      |      |      |      |      |      |      |      |         |      |      |      |      |      |      |      |      |      |      |      |         |      |      |      |      |      |      |      |      |      |      |      |         |      |      |      |      |      |      |      |      |      |      |      |         |      |      |      |      |      |      |      |      |      |      |      |          |      |      |      |      |      |      |      |      |      |      |      |          |      |      |      |      |      |      |      |      |      |      |      |          |      |      |      |      |      |      |      |      |      |      |      |        |      |      |      |      |      |      |      |      |      |      |      |        |      |      |      |      |      |      |      |      |      |       |       |        |      |      |      |      |      |      |      |      |       |       |       |        |      |      |      |      |      |      |       |       |       |       |       |        |      |      |      |      |       |       |       |       |       |       |       |         |      |      |       |       |       |       |       |       |       |       |       |         |      |       |       |       |       |       |       |       |       |       |       |         |       |       |       |       |       |       |       |       |       |       |       |         |       |       |       |       |       |       |       |       |       |       |       |         |       |       |       |       |       |       |       |       |       |       |       |
| 30 mins  | 5.9                         | 7.9   | 8.9      | 10.4  | 11.4  | 12.2  | 14.7  | 17.4  | 19.1  | 21.5  | 23.6  |    |     |     |        |     |     |     |     |     |     |     |     |     |      |      |         |     |     |     |     |     |     |     |      |      |      |      |         |     |     |     |     |     |     |      |      |      |      |      |         |     |     |     |      |      |      |      |      |      |      |      |         |     |      |      |      |      |      |      |      |      |      |      |         |      |      |      |      |      |      |      |      |      |      |      |         |      |      |      |      |      |      |      |      |      |      |      |         |      |      |      |      |      |      |      |      |      |      |      |         |      |      |      |      |      |      |      |      |      |      |      |         |      |      |      |      |      |      |      |      |      |      |      |          |      |      |      |      |      |      |      |      |      |      |      |          |      |      |      |      |      |      |      |      |      |      |      |          |      |      |      |      |      |      |      |      |      |      |      |        |      |      |      |      |      |      |      |      |      |      |      |        |      |      |      |      |      |      |      |      |      |       |       |        |      |      |      |      |      |      |      |      |       |       |       |        |      |      |      |      |      |      |       |       |       |       |       |        |      |      |      |      |       |       |       |       |       |       |       |         |      |      |       |       |       |       |       |       |       |       |       |         |      |       |       |       |       |       |       |       |       |       |       |         |       |       |       |       |       |       |       |       |       |       |       |         |       |       |       |       |       |       |       |       |       |       |       |         |       |       |       |       |       |       |       |       |       |       |       |
| 1 hours  | 7.8                         | 10.3  | 11.6     | 13.4  | 14.7  | 15.6  | 18.6  | 21.8  | 23.9  | 26.8  | 29.3  |    |     |     |        |     |     |     |     |     |     |     |     |     |      |      |         |     |     |     |     |     |     |     |      |      |      |      |         |     |     |     |     |     |     |      |      |      |      |      |         |     |     |     |      |      |      |      |      |      |      |      |         |     |      |      |      |      |      |      |      |      |      |      |         |      |      |      |      |      |      |      |      |      |      |      |         |      |      |      |      |      |      |      |      |      |      |      |         |      |      |      |      |      |      |      |      |      |      |      |         |      |      |      |      |      |      |      |      |      |      |      |         |      |      |      |      |      |      |      |      |      |      |      |          |      |      |      |      |      |      |      |      |      |      |      |          |      |      |      |      |      |      |      |      |      |      |      |          |      |      |      |      |      |      |      |      |      |      |      |        |      |      |      |      |      |      |      |      |      |      |      |        |      |      |      |      |      |      |      |      |      |       |       |        |      |      |      |      |      |      |      |      |       |       |       |        |      |      |      |      |      |      |       |       |       |       |       |        |      |      |      |      |       |       |       |       |       |       |       |         |      |      |       |       |       |       |       |       |       |       |       |         |      |       |       |       |       |       |       |       |       |       |       |         |       |       |       |       |       |       |       |       |       |       |       |         |       |       |       |       |       |       |       |       |       |       |       |         |       |       |       |       |       |       |       |       |       |       |       |
| 2 hours  | 10.3                        | 13.4  | 15.0     | 17.3  | 18.8  | 19.9  | 23.6  | 27.5  | 30.0  | 33.4  | 36.4  |    |     |     |        |     |     |     |     |     |     |     |     |     |      |      |         |     |     |     |     |     |     |     |      |      |      |      |         |     |     |     |     |     |     |      |      |      |      |      |         |     |     |     |      |      |      |      |      |      |      |      |         |     |      |      |      |      |      |      |      |      |      |      |         |      |      |      |      |      |      |      |      |      |      |      |         |      |      |      |      |      |      |      |      |      |      |      |         |      |      |      |      |      |      |      |      |      |      |      |         |      |      |      |      |      |      |      |      |      |      |      |         |      |      |      |      |      |      |      |      |      |      |      |          |      |      |      |      |      |      |      |      |      |      |      |          |      |      |      |      |      |      |      |      |      |      |      |          |      |      |      |      |      |      |      |      |      |      |      |        |      |      |      |      |      |      |      |      |      |      |      |        |      |      |      |      |      |      |      |      |      |       |       |        |      |      |      |      |      |      |      |      |       |       |       |        |      |      |      |      |      |      |       |       |       |       |       |        |      |      |      |      |       |       |       |       |       |       |       |         |      |      |       |       |       |       |       |       |       |       |       |         |      |       |       |       |       |       |       |       |       |       |       |         |       |       |       |       |       |       |       |       |       |       |       |         |       |       |       |       |       |       |       |       |       |       |       |         |       |       |       |       |       |       |       |       |       |       |       |
| 3 hours  | 12.1                        | 15.6  | 17.4     | 20.0  | 21.7  | 23.0  | 27.1  | 31.4  | 34.2  | 38.0  | 41.2  |    |     |     |        |     |     |     |     |     |     |     |     |     |      |      |         |     |     |     |     |     |     |     |      |      |      |      |         |     |     |     |     |     |     |      |      |      |      |      |         |     |     |     |      |      |      |      |      |      |      |      |         |     |      |      |      |      |      |      |      |      |      |      |         |      |      |      |      |      |      |      |      |      |      |      |         |      |      |      |      |      |      |      |      |      |      |      |         |      |      |      |      |      |      |      |      |      |      |      |         |      |      |      |      |      |      |      |      |      |      |      |         |      |      |      |      |      |      |      |      |      |      |      |          |      |      |      |      |      |      |      |      |      |      |      |          |      |      |      |      |      |      |      |      |      |      |      |          |      |      |      |      |      |      |      |      |      |      |      |        |      |      |      |      |      |      |      |      |      |      |      |        |      |      |      |      |      |      |      |      |      |       |       |        |      |      |      |      |      |      |      |      |       |       |       |        |      |      |      |      |      |      |       |       |       |       |       |        |      |      |      |      |       |       |       |       |       |       |       |         |      |      |       |       |       |       |       |       |       |       |       |         |      |       |       |       |       |       |       |       |       |       |       |         |       |       |       |       |       |       |       |       |       |       |       |         |       |       |       |       |       |       |       |       |       |       |       |         |       |       |       |       |       |       |       |       |       |       |       |
| 4 hours  | 13.6                        | 17.5  | 19.4     | 22.2  | 24.1  | 25.5  | 29.9  | 34.6  | 37.5  | 41.6  | 45.1  |    |     |     |        |     |     |     |     |     |     |     |     |     |      |      |         |     |     |     |     |     |     |     |      |      |      |      |         |     |     |     |     |     |     |      |      |      |      |      |         |     |     |     |      |      |      |      |      |      |      |      |         |     |      |      |      |      |      |      |      |      |      |      |         |      |      |      |      |      |      |      |      |      |      |      |         |      |      |      |      |      |      |      |      |      |      |      |         |      |      |      |      |      |      |      |      |      |      |      |         |      |      |      |      |      |      |      |      |      |      |      |         |      |      |      |      |      |      |      |      |      |      |      |          |      |      |      |      |      |      |      |      |      |      |      |          |      |      |      |      |      |      |      |      |      |      |      |          |      |      |      |      |      |      |      |      |      |      |      |        |      |      |      |      |      |      |      |      |      |      |      |        |      |      |      |      |      |      |      |      |      |       |       |        |      |      |      |      |      |      |      |      |       |       |       |        |      |      |      |      |      |      |       |       |       |       |       |        |      |      |      |      |       |       |       |       |       |       |       |         |      |      |       |       |       |       |       |       |       |       |       |         |      |       |       |       |       |       |       |       |       |       |       |         |       |       |       |       |       |       |       |       |       |       |       |         |       |       |       |       |       |       |       |       |       |       |       |         |       |       |       |       |       |       |       |       |       |       |       |
| 6 hours  | 16.0                        | 20.4  | 22.6     | 25.8  | 27.9  | 29.4  | 34.3  | 39.5  | 42.8  | 47.3  | 51.1  |    |     |     |        |     |     |     |     |     |     |     |     |     |      |      |         |     |     |     |     |     |     |     |      |      |      |      |         |     |     |     |     |     |     |      |      |      |      |      |         |     |     |     |      |      |      |      |      |      |      |      |         |     |      |      |      |      |      |      |      |      |      |      |         |      |      |      |      |      |      |      |      |      |      |      |         |      |      |      |      |      |      |      |      |      |      |      |         |      |      |      |      |      |      |      |      |      |      |      |         |      |      |      |      |      |      |      |      |      |      |      |         |      |      |      |      |      |      |      |      |      |      |      |          |      |      |      |      |      |      |      |      |      |      |      |          |      |      |      |      |      |      |      |      |      |      |      |          |      |      |      |      |      |      |      |      |      |      |      |        |      |      |      |      |      |      |      |      |      |      |      |        |      |      |      |      |      |      |      |      |      |       |       |        |      |      |      |      |      |      |      |      |       |       |       |        |      |      |      |      |      |      |       |       |       |       |       |        |      |      |      |      |       |       |       |       |       |       |       |         |      |      |       |       |       |       |       |       |       |       |       |         |      |       |       |       |       |       |       |       |       |       |       |         |       |       |       |       |       |       |       |       |       |       |       |         |       |       |       |       |       |       |       |       |       |       |       |         |       |       |       |       |       |       |       |       |       |       |       |
| 9 hours  | 18.8                        | 23.8  | 26.3     | 29.9  | 32.2  | 34.0  | 39.4  | 45.2  | 48.8  | 53.8  | 58.0  |    |     |     |        |     |     |     |     |     |     |     |     |     |      |      |         |     |     |     |     |     |     |     |      |      |      |      |         |     |     |     |     |     |     |      |      |      |      |      |         |     |     |     |      |      |      |      |      |      |      |      |         |     |      |      |      |      |      |      |      |      |      |      |         |      |      |      |      |      |      |      |      |      |      |      |         |      |      |      |      |      |      |      |      |      |      |      |         |      |      |      |      |      |      |      |      |      |      |      |         |      |      |      |      |      |      |      |      |      |      |      |         |      |      |      |      |      |      |      |      |      |      |      |          |      |      |      |      |      |      |      |      |      |      |      |          |      |      |      |      |      |      |      |      |      |      |      |          |      |      |      |      |      |      |      |      |      |      |      |        |      |      |      |      |      |      |      |      |      |      |      |        |      |      |      |      |      |      |      |      |      |       |       |        |      |      |      |      |      |      |      |      |       |       |       |        |      |      |      |      |      |      |       |       |       |       |       |        |      |      |      |      |       |       |       |       |       |       |       |         |      |      |       |       |       |       |       |       |       |       |       |         |      |       |       |       |       |       |       |       |       |       |       |         |       |       |       |       |       |       |       |       |       |       |       |         |       |       |       |       |       |       |       |       |       |       |       |         |       |       |       |       |       |       |       |       |       |       |       |
| 12 hours | 21.1                        | 26.6  | 29.3     | 33.2  | 35.7  | 37.6  | 43.5  | 49.7  | 53.6  | 58.9  | 63.4  |    |     |     |        |     |     |     |     |     |     |     |     |     |      |      |         |     |     |     |     |     |     |     |      |      |      |      |         |     |     |     |     |     |     |      |      |      |      |      |         |     |     |     |      |      |      |      |      |      |      |      |         |     |      |      |      |      |      |      |      |      |      |      |         |      |      |      |      |      |      |      |      |      |      |      |         |      |      |      |      |      |      |      |      |      |      |      |         |      |      |      |      |      |      |      |      |      |      |      |         |      |      |      |      |      |      |      |      |      |      |      |         |      |      |      |      |      |      |      |      |      |      |      |          |      |      |      |      |      |      |      |      |      |      |      |          |      |      |      |      |      |      |      |      |      |      |      |          |      |      |      |      |      |      |      |      |      |      |      |        |      |      |      |      |      |      |      |      |      |      |      |        |      |      |      |      |      |      |      |      |      |       |       |        |      |      |      |      |      |      |      |      |       |       |       |        |      |      |      |      |      |      |       |       |       |       |       |        |      |      |      |      |       |       |       |       |       |       |       |         |      |      |       |       |       |       |       |       |       |       |       |         |      |       |       |       |       |       |       |       |       |       |       |         |       |       |       |       |       |       |       |       |       |       |       |         |       |       |       |       |       |       |       |       |       |       |       |         |       |       |       |       |       |       |       |       |       |       |       |
| 18 hours | 24.9                        | 31.1  | 34.2     | 38.5  | 41.3  | 43.4  | 49.9  | 56.8  | 61.1  | 67.0  | 71.9  |    |     |     |        |     |     |     |     |     |     |     |     |     |      |      |         |     |     |     |     |     |     |     |      |      |      |      |         |     |     |     |     |     |     |      |      |      |      |      |         |     |     |     |      |      |      |      |      |      |      |      |         |     |      |      |      |      |      |      |      |      |      |      |         |      |      |      |      |      |      |      |      |      |      |      |         |      |      |      |      |      |      |      |      |      |      |      |         |      |      |      |      |      |      |      |      |      |      |      |         |      |      |      |      |      |      |      |      |      |      |      |         |      |      |      |      |      |      |      |      |      |      |      |          |      |      |      |      |      |      |      |      |      |      |      |          |      |      |      |      |      |      |      |      |      |      |      |          |      |      |      |      |      |      |      |      |      |      |      |        |      |      |      |      |      |      |      |      |      |      |      |        |      |      |      |      |      |      |      |      |      |       |       |        |      |      |      |      |      |      |      |      |       |       |       |        |      |      |      |      |      |      |       |       |       |       |       |        |      |      |      |      |       |       |       |       |       |       |       |         |      |      |       |       |       |       |       |       |       |       |       |         |      |       |       |       |       |       |       |       |       |       |       |         |       |       |       |       |       |       |       |       |       |       |       |         |       |       |       |       |       |       |       |       |       |       |       |         |       |       |       |       |       |       |       |       |       |       |       |
| 24 hours | 27.9                        | 34.7  | 38.0     | 42.8  | 45.8  | 48.1  | 55.1  | 62.5  | 67.1  | 73.3  | 78.6  |    |     |     |        |     |     |     |     |     |     |     |     |     |      |      |         |     |     |     |     |     |     |     |      |      |      |      |         |     |     |     |     |     |     |      |      |      |      |      |         |     |     |     |      |      |      |      |      |      |      |      |         |     |      |      |      |      |      |      |      |      |      |      |         |      |      |      |      |      |      |      |      |      |      |      |         |      |      |      |      |      |      |      |      |      |      |      |         |      |      |      |      |      |      |      |      |      |      |      |         |      |      |      |      |      |      |      |      |      |      |      |         |      |      |      |      |      |      |      |      |      |      |      |          |      |      |      |      |      |      |      |      |      |      |      |          |      |      |      |      |      |      |      |      |      |      |      |          |      |      |      |      |      |      |      |      |      |      |      |        |      |      |      |      |      |      |      |      |      |      |      |        |      |      |      |      |      |      |      |      |      |       |       |        |      |      |      |      |      |      |      |      |       |       |       |        |      |      |      |      |      |      |       |       |       |       |       |        |      |      |      |      |       |       |       |       |       |       |       |         |      |      |       |       |       |       |       |       |       |       |       |         |      |       |       |       |       |       |       |       |       |       |       |         |       |       |       |       |       |       |       |       |       |       |       |         |       |       |       |       |       |       |       |       |       |       |       |         |       |       |       |       |       |       |       |       |       |       |       |
| 2 days   | 36.3                        | 44.4  | 48.2     | 53.7  | 57.2  | 60.0  | 67.8  | 76.1  | 81.2  | 88.1  | 93.9  |    |     |     |        |     |     |     |     |     |     |     |     |     |      |      |         |     |     |     |     |     |     |     |      |      |      |      |         |     |     |     |     |     |     |      |      |      |      |      |         |     |     |     |      |      |      |      |      |      |      |      |         |     |      |      |      |      |      |      |      |      |      |      |         |      |      |      |      |      |      |      |      |      |      |      |         |      |      |      |      |      |      |      |      |      |      |      |         |      |      |      |      |      |      |      |      |      |      |      |         |      |      |      |      |      |      |      |      |      |      |      |         |      |      |      |      |      |      |      |      |      |      |      |          |      |      |      |      |      |      |      |      |      |      |      |          |      |      |      |      |      |      |      |      |      |      |      |          |      |      |      |      |      |      |      |      |      |      |      |        |      |      |      |      |      |      |      |      |      |      |      |        |      |      |      |      |      |      |      |      |      |       |       |        |      |      |      |      |      |      |      |      |       |       |       |        |      |      |      |      |      |      |       |       |       |       |       |        |      |      |      |      |       |       |       |       |       |       |       |         |      |      |       |       |       |       |       |       |       |       |       |         |      |       |       |       |       |       |       |       |       |       |       |         |       |       |       |       |       |       |       |       |       |       |       |         |       |       |       |       |       |       |       |       |       |       |       |         |       |       |       |       |       |       |       |       |       |       |       |
| 3 days   | 43.5                        | 52.5  | 56.9     | 62.9  | 66.8  | 69.6  | 78.4  | 87.5  | 93.1  | 100.5 | 106.7 |    |     |     |        |     |     |     |     |     |     |     |     |     |      |      |         |     |     |     |     |     |     |     |      |      |      |      |         |     |     |     |     |     |     |      |      |      |      |      |         |     |     |     |      |      |      |      |      |      |      |      |         |     |      |      |      |      |      |      |      |      |      |      |         |      |      |      |      |      |      |      |      |      |      |      |         |      |      |      |      |      |      |      |      |      |      |      |         |      |      |      |      |      |      |      |      |      |      |      |         |      |      |      |      |      |      |      |      |      |      |      |         |      |      |      |      |      |      |      |      |      |      |      |          |      |      |      |      |      |      |      |      |      |      |      |          |      |      |      |      |      |      |      |      |      |      |      |          |      |      |      |      |      |      |      |      |      |      |      |        |      |      |      |      |      |      |      |      |      |      |      |        |      |      |      |      |      |      |      |      |      |       |       |        |      |      |      |      |      |      |      |      |       |       |       |        |      |      |      |      |      |      |       |       |       |       |       |        |      |      |      |      |       |       |       |       |       |       |       |         |      |      |       |       |       |       |       |       |       |       |       |         |      |       |       |       |       |       |       |       |       |       |       |         |       |       |       |       |       |       |       |       |       |       |       |         |       |       |       |       |       |       |       |       |       |       |       |         |       |       |       |       |       |       |       |       |       |       |       |
| 4 days   | 49.9                        | 59.8  | 64.6     | 71.2  | 75.4  | 78.5  | 88.0  | 97.7  | 103.7 | 111.6 | 118.3 |    |     |     |        |     |     |     |     |     |     |     |     |     |      |      |         |     |     |     |     |     |     |     |      |      |      |      |         |     |     |     |     |     |     |      |      |      |      |      |         |     |     |     |      |      |      |      |      |      |      |      |         |     |      |      |      |      |      |      |      |      |      |      |         |      |      |      |      |      |      |      |      |      |      |      |         |      |      |      |      |      |      |      |      |      |      |      |         |      |      |      |      |      |      |      |      |      |      |      |         |      |      |      |      |      |      |      |      |      |      |      |         |      |      |      |      |      |      |      |      |      |      |      |          |      |      |      |      |      |      |      |      |      |      |      |          |      |      |      |      |      |      |      |      |      |      |      |          |      |      |      |      |      |      |      |      |      |      |      |        |      |      |      |      |      |      |      |      |      |      |      |        |      |      |      |      |      |      |      |      |      |       |       |        |      |      |      |      |      |      |      |      |       |       |       |        |      |      |      |      |      |      |       |       |       |       |       |        |      |      |      |      |       |       |       |       |       |       |       |         |      |      |       |       |       |       |       |       |       |       |       |         |      |       |       |       |       |       |       |       |       |       |       |         |       |       |       |       |       |       |       |       |       |       |       |         |       |       |       |       |       |       |       |       |       |       |       |         |       |       |       |       |       |       |       |       |       |       |       |
| 6 days   | 61.7                        | 73.1  | 78.6     | 86.1  | 90.9  | 94.4  | 105.1 | 116.0 | 122.7 | 131.5 | 138.8 |    |     |     |        |     |     |     |     |     |     |     |     |     |      |      |         |     |     |     |     |     |     |     |      |      |      |      |         |     |     |     |     |     |     |      |      |      |      |      |         |     |     |     |      |      |      |      |      |      |      |      |         |     |      |      |      |      |      |      |      |      |      |      |         |      |      |      |      |      |      |      |      |      |      |      |         |      |      |      |      |      |      |      |      |      |      |      |         |      |      |      |      |      |      |      |      |      |      |      |         |      |      |      |      |      |      |      |      |      |      |      |         |      |      |      |      |      |      |      |      |      |      |      |          |      |      |      |      |      |      |      |      |      |      |      |          |      |      |      |      |      |      |      |      |      |      |      |          |      |      |      |      |      |      |      |      |      |      |      |        |      |      |      |      |      |      |      |      |      |      |      |        |      |      |      |      |      |      |      |      |      |       |       |        |      |      |      |      |      |      |      |      |       |       |       |        |      |      |      |      |      |      |       |       |       |       |       |        |      |      |      |      |       |       |       |       |       |       |       |         |      |      |       |       |       |       |       |       |       |       |       |         |      |       |       |       |       |       |       |       |       |       |       |         |       |       |       |       |       |       |       |       |       |       |       |         |       |       |       |       |       |       |       |       |       |       |       |         |       |       |       |       |       |       |       |       |       |       |       |
| 8 days   | 72.4                        | 85.2  | 91.3     | 99.7  | 104.9 | 108.8 | 120.5 | 132.5 | 139.8 | 149.3 | 157.3 |    |     |     |        |     |     |     |     |     |     |     |     |     |      |      |         |     |     |     |     |     |     |     |      |      |      |      |         |     |     |     |     |     |     |      |      |      |      |      |         |     |     |     |      |      |      |      |      |      |      |      |         |     |      |      |      |      |      |      |      |      |      |      |         |      |      |      |      |      |      |      |      |      |      |      |         |      |      |      |      |      |      |      |      |      |      |      |         |      |      |      |      |      |      |      |      |      |      |      |         |      |      |      |      |      |      |      |      |      |      |      |         |      |      |      |      |      |      |      |      |      |      |      |          |      |      |      |      |      |      |      |      |      |      |      |          |      |      |      |      |      |      |      |      |      |      |      |          |      |      |      |      |      |      |      |      |      |      |      |        |      |      |      |      |      |      |      |      |      |      |      |        |      |      |      |      |      |      |      |      |      |       |       |        |      |      |      |      |      |      |      |      |       |       |       |        |      |      |      |      |      |      |       |       |       |       |       |        |      |      |      |      |       |       |       |       |       |       |       |         |      |      |       |       |       |       |       |       |       |       |       |         |      |       |       |       |       |       |       |       |       |       |       |         |       |       |       |       |       |       |       |       |       |       |       |         |       |       |       |       |       |       |       |       |       |       |       |         |       |       |       |       |       |       |       |       |       |       |       |
| 10 days  | 82.6                        | 96.6  | 103.2    | 112.3 | 118.0 | 122.3 | 135.0 | 147.8 | 155.7 | 165.9 | 174.5 |    |     |     |        |     |     |     |     |     |     |     |     |     |      |      |         |     |     |     |     |     |     |     |      |      |      |      |         |     |     |     |     |     |     |      |      |      |      |      |         |     |     |     |      |      |      |      |      |      |      |      |         |     |      |      |      |      |      |      |      |      |      |      |         |      |      |      |      |      |      |      |      |      |      |      |         |      |      |      |      |      |      |      |      |      |      |      |         |      |      |      |      |      |      |      |      |      |      |      |         |      |      |      |      |      |      |      |      |      |      |      |         |      |      |      |      |      |      |      |      |      |      |      |          |      |      |      |      |      |      |      |      |      |      |      |          |      |      |      |      |      |      |      |      |      |      |      |          |      |      |      |      |      |      |      |      |      |      |      |        |      |      |      |      |      |      |      |      |      |      |      |        |      |      |      |      |      |      |      |      |      |       |       |        |      |      |      |      |      |      |      |      |       |       |       |        |      |      |      |      |      |      |       |       |       |       |       |        |      |      |      |      |       |       |       |       |       |       |       |         |      |      |       |       |       |       |       |       |       |       |       |         |      |       |       |       |       |       |       |       |       |       |       |         |       |       |       |       |       |       |       |       |       |       |       |         |       |       |       |       |       |       |       |       |       |       |       |         |       |       |       |       |       |       |       |       |       |       |       |
| 12 days  | 92.3                        | 107.5   | 114.6    | 124.4 | 130.5 | 135.0 | 148.6 | 162.4 | 170.7 | 181.6 | 190.7 |    |     |     |        |     |     |     |     |     |     |     |     |     |      |      |         |     |     |     |     |     |     |     |      |      |      |      |         |     |     |     |     |     |     |      |      |      |      |      |         |     |     |     |      |      |      |      |      |      |      |      |         |     |      |      |      |      |      |      |      |      |      |      |         |      |      |      |      |      |      |      |      |      |      |      |         |      |      |      |      |      |      |      |      |      |      |      |         |      |      |      |      |      |      |      |      |      |      |      |         |      |      |      |      |      |      |      |      |      |      |      |         |      |      |      |      |      |      |      |      |      |      |      |          |      |      |      |      |      |      |      |      |      |      |      |          |      |      |      |      |      |      |      |      |      |      |      |          |      |      |      |      |      |      |      |      |      |      |      |        |      |      |      |      |      |      |      |      |      |      |      |        |      |      |      |      |      |      |      |      |      |       |       |        |      |      |      |      |      |      |      |      |       |       |       |        |      |      |      |      |      |      |       |       |       |       |       |        |      |      |      |      |       |       |       |       |       |       |       |         |      |      |       |       |       |       |       |       |       |       |       |         |      |       |       |       |       |       |       |       |       |       |       |         |       |       |       |       |       |       |       |       |       |       |       |         |       |       |       |       |       |       |       |       |       |       |       |         |       |       |       |       |       |       |       |       |       |       |       |
| 16 days  | 110.9                       | 128.1   | 136.2    | 147.3 | 154.1 | 159.2 | 174.4 | 189.7 | 198.9 | 211.0 | 221.0 |    |     |     |        |     |     |     |     |     |     |     |     |     |      |      |         |     |     |     |     |     |     |     |      |      |      |      |         |     |     |     |     |     |     |      |      |      |      |      |         |     |     |     |      |      |      |      |      |      |      |      |         |     |      |      |      |      |      |      |      |      |      |      |         |      |      |      |      |      |      |      |      |      |      |      |         |      |      |      |      |      |      |      |      |      |      |      |         |      |      |      |      |      |      |      |      |      |      |      |         |      |      |      |      |      |      |      |      |      |      |      |         |      |      |      |      |      |      |      |      |      |      |      |          |      |      |      |      |      |      |      |      |      |      |      |          |      |      |      |      |      |      |      |      |      |      |      |          |      |      |      |      |      |      |      |      |      |      |      |        |      |      |      |      |      |      |      |      |      |      |      |        |      |      |      |      |      |      |      |      |      |       |       |        |      |      |      |      |      |      |      |      |       |       |       |        |      |      |      |      |      |      |       |       |       |       |       |        |      |      |      |      |       |       |       |       |       |       |       |         |      |      |       |       |       |       |       |       |       |       |       |         |      |       |       |       |       |       |       |       |       |       |       |         |       |       |       |       |       |       |       |       |       |       |       |         |       |       |       |       |       |       |       |       |       |       |       |         |       |       |       |       |       |       |       |       |       |       |       |
| 20 days  | 128.6                       | 147.8   | 156.8    | 168.9 | 176.5 | 182.0 | 198.7 | 215.4 | 225.4 | 238.5 | 249.4 |    |     |     |        |     |     |     |     |     |     |     |     |     |      |      |         |     |     |     |     |     |     |     |      |      |      |      |         |     |     |     |     |     |     |      |      |      |      |      |         |     |     |     |      |      |      |      |      |      |      |      |         |     |      |      |      |      |      |      |      |      |      |      |         |      |      |      |      |      |      |      |      |      |      |      |         |      |      |      |      |      |      |      |      |      |      |      |         |      |      |      |      |      |      |      |      |      |      |      |         |      |      |      |      |      |      |      |      |      |      |      |         |      |      |      |      |      |      |      |      |      |      |      |          |      |      |      |      |      |      |      |      |      |      |      |          |      |      |      |      |      |      |      |      |      |      |      |          |      |      |      |      |      |      |      |      |      |      |      |        |      |      |      |      |      |      |      |      |      |      |      |        |      |      |      |      |      |      |      |      |      |       |       |        |      |      |      |      |      |      |      |      |       |       |       |        |      |      |      |      |      |      |       |       |       |       |       |        |      |      |      |      |       |       |       |       |       |       |       |         |      |      |       |       |       |       |       |       |       |       |       |         |      |       |       |       |       |       |       |       |       |       |       |         |       |       |       |       |       |       |       |       |       |       |       |         |       |       |       |       |       |       |       |       |       |       |       |         |       |       |       |       |       |       |       |       |       |       |       |
| 25 days  | 150.1                       | 171.5   | 181.4    | 194.9 | 203.2 | 209.3 | 227.6 | 245.9 | 256.9 | 271.2 | 283.0 |    |     |     |        |     |     |     |     |     |     |     |     |     |      |      |         |     |     |     |     |     |     |     |      |      |      |      |         |     |     |     |     |     |     |      |      |      |      |      |         |     |     |     |      |      |      |      |      |      |      |      |         |     |      |      |      |      |      |      |      |      |      |      |         |      |      |      |      |      |      |      |      |      |      |      |         |      |      |      |      |      |      |      |      |      |      |      |         |      |      |      |      |      |      |      |      |      |      |      |         |      |      |      |      |      |      |      |      |      |      |      |         |      |      |      |      |      |      |      |      |      |      |      |          |      |      |      |      |      |      |      |      |      |      |      |          |      |      |      |      |      |      |      |      |      |      |      |          |      |      |      |      |      |      |      |      |      |      |      |        |      |      |      |      |      |      |      |      |      |      |      |        |      |      |      |      |      |      |      |      |      |       |       |        |      |      |      |      |      |      |      |      |       |       |       |        |      |      |      |      |      |      |       |       |       |       |       |        |      |      |      |      |       |       |       |       |       |       |       |         |      |      |       |       |       |       |       |       |       |       |       |         |      |       |       |       |       |       |       |       |       |       |       |         |       |       |       |       |       |       |       |       |       |       |       |         |       |       |       |       |       |       |       |       |       |       |       |         |       |       |       |       |       |       |       |       |       |       |       |
| 5.       | Global time of entry        | 5 mins  |          |       |       |       |       |       |       |       |       |    |     |     |        |     |     |     |     |     |     |     |     |     |      |      |         |     |     |     |     |     |     |     |      |      |      |      |         |     |     |     |     |     |     |      |      |      |      |      |         |     |     |     |      |      |      |      |      |      |      |      |         |     |      |      |      |      |      |      |      |      |      |      |         |      |      |      |      |      |      |      |      |      |      |      |         |      |      |      |      |      |      |      |      |      |      |      |         |      |      |      |      |      |      |      |      |      |      |      |         |      |      |      |      |      |      |      |      |      |      |      |         |      |      |      |      |      |      |      |      |      |      |      |          |      |      |      |      |      |      |      |      |      |      |      |          |      |      |      |      |      |      |      |      |      |      |      |          |      |      |      |      |      |      |      |      |      |      |      |        |      |      |      |      |      |      |      |      |      |      |      |        |      |      |      |      |      |      |      |      |      |       |       |        |      |      |      |      |      |      |      |      |       |       |       |        |      |      |      |      |      |      |       |       |       |       |       |        |      |      |      |      |       |       |       |       |       |       |       |         |      |      |       |       |       |       |       |       |       |       |       |         |      |       |       |       |       |       |       |       |       |       |       |         |       |       |       |       |       |       |       |       |       |       |       |         |       |       |       |       |       |       |       |       |       |       |       |         |       |       |       |       |       |       |       |       |       |       |       |
| 6.       | Maximum rainfall            | 250 mm/hr   |          |       |       |       |       |       |       |       |       |    |     |     |        |     |     |     |     |     |     |     |     |     |      |      |         |     |     |     |     |     |     |     |      |      |      |      |         |     |     |     |     |     |     |      |      |      |      |      |         |     |     |     |      |      |      |      |      |      |      |      |         |     |      |      |      |      |      |      |      |      |      |      |         |      |      |      |      |      |      |      |      |      |      |      |         |      |      |      |      |      |      |      |      |      |      |      |         |      |      |      |      |      |      |      |      |      |      |      |         |      |      |      |      |      |      |      |      |      |      |      |         |      |      |      |      |      |      |      |      |      |      |      |          |      |      |      |      |      |      |      |      |      |      |      |          |      |      |      |      |      |      |      |      |      |      |      |          |      |      |      |      |      |      |      |      |      |      |      |        |      |      |      |      |      |      |      |      |      |      |      |        |      |      |      |      |      |      |      |      |      |       |       |        |      |      |      |      |      |      |      |      |       |       |       |        |      |      |      |      |      |      |       |       |       |       |       |        |      |      |      |      |       |       |       |       |       |       |       |         |      |      |       |       |       |       |       |       |       |       |       |         |      |       |       |       |       |       |       |       |       |       |       |         |       |       |       |       |       |       |       |       |       |       |       |         |       |       |       |       |       |       |       |       |       |       |       |         |       |       |       |       |       |       |       |       |       |       |       |
| 7.       | Minimum Velocity            | 1.00 m/s (Clause 6.5.1 Table 6.4, GSDSDS-new-development)   |          |       |       |       |       |       |       |       |       |    |     |     |        |     |     |     |     |     |     |     |     |     |      |      |         |     |     |     |     |     |     |     |      |      |      |      |         |     |     |     |     |     |     |      |      |      |      |      |         |     |     |     |      |      |      |      |      |      |      |      |         |     |      |      |      |      |      |      |      |      |      |      |         |      |      |      |      |      |      |      |      |      |      |      |         |      |      |      |      |      |      |      |      |      |      |      |         |      |      |      |      |      |      |      |      |      |      |      |         |      |      |      |      |      |      |      |      |      |      |      |         |      |      |      |      |      |      |      |      |      |      |      |          |      |      |      |      |      |      |      |      |      |      |      |          |      |      |      |      |      |      |      |      |      |      |      |          |      |      |      |      |      |      |      |      |      |      |      |        |      |      |      |      |      |      |      |      |      |      |      |        |      |      |      |      |      |      |      |      |      |       |       |        |      |      |      |      |      |      |      |      |       |       |       |        |      |      |      |      |      |      |       |       |       |       |       |        |      |      |      |      |       |       |       |       |       |       |       |         |      |      |       |       |       |       |       |       |       |       |       |         |      |       |       |       |       |       |       |       |       |       |       |         |       |       |       |       |       |       |       |       |       |       |       |         |       |       |       |       |       |       |       |       |       |       |       |         |       |       |       |       |       |       |       |       |       |       |       |
| 8.       | Maximum Velocity            | 3.00 m/s  |          |       |       |       |       |       |       |       |       |    |     |     |        |     |     |     |     |     |     |     |     |     |      |      |         |     |     |     |     |     |     |     |      |      |      |      |         |     |     |     |     |     |     |      |      |      |      |      |         |     |     |     |      |      |      |      |      |      |      |      |         |     |      |      |      |      |      |      |      |      |      |      |         |      |      |      |      |      |      |      |      |      |      |      |         |      |      |      |      |      |      |      |      |      |      |      |         |      |      |      |      |      |      |      |      |      |      |      |         |      |      |      |      |      |      |      |      |      |      |      |         |      |      |      |      |      |      |      |      |      |      |      |          |      |      |      |      |      |      |      |      |      |      |      |          |      |      |      |      |      |      |      |      |      |      |      |          |      |      |      |      |      |      |      |      |      |      |      |        |      |      |      |      |      |      |      |      |      |      |      |        |      |      |      |      |      |      |      |      |      |       |       |        |      |      |      |      |      |      |      |      |       |       |       |        |      |      |      |      |      |      |       |       |       |       |       |        |      |      |      |      |       |       |       |       |       |       |       |         |      |      |       |       |       |       |       |       |       |       |       |         |      |       |       |       |       |       |       |       |       |       |       |         |       |       |       |       |       |       |       |       |       |       |       |         |       |       |       |       |       |       |       |       |       |       |       |         |       |       |       |       |       |       |       |       |       |       |       |
| 9.       | Minimum Pipe Diameter       | 225 mm (Clause 11.4, GSDSDS-code-of-practice-for-drainage-works)  |          |       |       |       |       |       |       |       |       |    |     |     |        |     |     |     |     |     |     |     |     |     |      |      |         |     |     |     |     |     |     |     |      |      |      |      |         |     |     |     |     |     |     |      |      |      |      |      |         |     |     |     |      |      |      |      |      |      |      |      |         |     |      |      |      |      |      |      |      |      |      |      |         |      |      |      |      |      |      |      |      |      |      |      |         |      |      |      |      |      |      |      |      |      |      |      |         |      |      |      |      |      |      |      |      |      |      |      |         |      |      |      |      |      |      |      |      |      |      |      |         |      |      |      |      |      |      |      |      |      |      |      |          |      |      |      |      |      |      |      |      |      |      |      |          |      |      |      |      |      |      |      |      |      |      |      |          |      |      |      |      |      |      |      |      |      |      |      |        |      |      |      |      |      |      |      |      |      |      |      |        |      |      |      |      |      |      |      |      |      |       |       |        |      |      |      |      |      |      |      |      |       |       |       |        |      |      |      |      |      |      |       |       |       |       |       |        |      |      |      |      |       |       |       |       |       |       |       |         |      |      |       |       |       |       |       |       |       |       |       |         |      |       |       |       |       |       |       |       |       |       |       |         |       |       |       |       |       |       |       |       |       |       |       |         |       |       |       |       |       |       |       |       |       |       |       |         |       |       |       |       |       |       |       |       |       |       |       |
| 10.      | Pipe diameter               | 225 mm, 300 mm, 375 mm, 450 mm, 525 mm, 600 mm  |          |       |       |       |       |       |       |       |       |    |     |     |        |     |     |     |     |     |     |     |     |     |      |      |         |     |     |     |     |     |     |     |      |      |      |      |         |     |     |     |     |     |     |      |      |      |      |      |         |     |     |     |      |      |      |      |      |      |      |      |         |     |      |      |      |      |      |      |      |      |      |      |         |      |      |      |      |      |      |      |      |      |      |      |         |      |      |      |      |      |      |      |      |      |      |      |         |      |      |      |      |      |      |      |      |      |      |      |         |      |      |      |      |      |      |      |      |      |      |      |         |      |      |      |      |      |      |      |      |      |      |      |          |      |      |      |      |      |      |      |      |      |      |      |          |      |      |      |      |      |      |      |      |      |      |      |          |      |      |      |      |      |      |      |      |      |      |      |        |      |      |      |      |      |      |      |      |      |      |      |        |      |      |      |      |      |      |      |      |      |       |       |        |      |      |      |      |      |      |      |      |       |       |       |        |      |      |      |      |      |      |       |       |       |       |       |        |      |      |      |      |       |       |       |       |       |       |       |         |      |      |       |       |       |       |       |       |       |       |       |         |      |       |       |       |       |       |       |       |       |       |       |         |       |       |       |       |       |       |       |       |       |       |       |         |       |       |       |       |       |       |       |       |       |       |       |         |       |       |       |       |       |       |       |       |       |       |       |
| 11.      | Minimum cover depth of pipe | 0.6m in fields and open spaces<br><br>0.9m below lightly trafficked areas<br><br>1.2m (If that cannot be achieved, the pipes shall be fully surrounded in 150mm thick concrete with an absolute   |          |       |       |       |       |       |       |       |       |    |     |     |        |     |     |     |     |     |     |     |     |     |      |      |         |     |     |     |     |     |     |     |      |      |      |      |         |     |     |     |     |     |     |      |      |      |      |      |         |     |     |     |      |      |      |      |      |      |      |      |         |     |      |      |      |      |      |      |      |      |      |      |         |      |      |      |      |      |      |      |      |      |      |      |         |      |      |      |      |      |      |      |      |      |      |      |         |      |      |      |      |      |      |      |      |      |      |      |         |      |      |      |      |      |      |      |      |      |      |      |         |      |      |      |      |      |      |      |      |      |      |      |          |      |      |      |      |      |      |      |      |      |      |      |          |      |      |      |      |      |      |      |      |      |      |      |          |      |      |      |      |      |      |      |      |      |      |      |        |      |      |      |      |      |      |      |      |      |      |      |        |      |      |      |      |      |      |      |      |      |       |       |        |      |      |      |      |      |      |      |      |       |       |       |        |      |      |      |      |      |      |       |       |       |       |       |        |      |      |      |      |       |       |       |       |       |       |       |         |      |      |       |       |       |       |       |       |       |       |       |         |      |       |       |       |       |       |       |       |       |       |       |         |       |       |       |       |       |       |       |       |       |       |       |         |       |       |       |       |       |       |       |       |       |       |       |         |       |       |       |       |       |       |       |       |       |       |       |



## BASELINE

|                          |  |  |
|--------------------------|--|--|
|                          |  | minimum depth of cover of 750mm) (Clause 11.8.2, GDSDS-code-of-practice-for-drainage-works)  |
| 12.                      | Chamber Diameter   | Technical Design Guidelines Part H – Table 9<br>Type J – 1200mm (Depth of pipe is over 1.5m) |
| 13.                      | Colebrook white pipe roughness coefficients for carrier drains | Ks=0.600 (Clause 6.5.1 Table 6.4, GDSDS-new-development)                                     |
| 14.                      | Colebrook white pipe roughness coefficients for filter drains  | 1.500  |
| 15.                      | Manning's 'n' for ditch and swale (If applicable)              | 0.045 to 0.050   |
| 16.                      | Minimum design gradient for ditch and swale                    | 0.2% (1/500) to ensure flow conveyance in flat areas   |
| 17.                      | Minimum design gradient for pipes                              | 1/500 (Such that the velocity is not less than 1.00 m/s)                                     |
| 18.                      | Maximum design gradient for pipes                              | Slope such that velocity of 3.0 m/s is not exceeded  |
| 19.                      | MADD factor  | 0 m <sup>3</sup> /ha   |
| <b>Percentage Runoff</b> |  |  |
| 1.                       | Carriageways   | 1.00 (100% of impermeable area)  |
| 2.                       | Green fields and open spaces                                   | 0.15 (15% of impermeable area)   |
| 3.                       | Concrete   | 0.95 (95% of impermeable area)   |
| 4.                       | Gravel   | 0.30 (30% of impermeable area)   |
| <b>Soakaway</b>          |  |  |
| 1.                       | Drainage Stone Porosity  | 0.30   |
| 2.                       | Infiltration coefficient                                       | 0.2196 m/hr  |
| 3.                       | Infiltration depth   | 2.4m   |
| 4.                       | Porosity of the soakaway                                       | 0.95 (95%) (Modelled as Geocellular soakaway)  |

**Table 4-2 - Storm Drainage Design Parameters**



QBar calculations are not required as all storm water will be contained within the site and discharged to ground water. The storm sewer design calculations are presented in Appendix C

## 4.2.2 Temporary stormwater management

During construction, and until the permanent infiltration pond and hydrocarbon separators are operational, a temporary infiltration lagoon will be provided. The lagoon will be sized for the 1-in-10-year, 24-hour storm event and lined with permeable geotextile, filter aggregates, and sand to remove suspended solids before infiltration to groundwater. Surface water runoff generated during construction will be pumped to this lagoon for controlled infiltration.

## 4.3 Contaminated Firewater

Due to EPA licensing requirements, the site must collect all potentially contaminated firewater produced during a fire and store it for later disposal off-site by tankers. Typically these are high risk areas including buildings and generators/turbines etc. Roads with no buildings and grassed areas do not require to be included. The storage tanks must be sized to accommodate 2 hours of firefighting plus the runoff from a 10-year, 24-hour storm.

According to UK National guidance on water provision for firefighting, an industrial site exceeding 3 hectares should be capable of supplying 75 litres per second. Since Uisce Éireann cannot supply this volume, a static firefighting tank with a capacity of 540 cubic meters will be installed giving an allowance of 75 litres per second for 2 hours. This tank will also be combined with the service water tank with a final total volume of 1480 cu.m which includes the 540 cu.m.

To manage the contaminated firewater tank, which is also based on the 10-year, 24-hour storm runoff, it is proposed to divide the storm network into multiple individual areas. Each area will have a pH-controlled actuator valve. In the event of a fire, the firewater from the affected area will be diverted to the firewater tanks using these actuator valves, while any rainfall during the fire in other areas will continue to flow unimpeded to the soakaway pond northeast of the site. This division into separate areas helps reduce the size of the contaminated firewater storage tanks.

The maximum calculated runoff for the 10-year, 24-hour storm is 197 cubic meters, meaning the total storage tank size required will be  $540 + 197 = 737$  cubic meters. The contaminated firewater will be disposed of off-site by tanker to a suitable external wastewater treatment facility.

The tank will also dual use as a storage tank for rejected water during the production of demineralised water. As such the tank will have an additional 350 cu.m to store this rejected water making the total volume of the tank 1087 cu.m.

## 4.4 Demineralised water production wastewater

As part of the plant's turbine operation requirements, demineralised water is necessary. This water is injected into the turbine either for power augmentation when using gas or to reduce NOx gases when running on fuel oil. In both cases, the injected water vaporizes and exits the turbine through the stack.

To produce the demineralised water, an onsite treatment plant will convert potable water supplied by Uisce Éireann into demineralised water, which will be stored in a tank until needed. The process of creating and filling the tank with demineralised water takes several weeks.

The conversion process is expected to be approximately 75% efficient, meaning that 25% of the water used will be rejected as heavily mineralised waste water. This waste water will be stored in an above ground tank in the short term and moved to the underground contaminated firewater tank in the long term as required and removed off-site as required to a wastewater treatment plant for disposal by a licensed contractor.



## 4.5 Generator/Turbine solvent clean down disposal

Routine maintenance of the turbine involves cleaning the machine with solvents. These solvents are injected internally and drain down for collection beneath the machine. The collection system is closed and discharges all solvents to an underground tank, from where they are collected by tanker and disposed of off-site at a licensed facility capable of handling hydrocarbon waste. It is anticipated that this maintenance will occur several times a year, generating no more than 2 cubic meters of waste hydrocarbons each time.

## 4.6 Potable Water

It is proposed to supply the site with potable water via a new 150mm diameter water main which will come from Athenry (approx. 2km) and be installed by Uisce Éireann to the site entrance on the L3103 as outlined in the Confirmation of Feasibility. The water demand calculations are contained within the pre-connection enquiry to Uisce Éireann which is presented in Appendix E along with the Confirmation of Feasibility.

All new water mains will be designed and installed in accordance with Uisce Éireann Code of Practice and standard details.

The proposed watermain drawings are submitted as part of the S37E planning application.

A pre-connection enquiry has been submitted to Uisce Éireann for consideration and Confirmation of Feasibility received under reference number CDS25000940 (see appendix E of this report).



## 5. Roads and surfaces

The proposed roads within the peaker plant itself are proposed to be kerbed asphalt roads. It is proposed that the standard buildup will be (Roads outside the plant will be unkerbed):

- 40mm SMA surf (IS EM 13108-5)
- 60mm AC 20 Dense Bin (IS EN 13108-1)
- 120mm AC 32 Dense Base (IS EN 13108-1)
- 150mm Type B Granular Material
- 600mm Type 6F2 Capping

The concrete paved areas surrounding the generator are proposed to be:

- 300mm C32/40 concrete (Suitable exposure class) A393 mesh T&B
- 150 Type B Granular Material
- 600mm Type 6F2 capping

Concrete Areas in the tank farm are to be

- 200mm C32/40 concrete (Suitable exposure class) A393 mesh T&B
- 150 Type B granular material
- 600mm Type 6F2 capping

Gravel areas are to be gravel topping on soil lined with impermeable membrane underneath with a series of land drains to collect infiltrated runoff and discharge to soakaway via petrol interceptor.

- 100mm pea gravel/shingle
- Separation membrane
- 300mm soil with 100mm perforate land drain @ 5m c/c
- Impermeable membrane

Footpaths

- 100mm concrete
- 150mm type B granular material



## 5.1 Parking

A review of the Galway County Development Plan was undertaken to assess parking requirements for the proposed development. While the Plan does not specify a parking rate for developments of this particular type, it does provide guidance for industrial, manufacturing, and light industrial uses. According to Table 15.5 under Development Management Standard 31, the requirement is 1 parking space per 33 m<sup>2</sup> of floor area. Based on an estimated total floor area of approximately 2,053 m<sup>2</sup>, this would equate to a requirement of 62 parking spaces.

The proposed development is a power station, which is likely to be classified as industrial. However, the facility is designed to operate remotely, with only a minimal on-site presence consisting primarily of security personnel. It is anticipated that no more than 10 individuals will be present on-site at any given time.

If the development were to be classified similarly to a data centre—based on its low occupancy—the parking requirement would be reduced to approximately 20.5 spaces. The current project includes provision for 19 parking bays, comprising 1 accessible bay, 4 EV charging bays, and 14 standard bays of which 4 will be provided as part of a substation subject of a future planning application to An Coimisiún Pleanála, along with 20 bicycle stands.

Parking provision has been determined based on the expected operational characteristics of the site. While the facility will be remotely operated for the majority of its lifecycle, it will require parking for both security and maintenance personnel. Although the exact number of vehicles associated with these functions cannot be precisely determined, the site is expected to accommodate up to 2 security vehicles and 10 maintenance vehicles during peak activity.

# 6. Cut and fill

It is proposed to cut and fill the site as presented in Table 6-1. The cut and fill has been calculated on a comparison of the final grade levels compared to the initial grade levels from the topographic survey.

| SURFACE LEVEL DATA |               |               |   |      |
|--------------------|---------------|---------------|---|------|
| NUMBER             | MINIMUM LEVEL | MAXIMUM LEVEL | COLOUR                                    |      |
| 1                  | -2.50         | -2.00         | <span style="color: red;">■</span>        | CUT  |
| 2                  | -2.00         | -1.50         | <span style="color: darkred;">■</span>    |      |
| 3                  | -1.50         | -1.00         | <span style="color: brown;">■</span>      |      |
| 4                  | -1.00         | -0.50         | <span style="color: darkbrown;">■</span>  |      |
| 5                  | -0.50         | 0.00          | <span style="color: black;">■</span>      |      |
| 6                  | 0.00          | 0.50          | <span style="color: darkgreen;">■</span>  | FILL |
| 7                  | 0.50          | 1.00          | <span style="color: green;">■</span>      |      |
| 8                  | 1.00          | 1.50          | <span style="color: lightgreen;">■</span> |      |

The maximum depth excavated in the overall cut and fill is 2.5m. This is the level cut down to in the rough site grading. There will be an initial topsoil strip of the site which is approximately 150mm deep over the entire site.

The deepest excavation on the site will be the storage tank for the contaminated firewater which will be excavated to a depth of 47.495m AoD.

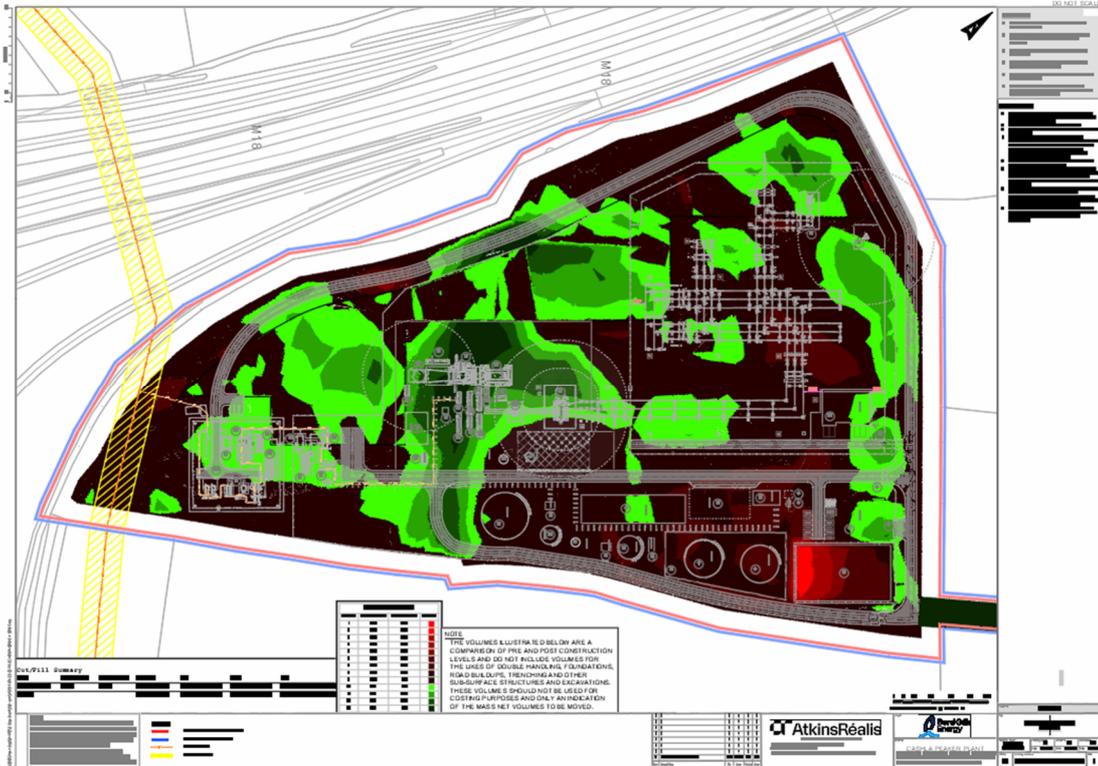


Table 6-1 - Cut and Fill Heat Map



|               | Cut (cu.m) | Fill (cu.m) | Net (cu.m)      |
|---------------|------------|-------------|-----------------|
| Topsoil Strip | 10,698.00  | 0.00        | 10,698.00 (cut) |
| Volume (c     | 22,345.00  | 20533.00    | 1,812.00 (cut)  |

**Table 6-2 - Cut and Fill Volumes**

In addition to this the following high level volumes should be considered and incorporated

| Construction Item                      | Associated Volume (cu.m) |
|--|--------------------------|
| Roads imported materials               | 8,150                    |
| Concrete slabs imported materials      | 10,450                   |
| Building foundation imported materials | 10,450                   |
| Gravel areas imported materials        | 5,217                    |

**Table 6-3 - Imported Materials**

It is anticipated that ca. 13,000 m3 of excess subsoil (topsoil, native soil) will require offsite disposal. All such material will be removed and disposed of offsite to a suitably permitted / licenced waste recovery / disposal facility in accordance with relevant waste management legislation (including but not limited to the Waste Management Act of 1996 (as amended) and all subsequent waste management regulations as amended.



## 7. Traffic

The description of traffic and management of for the project is described in Chapter 10 of the EIAR as well as the Construction Traffic Management Plan. The reader is referred to those documents for a complete description.



## 8. Electrical

### 8.1 220kV Substation

The proposed project will involve construction of a 220 kV AIS 2-bay extendable to 4-bay substation compliant with EirGrid standards. As set out in Section 2.2 Project Description, the 220kV AIS substation and associated 220kV grid connection works will be subject of a S182B planning application to An Coimisiún Pleanála. Ownership of the substation will be transferred to EirGrid/ESB following construction. All substation works will be contained within the boundary of the proposed site.

The proposed substation will comprise:

- 1No. control building housing control and protection panels, telecoms, batteries, 1No. diesel generator and welfare facilities.
- 1No. telecommunications mast.
- 220 kV air insulated equipment including cables sealing ends, circuit breakers, disconnectors, surge arresters, current and voltage transformers, post insulators and associated busbars.
- 2.4m high palisade fencing and 1.4m high post & rail fencing, gates and access tracks, car-parking, lightning masts, lamp posts and CCTV.
- 1No. reactor

A customer owned compound connecting to the EirGrid/ESB owned substation via overhead busbars is also proposed consisting of:

- 1No. Electrical control building
- 1No. 220 kV power transformer with associated concrete bund and blast wall
- 1No. auxiliary transformer
- 220 kV air insulated equipment including circuit breakers, disconnectors, surge arresters, current and voltage transformers, post insulators and associated isolated phase busduct.
- Security fencing, gates and access tracks, lightning masts, lamp posts and CCTV.

### 8.2 Grid Connection

It is proposed to connect the 220 kV substation to the existing ESB 220kV Cashla substation via approximately 8.1km of underground cable (UGC). The grid connection, which will be subject to a future planning application to ACP, will comprise a single 220 kV circuit with three 200mm HDPE power cable ducts and two 125mm HDPE comms ducts installed in an open-cut trench, typically 700mm wide and 1425mm deep. The depth of the trench may vary depending on service crossings and the final design.



## BASELINE

The majority of the Grid Connection is located within public roadways as shown in Figure 8-1, with precast cable joint bays and associated link box and comms chambers at approximately 760m to 900m intervals. There will be short sections of the UGC route located off-road for navigating into termination points at either end of the line.

The Grid Connection will also include trenchless installation in the form of horizontal directional drilling (HDD) at the proposed locations:

- Motorway (M17) crossing in townland of Castlambert, converging onto road L3103
- Motorway (M6) crossing in townland of Caherbriskaun, converging onto road L-7108-28
- Motorway (M6) crossing in townland of Lisheenkyle East, converging onto road L7109

The UGC will also need to cross a Gas Networks Ireland (GNI) high pressure gas transmission pipeline along the L-7108-28. The crossing will be designed and built in accordance with GNI Code of Practice.



**Figure 8-1 – Proposed Grid Connection UGC Route**

A full set of drawings and documents relating to the cable route are included in the submission from TLI.

## 9. Mechanical

The Cashla Peaker Plant shall generate electricity for grid transmission using a single open cycle gas turbine and generator.

The turbine shall be equipped with an inlet air filtration system which will filter out any airborne particles. The inlet system shall also include noise silencers to minimize the noise from the turbine inlet. The turbine shall exhaust via an exhaust inline noise silencer to a vertical exhaust stack. The stack dimensions shall be sufficiently specified to ensure external air emissions shall remain within statutory air quality limits.

The turbine shall primarily combust natural gas fuel supplied from the national gas transmission network. The combustion process within the turbine shall control the polluting emissions to within the European 2010/75/EU Directive emission limits using a dry low NOx combustion process. Low sulphur diesel shall be used as a secondary fuel when the turbine is required to support the electrical grid and there is insufficient natural gas available. Low sulphur diesel combustion polluting emissions shall be controlled by a combination of a low NOx combustion system enhanced as required with demineralized water injection, and use of low sulphur fuel. Low sulphur diesel combustion emission limits shall be controlled within the European BREF Large Combustion Plant Best Available Techniques limits for fuels used for less than 500 hours per year.

The turbine and generator shall be supported by various auxiliary equipment for fuel supply, cooling, lubrication and cleaning purposes.

The fuel system includes a propane tank to supply propane gas for combustion ignition purposes when starting the turbine using low sulphur diesel.

### 9.1 Tank Farm

The plant is required to store a specified quantity of secondary fuel, in this case low sulphur diesel, to comply with the electrical transmission system's Grid Code. This fuel will be stored in two steel cylindrical fuel tanks contained within a sealed concrete bunded area to ensure any potential leakage is controlled and prevented from being released. The bund is sufficiently sized to accommodate 110% of each fuel tank volume and will be 2.5m high.

The combustion of low sulphur diesel requires injection of demineralised water into the turbine's combustion system to control emissions to the required levels. The volume of demineralised water stored is in direct relationship to the storage volume of low sulphur diesel.

A quantity of the water supplied to the site is stored as service water. The service water tank supplies all the water systems on site including the raw supply to the demineralised water system. It also serves as a break tank from the external potable water supply system. The service water volume is included in a combined fire and service water tank with a volume of 1480 cu.m.

### 9.2 Gas Fuel

Gas will be supplied from the high pressure national transmission pipeline system. The gas will be conditioned prior to supply to the gas turbine combustion control system. This conditioning will consist of filtration, heating, pressure control and removal of any liquid condensate. The system will also include a motor driven gas compressor in the event the supplied gas pressure falls below the minimum required for the gas turbine system.



## 9.3 Low sulphur diesel System

The low sulphur diesel system shall include motor driven pumps to offload the fuel oil from the supply tankers to the two storage tanks. The system shall also include motor driven pumps, filters and coalescer to supply the fuel to the gas turbine combustion system in a suitable condition.

## 9.4 Lubricating Oil

An auxiliary lubricating oil skid including a storage tank and associated pumps circulate lubricating oil to the gas turbine and generator.

## 9.5 Diesel Generator

An emergency diesel engine driven generator provides power to safely shut down the plant in the event the normal electrical transmission grid connection is not available. Other than routine start-up testing, the diesel generator shall rarely be operated.

## 9.6 Fire System

The fire system comprises a fire water tank, fire water distribution system with associated hydrants and spray nozzles, motor driven supply and jockey pumps and an emergency diesel driven pump.

## 9.7 Demineralised Water System

Demineralised water is primarily required for water injection into the turbine. The potable water supply to the site is required to be demineralised to avoid mineral deposits on the turbine combustion system and blading which would degrade their integrity. The potable water will be demineralised using a containerised water treatment system suitable for the chemical make-up of the water. This treatment system is expected to consist of either a reverse osmosis system or ion exchange system.

The demineralised water system will include motor driven pumps to pump the water through the water treatment system and to and from the demineralised water storage tank.



# 10. Gas AGI

A gas AGI designed by Gas Networks Ireland (GNI) is shown in the planning drawings. At this stage it is envisioned that the access to the AGI will be through the main site access to the north as illustrated in Figure 10-1. It is assumed that in general traffic to the AGI from the south will be light commercial vehicles such as vans. The AGI will be owned and operated by GNI and will not form part of the IED License for the Peaker Plant. Additional gas processing equipment is illustrated within the Peaker Plant north of the AGI to raise the temperature of the supplied gas to the temperature required by the turbine.

The GNI146 Rathmorrissy gas pipeline does not form part of the proposed development subject of the SID planning application but will be subject to a Section 39A Consent under the Gas Act 1976, as amended.

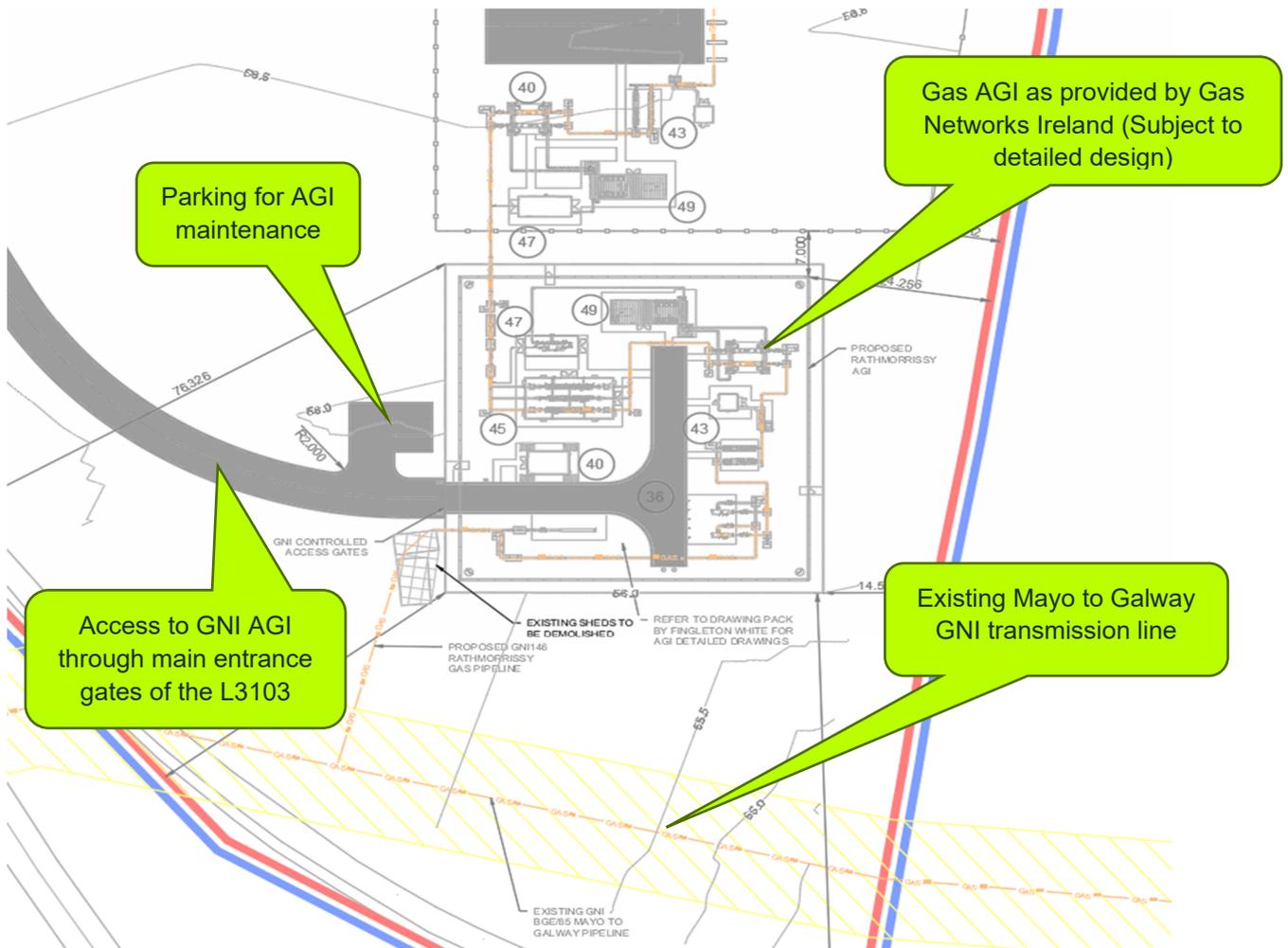


Figure 10-1 - Snip from drawing DR-CE-900031 showing access to gas AGI

The gas AGI will contain storm drainage which will discharge to a local soak pit within the AGI. As part of the controls to protect groundwater a Class 1 bypass hydrocarbon separator will be fitted prior to discharge to ground.

Drawings are included in the drawing pack from Gas Networks Ireland submitted as part of the S37E planning application drawing pack. Details on the operation of the AGI are set out in Chapter 2 Project Description of the EIAR.



# 11. Abnormal Load

## 11.1 Abnormal Load - Introduction

This section outlines the transportation requirements and constraints associated with delivering major equipment components to the project site. Equipment will arrive either as large standalone units or as smaller assemblies integrated into pre-assembled, skid-mounted systems.

The primary large-scale components include:

- Gas turbine
- Electrical generator
- Grid transformer

It is anticipated that three abnormal load movements will be required, each exceeding 280 tonnes. These movements will be scheduled over several months to align with the delivery timelines of individual equipment packages.

The following assessments have been undertaken:

- Auto-tracking from port to site
- Topographical survey to identify geometric constraints
- Structural assessment of bridges and culverts along proposed routes
- Pavement capacity analysis

The following reports have been produced:

- Abnormal Load Assessment Report
- Haulage Routes Pavement Analysis – Technical Note

The conclusions of these reports are summarized in this section. The final haul route will be agreed prior to the delivery of extraordinary or abnormal loads, which may occur several months after on-site construction begins. Pre- and post-construction surveys of the public road network proposed for use as haul routes—including inspections of bridges, culverts, and other relevant structures—shall be carried out by the applicant before any phase involving abnormal load movements. These requirements do not apply to earlier phases without such movements. The scope and locations of these surveys shall be agreed in advance with Galway County Council Roads Authority and include structural capacity assessments where required.



## 11.2 Abnormal Load - Delivery Road map

Equipment will arrive either as large standalone components or as smaller units integrated into skid-mounted systems. To facilitate transportation, major components will be partially disassembled, with removable parts shipped separately to reduce size and weight.

### Disassembly Details:

- **Gas Turbine:** Shipped without enclosure, external fuel piping, and auxiliary systems (e.g., compressor bleed valves, ventilation fans).
- **Electrical Generator:** External cooling systems and auxiliary connections removed.
- **Transformer:** Insulated bushings and external oil tank detached; oil drained and unit sealed with dry gas for transport.

Following disassembly, the heaviest single component weighs approximately 380 tonnes. Transport height is constrained by the lowest bridge clearance along the designated route. Three abnormal load movements are expected, each exceeding 280 tonnes, scheduled over several months.

## 11.3 Extraordinary Abnormal Load Details

### 11.3.1 Proposed Loads

There are three proposed Extraordinary Abnormal Loads (EAL's) to be delivered to the project site. These loads are detailed below:

| Component           | Weight (t) | Length (mm) | Width (mm) | Height (mm) |
|---------------------|------------|-------------|------------|-------------|
| Turbine             | 360        | 12,000      | 5,500      | 5,020       |
| Generator           | 380        | 14,000      | 4,250      | 4,850       |
| Step up Transformer | 288        | 11,300      | 4,730      | 4,750       |

Table 11-1 - Extraordinary Abnormal Loads (EAL's) to be delivered to site

### 11.3.2 Proposed delivery routes

Two initial routes were identified from Galway Port to the project site in Pollinagroagh, Athenry, Co. Galway (red and blue routes). Both share a common section (yellow). After assessment, the red route was discounted due to inadequate bridge capacity. The blue route is therefore the preferred option.



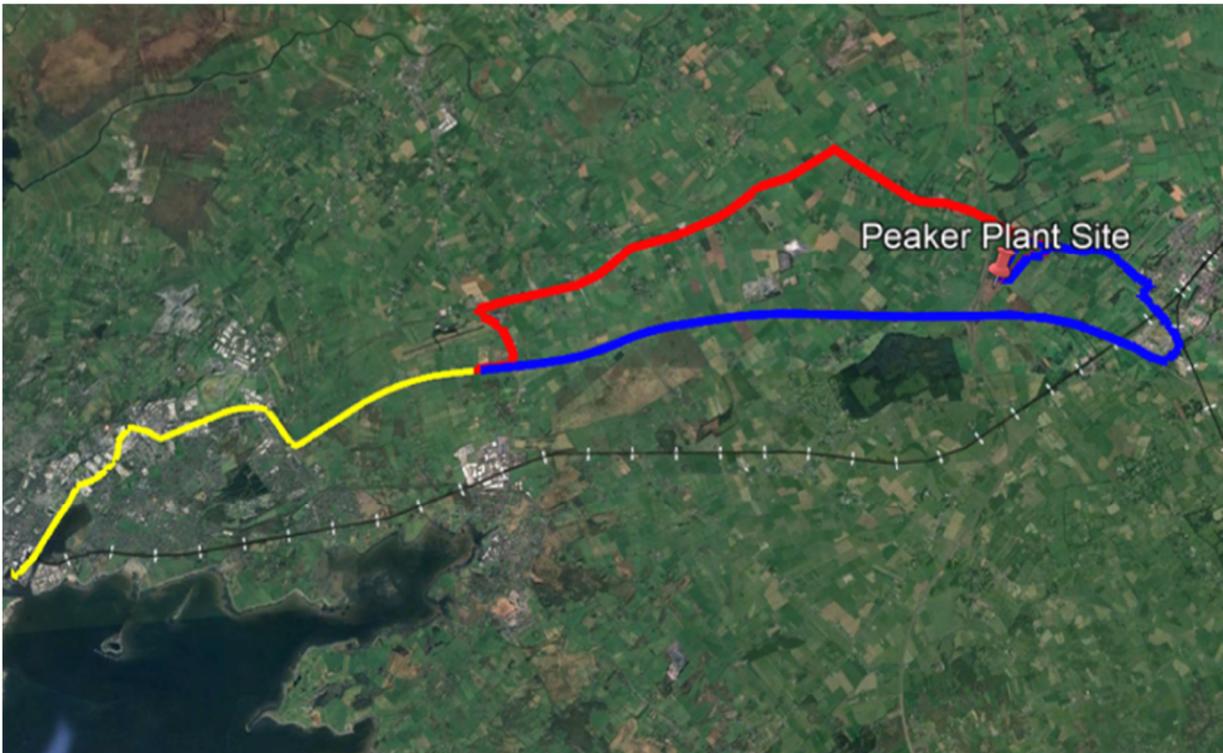


Figure 11-1 - Proposed delivery routes assessed (red route discounted)

### 11.3.3 Common yellow route

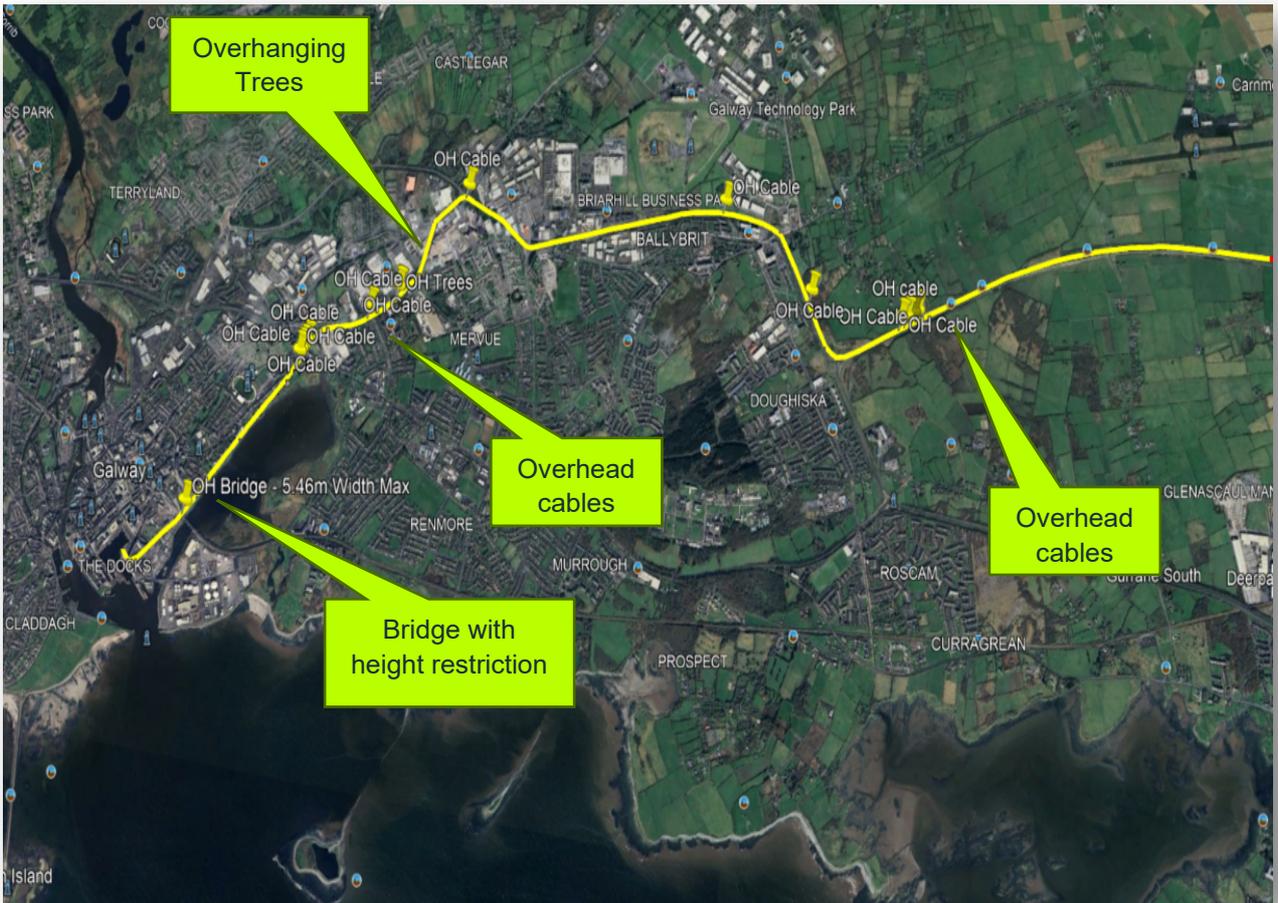


Figure 11-2 - Common route with restrictions identified



### 11.3.4 Red route with restrictions identified

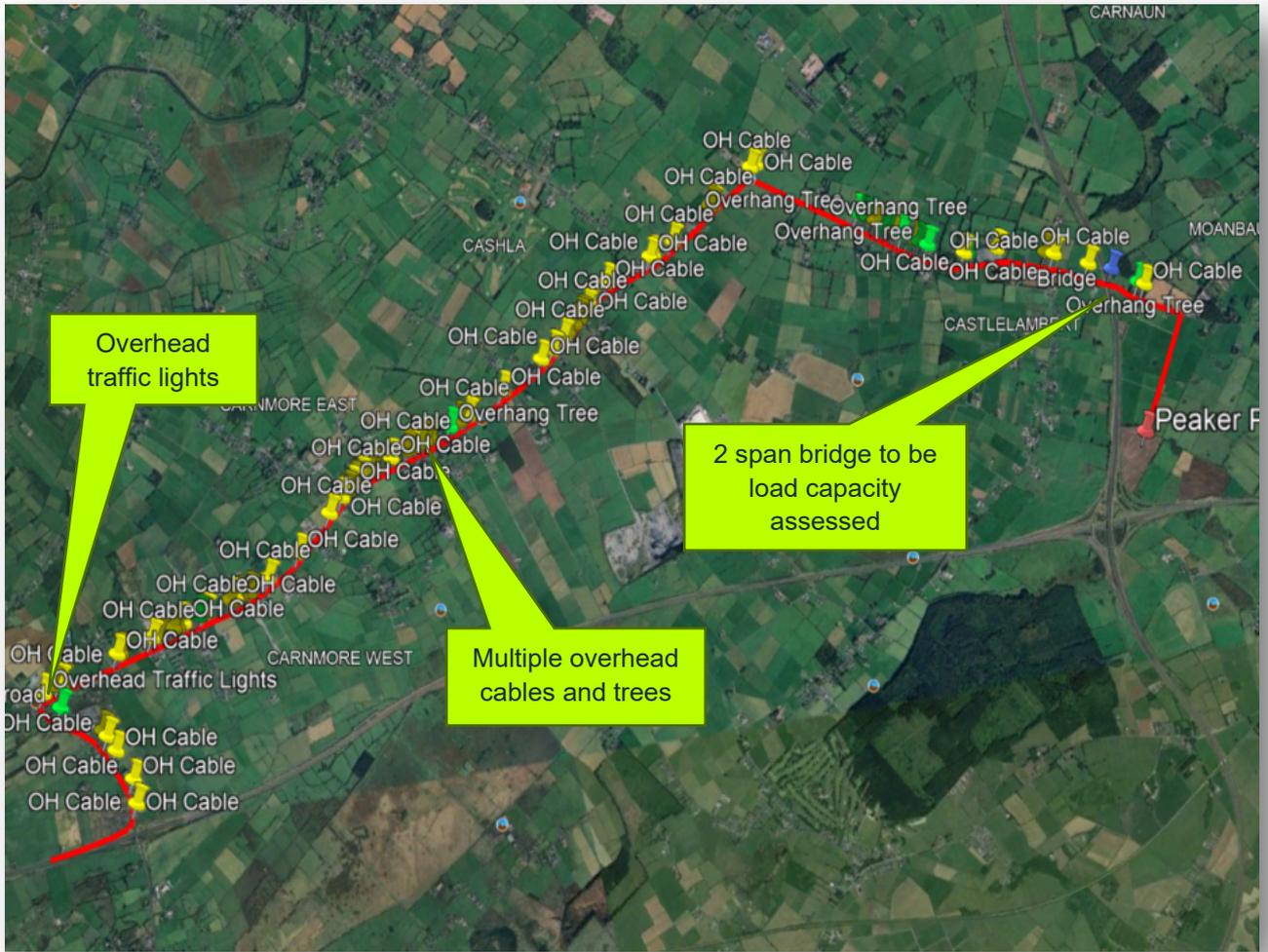


Figure 11-3 - Red route with restrictions identified

### 11.3.5 Blue route with restrictions identified

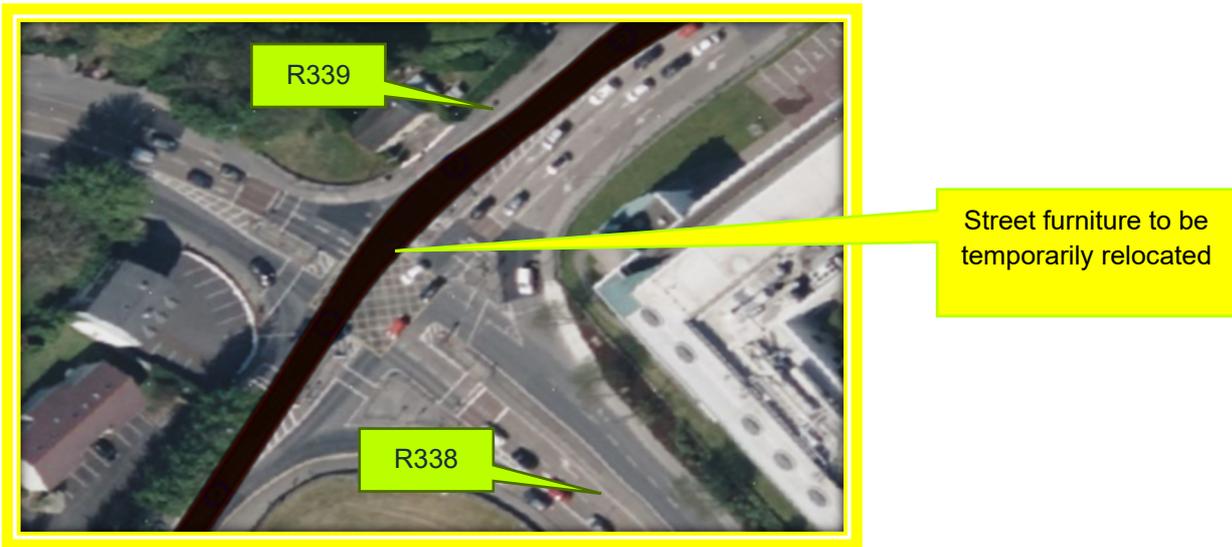


Figure 11-4 - Blue route with restrictions identified

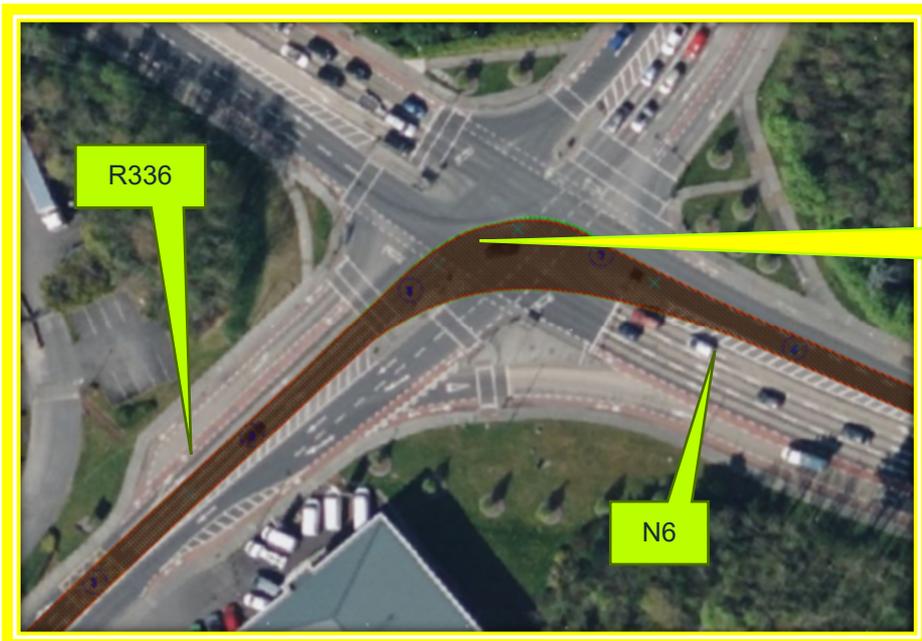
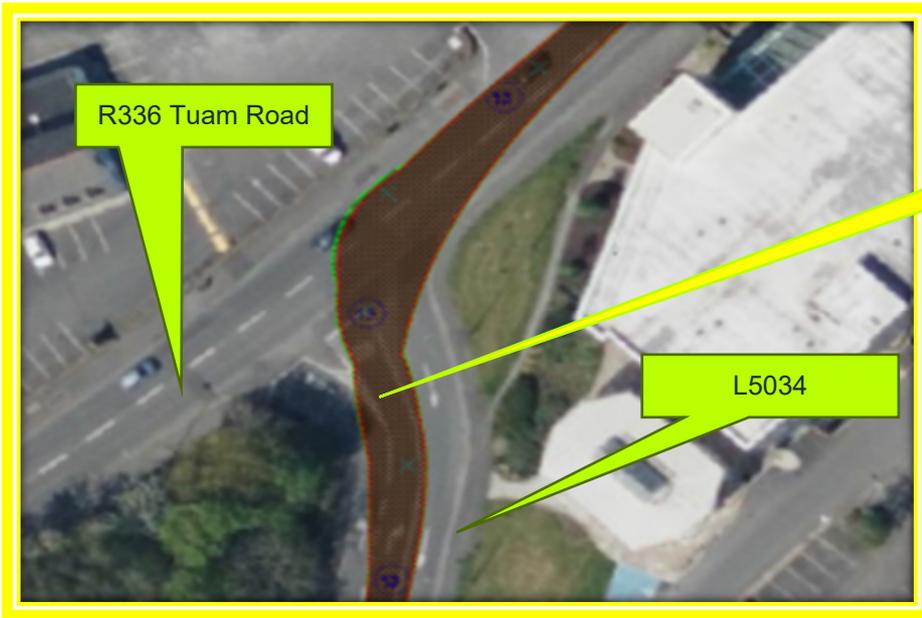


# 11.4 Auto tracking

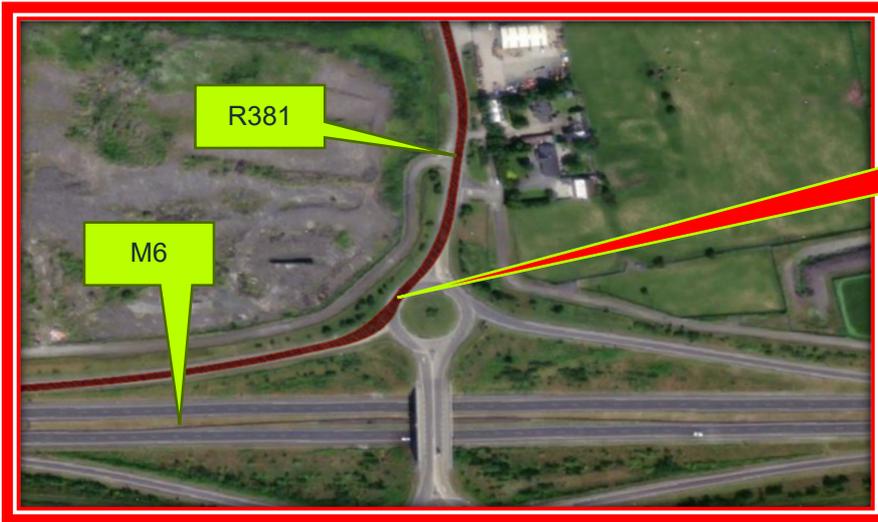
## 11.4.1 Yellow (common) route



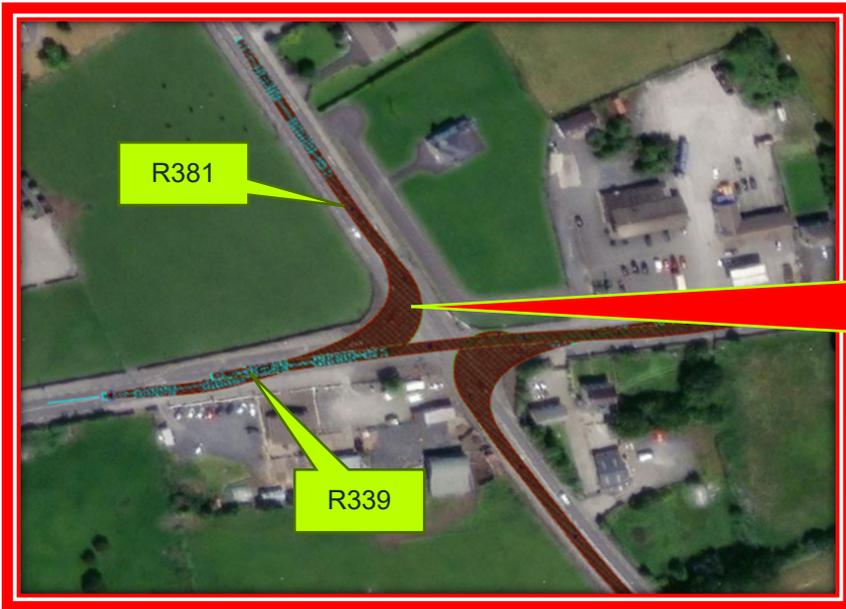
BASELINE



### 11.4.2 Red Route (discounted)

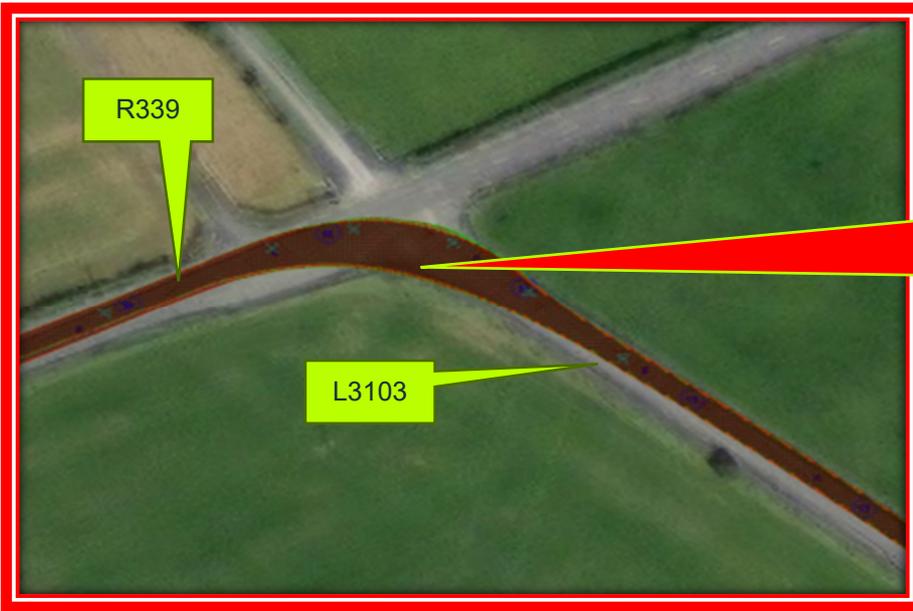


No additional Works required in the roundabout



Temporary road closure for public to facilitate the mobilisation of truck. Alternative route to be proposed to avoid traffic congestion.





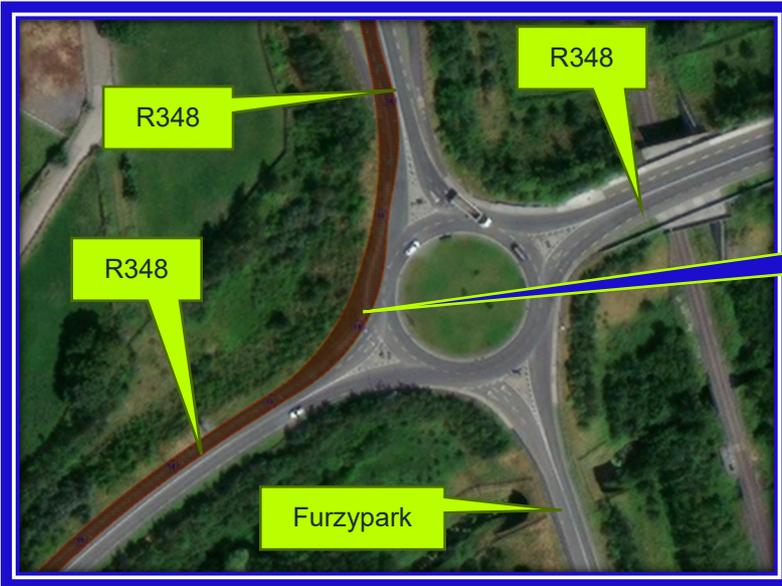
Overturn of Truck on the adjacent green spaces. Temporary track to be created to facilitate truck movements. Need approval from the land owner.

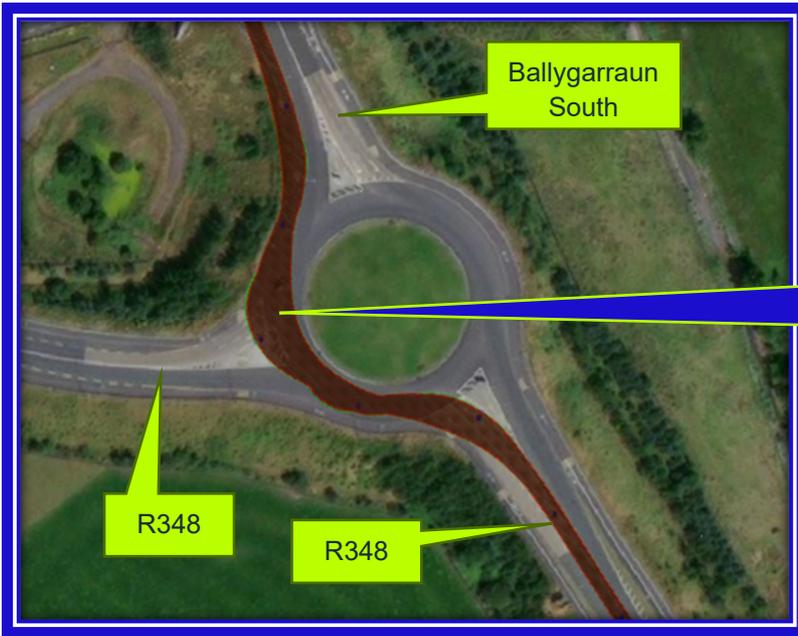


Temporary road to be constructed to facilitate delivery to the site.



### 11.4.3 Blue Route





Overrun of Truck on the island. Temporary track/works to be laid/carried out, to facilitate free flow of the truck



Reverse in the roundabout may be required. Temporary diversion of traffic may be needed. Temporary works to roundabout required



## 11.5 Bridges Assessment Along the Routes

Included within this submission is an Abnormal Load Assessment Report which has been commissioned by Bord Gáis Energy to confirm that the equipment up to 380 tonnes can be safely transported from Galway Port to the Cashla Peaker Plant using EAL vehicles. A summary of the report is provided below.

**Routes Considered:** Blue and red routes (with shared sections).

**Structures Assessed:** 20 identified; 9 key bridges and culverts analyzed in detail.

### Methodology:

- Review of drawings and inspection reports
- Computer modeling of structural response under heavy loads
- Conservative assumptions applied where data was incomplete
- Comparison of expected stresses with original design capacities

### Findings:

- All structures on the blue route passed safety checks.
- One structure on the red route (Castlelambert Overbridge) failed—overstressed under proposed loads.
- Conclusion: Blue route approved; red route unsuitable.

### Conditions for Safe Transport:

- Vehicle speed  $\leq 10$  mph
- Use of slow lane
- No other traffic on bridge during crossing

### Recommendations:

- Pre- and post-movement inspections for all bridges
- Confirm axle loads and spacing with haulier
- No further structural checks required for blue route

## 11.6 Pavement Assessment

A Level 1 and Level 2 FWD analysis is included within this submission. Within the analysis, IAPDM structural review concluded that pavement structures along the proposed route have sufficient residual capacity for anticipated loading. The cumulative demand ( $\sim 0.02$  MSA for 3 loads, 4 passes) is well below residual pavement life. No strengthening works are required, provided standard traffic management and operational controls are implemented.



## 11.7 Conclusion

EAL delivery planning involves multiple interconnected elements that require close coordination among stakeholders. As the project progresses and new information becomes available, timelines and deliverables may be adjusted. These changes are a result of project complexity rather than any lack of assessment.

### Current Position:

- The **Blue route** is confirmed as suitable for abnormal load transport.
- The **Red route** is viable up to a limit of 275t but not all loads would be suitable for this route.

Final confirmation of the haul route will occur prior to EAL delivery, which may take place several months after construction begins. Pre- and post-construction surveys of the public road network—including bridges, culverts, and other relevant structures—will be undertaken by the applicant before any abnormal load movements. The scope and locations of these surveys will be agreed in advance with Galway County Council Roads Authority.

BASELINE

# APPENDICES

# Appendix A. Utility Record Maps





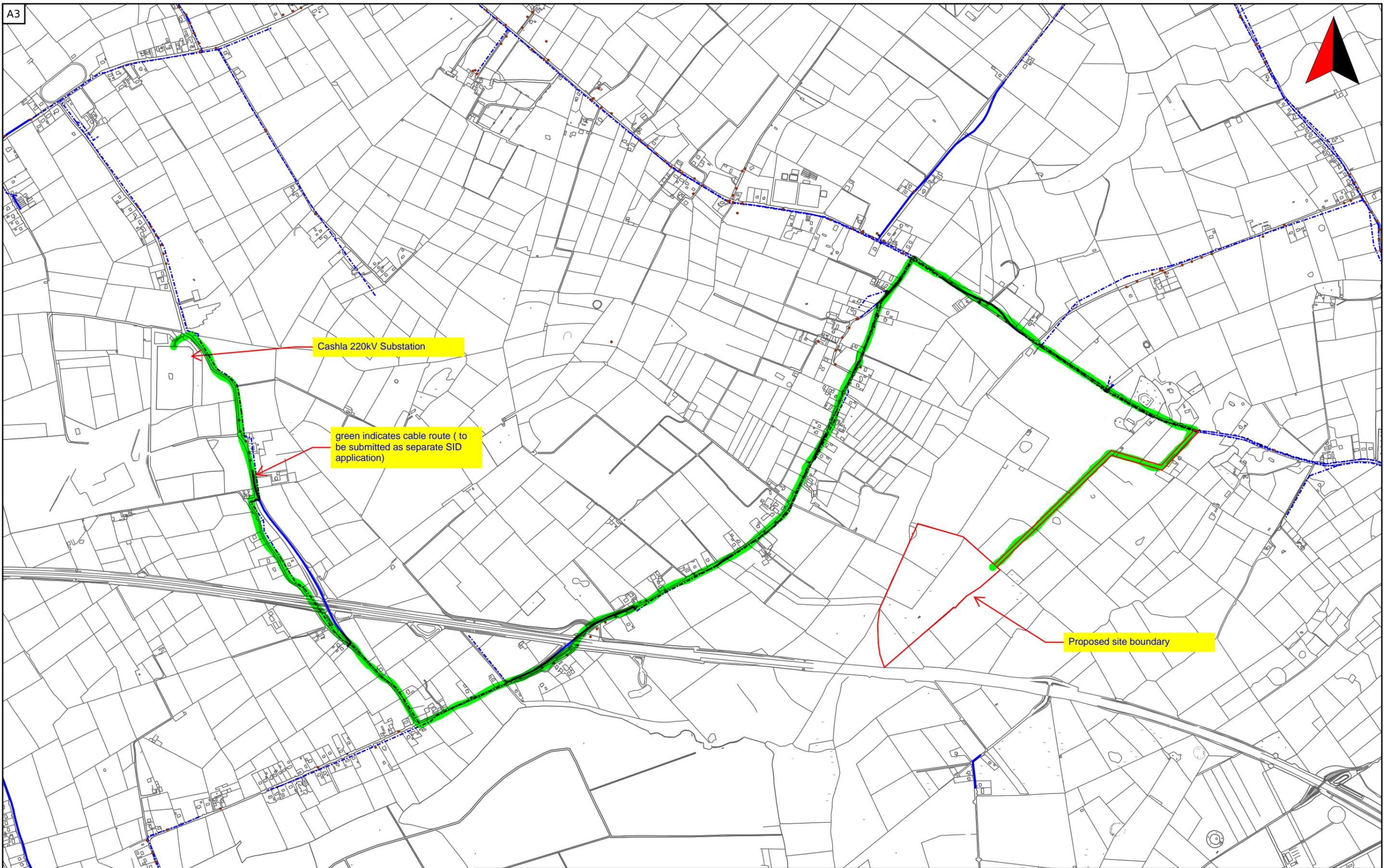










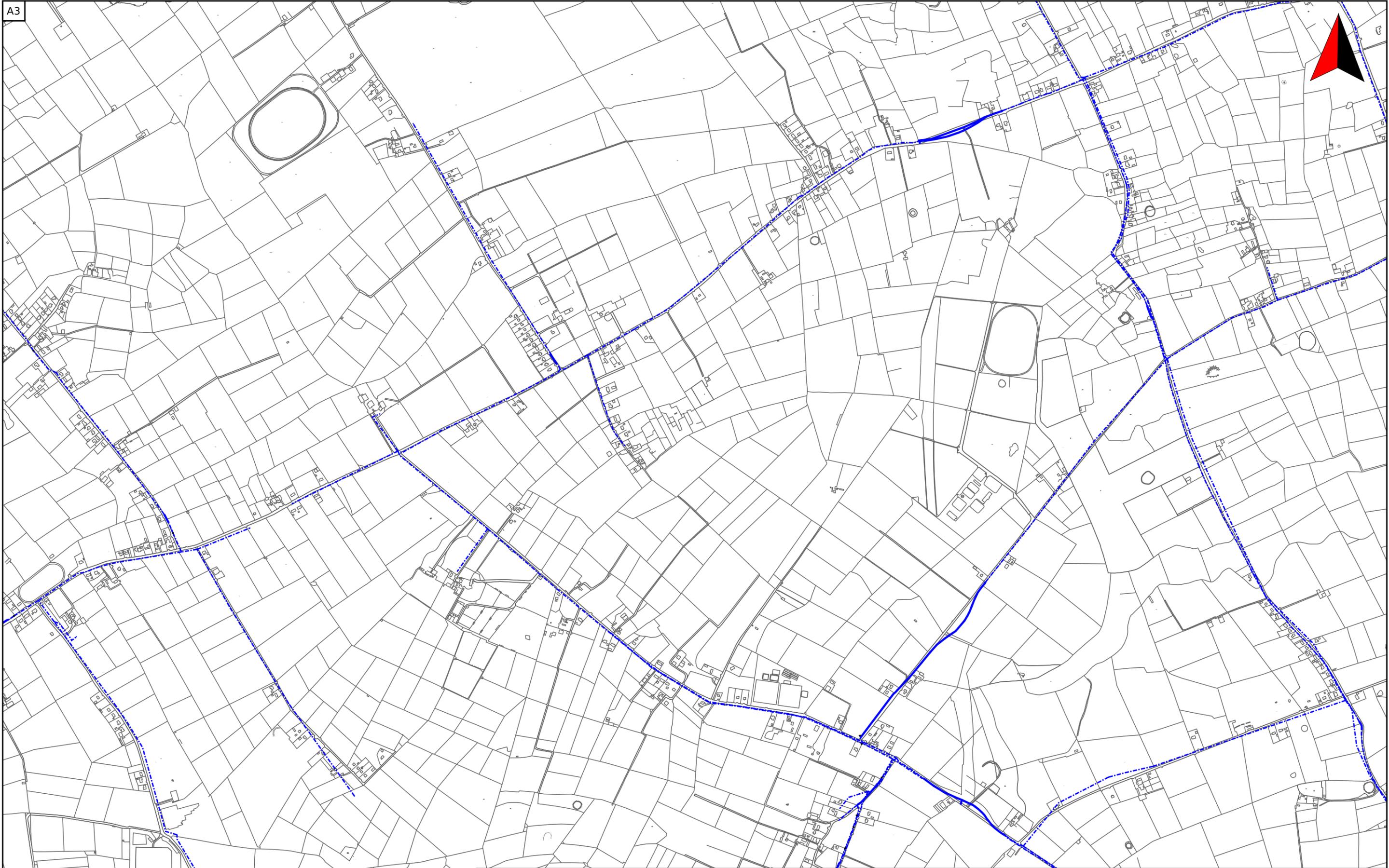


Cashla 220kV Substation

green indicates cable route ( to be submitted as separate SID application)

Proposed site boundary

|   |  |   |   |
|---|--|---|---|
| <b>open eir Civil Engineering Infrastructure Service</b>  |  | Scale:<br>1:15000   | Irish National Grid<br>Centre XY: 545413 m,<br>728546 m |
|   |  | Date<br>02/12/2025  | Smallworld<br>Powered by GE                             |
| <p>THE INFORMATION IN THIS DRAWING IS CONFIDENTIAL AND SHOULD NOT BE DISCLOSED TO ANY THIRD PARTY WITHOUT THE EXPRESS WRITTEN CONSENT OF open eir. THE DRAWING MAY NOT BE PHOTOCOPIED OR REPRODUCED IN ANY WAY.</p>   |  | <p>THE INFORMATION GIVEN IS COMPILED FROM PASSIVE ACCESS RECORDS AND IS BELIEVED TO BE CORRECT. THERE MAY, HOWEVER, BE DEPARTURES FROM THE COURSE(S) AND DEPTH(S) SHOWN OR INDICATED. THERE MAY ALSO BE ITEMS OF open eir INFRASTRUCTURE OF WHICH NO RECORDS IS HELD. THE INFORMATION IS GIVEN WITHOUT PREJUDICE TO THE LEGAL RIGHTS OF open eir TO COMPENSATION SHOULD open eir INFRASTRUCTURE BE DAMAGED.</p> |   |
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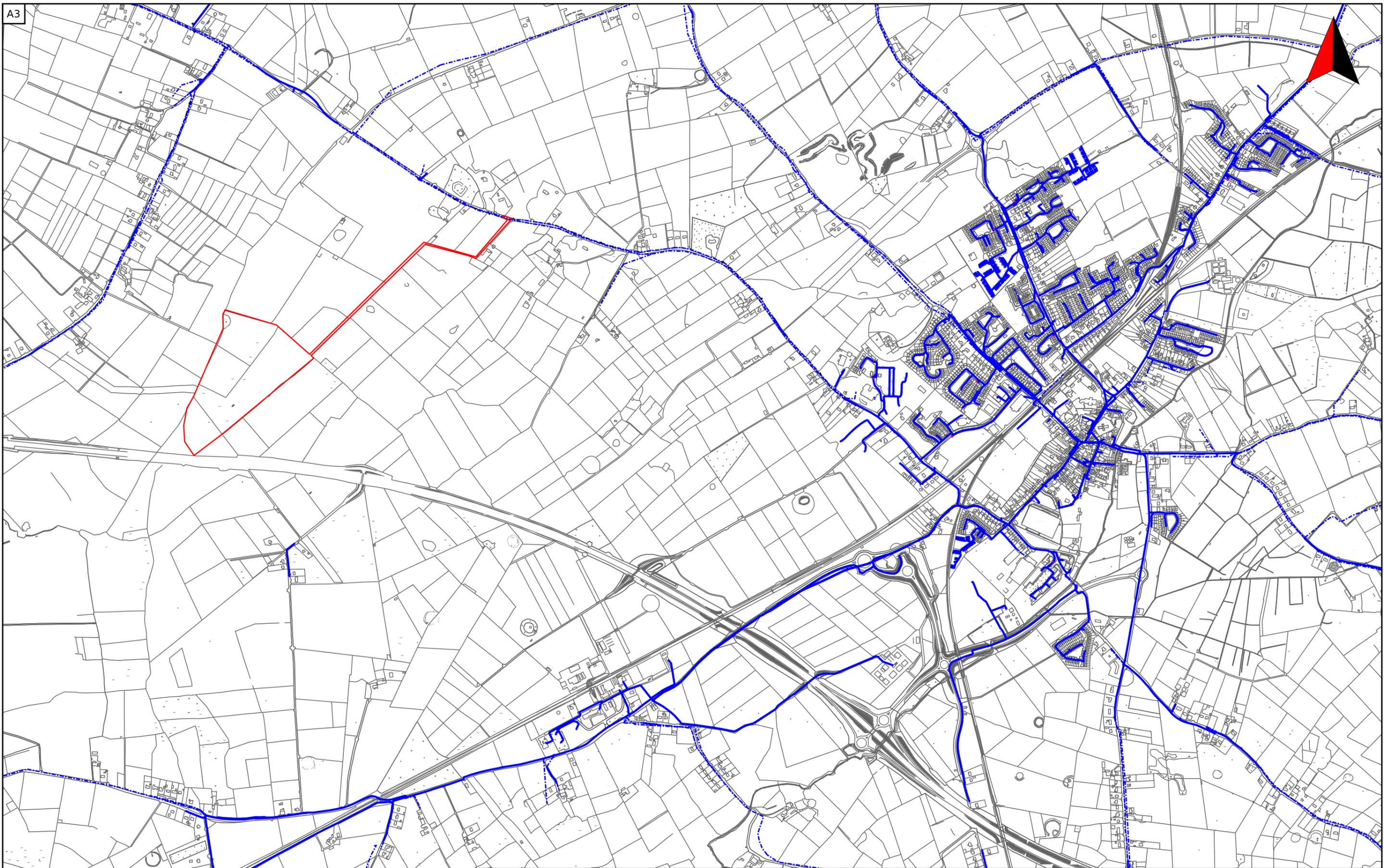
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Scale:  
1:15000

Irish National Grid  
Centre XY: 516458 m,  
727666 m

Date  
08/05/2025

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Drawing Produced: 25/04/2025 16:31

Description of Works:

Peaker Plant Route B

Project Reference:

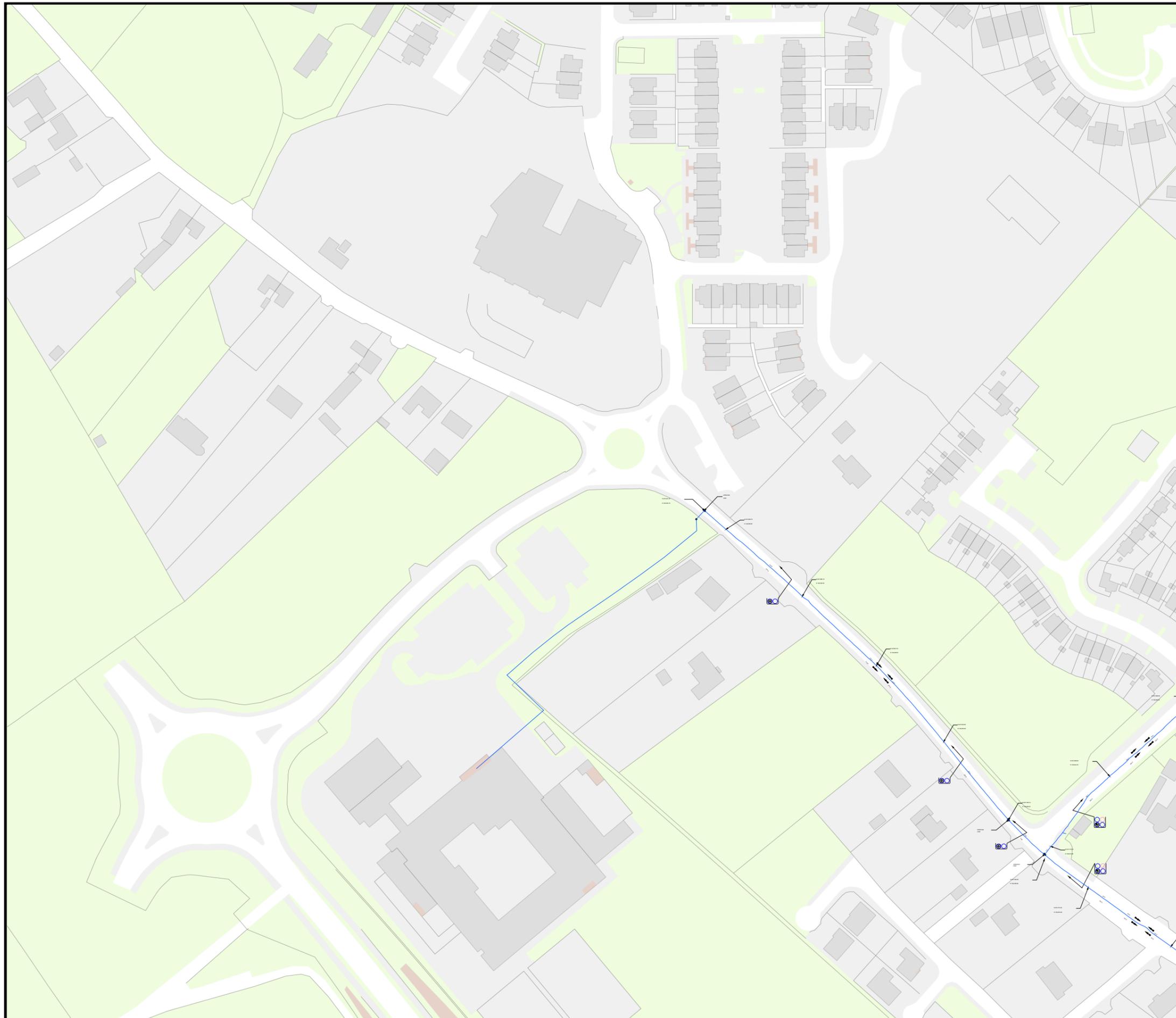
Peaker Plant Route B

Customer Name: Caoimhe Maguire

Company: Atkins Realis

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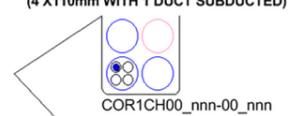
LEGEND

- DUCT
- THIRD PARTY DUCT
- THIRD PARTY CHAMBER
- CARRIAGEWAY CHAMBER (CW1)
- CARRIAGEWAY CHAMBER (CW2)
- CARRIAGEWAY CHAMBER (CW3)
- VERGECHAMBER (VW1)
- VERGE CHAMBER (VW2)
- VERGE CHAMBER (VW3)
- FOOTWAY CHAMBER (FW1)
- FOOTWAY CHAMBER (FW2)
- FOOTWAY CHAMBER (FW3)
- CHAMBER LXXX
- SWEPT T SWTXXX
- CAP END CPXXX
- SPLICE POINT
- LOOPJOINT
- SPECIAL ENGINEERING DIFFICULTY
- SWEPT TEE

NOTES:  
ALL DUCTS AT STANDARD DEPTH  
600mm IN CARRIAGEWAY  
450mm IN FOOTWAY/GRASS  
UNLESS OTHERWISE SHOWN eg

- SHEET SCHEMATIC
- CUSTOMER PREMISES

DUCT CONFIGURATION  
(4 X 110mm WITH 1 DUCT SUBDUCTED)



COR1CH00\_nnn-00\_nnn



Drawing Produced: 25/04/2025 16:31

Description of Works:

Peaker Plant Route B

Project Reference:

Peaker Plant Route B

Customer Name: Caoimhe Maguire

Company: Atkins Realis

Disclaimer:

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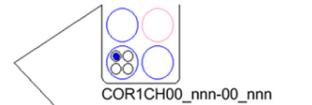
LEGEND

- DUCT
- THIRD PARTY DUCT
- THIRD PARTY CHAMBER
- CARRIAGEWAY CHAMBER (CW1)
- CARRIAGEWAY CHAMBER (CW2)
- CARRIAGEWAY CHAMBER (CW3)
- VERGECHAMBER (VW1)
- VERGE CHAMBER (VW2)
- VERGE CHAMBER (VW3)
- FOOTWAY CHAMBER (FW1)
- FOOTWAY CHAMBER (FW2)
- FOOTWAY CHAMBER (FW3)
- CHAMBER LXXX
- SWEPT T SWTXXX
- CAP END CPXXX
- SPLICE POINT
- LOOPJOINT
- SPECIAL ENGINEERING DIFFICULTY
- SWEPT TEE
- SHEET SCHEMATIC
- CUSTOMER PREMISES

NOTES:  
ALL DUCTS AT STANDARD DEPTH  
600mm IN CARRIAGEWAY  
450mm IN FOOTWAY/GRASS  
UNLESS OTHERWISE SHOWN eg



DUCT CONFIGURATION  
(4 X110mm WITH 1 DUCT SUBDUCTED)





Drawing Produced: 25/04/2025 16:34

Description of Works:

Peaker Plant Route A

Project Reference:

Peaker Plant Route A

Customer Name: Caoimhe Maguire

Company: Atkins Realis

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LEGEND

- DUCT
- THIRD PARTY DUCT
- THIRD PARTY CHAMBER
- CARRIAGEWAY CHAMBER (CW1)
- CARRIAGEWAY CHAMBER (CW2)
- CARRIAGEWAY CHAMBER (CW3)
- FOOTWAY CHAMBER (FW1)
- FOOTWAY CHAMBER (FW2)
- FOOTWAY CHAMBER (FW3)
- VERGECHAMBER (VW1)
- VERGE CHAMBER (VW2)
- VERGE CHAMBER (VW3)
- CHAMBER LXXX
- SWEPT T SWTXXX
- CAP END CPXXX
- SPLICE POINT
- LOOPJOINT
- SPECIAL ENGINEERING DIFFICULTY
- SWEPT TEE

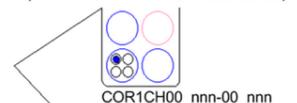
NOTES:  
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600mm IN CARRIAGEWAY  
450mm IN FOOTWAY/GRASS  
UNLESS OTHERWISE SHOWN eg



SHEET SCHEMATIC



DUCT CONFIGURATION  
(4 X 110mm WITH 1 DUCT SUBDUCTED)





Drawing Produced: 25/04/2025 16:34

Description of Works:

Peaker Plant Route A

Project Reference:

Peaker Plant Route A

Customer Name: Caoimhe Maguire

Company: Atkins Realis

Disclaimer:

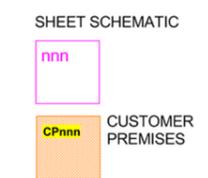
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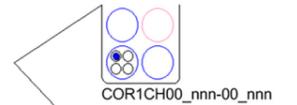
LEGEND

- DUCT
- THIRD PARTY DUCT
- THIRD PARTY CHAMBER
- CARRIAGEWAY CHAMBER (CW1)
- CARRIAGEWAY CHAMBER (CW2)
- CARRIAGEWAY CHAMBER (CW3)
- FOOTWAY CHAMBER (FW1)
- FOOTWAY CHAMBER (FW2)
- FOOTWAY CHAMBER (FW3)
- VERGECHAMBER (VW1)
- VERGE CHAMBER (VW2)
- VERGE CHAMBER (VW3)
- CHAMBER LXXX
- SWEPT T SWTXXX
- CAP END CPXXX
- SPLICE POINT
- LOOPJOINT
- SPECIAL ENGINEERING DIFFICULTY
- SWEPT TEE

NOTES:  
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600mm IN CARRIAGEWAY  
450mm IN FOOTWAY/GRASS  
UNLESS OTHERWISE SHOWN eg



DUCT CONFIGURATION  
(4 X110mm WITH 1 DUCT SUBDUCTED)





**Drawing Produced:** 25/04/2025 16:34

**Description of Works:**

Peaker Plant Route A

**Project Reference:**

Peaker Plant Route A

**Customer Name:** Caoimhe Maguire

**Company:** Atkins Realis

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**LEGEND**

- DUCT
- THIRD PARTY DUCT
- THIRD PARTY CHAMBER
- CARRIAGEWAY CHAMBER (CW1)
- CARRIAGEWAY CHAMBER (CW2)
- CARRIAGEWAY CHAMBER (CW3)
- FOOTWAY CHAMBER (FW1)
- FOOTWAY CHAMBER (FW2)
- FOOTWAY CHAMBER (FW3)
- VERGECHAMBER (VW1)
- VERGE CHAMBER (VW2)
- VERGE CHAMBER (VW3)
- CHAMBER LXXX
- SWEPT T SWTXXX
- CAP END CPXXX
- SPLICE POINT
- LOOPJOINT
- SPECIAL ENGINEERING DIFFICULTY
- SWEPT TEE

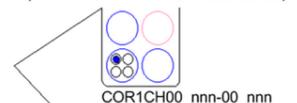
NOTES:  
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600mm IN CARRIAGEWAY  
450mm IN FOOTWAY/GRASS  
UNLESS OTHERWISE SHOWN eg



SHEET SCHEMATIC



DUCT CONFIGURATION  
(4 X110mm WITH 1 DUCT SUBDUCTED)





ESB Networks

TITLE:

20250512-070\_A0\_1

COLOUR CODE:

- BLACK - 38KV & HIGHER VOLTAGE OVERHEAD LINES
- GREEN - MV(10KV/20KV) OVERHEAD LINES
- BLUE - LV (400V/230V) OVERHEAD LINES
- CYAN - 38KV & HIGHER VOLTAGE UNDERGROUND CABLE ROUTES
- RED - MV/LV (10KV/20KV/400V/230V) UNDERGROUND CABLE ROUTES

DATE: 12-May-2025

\*\* SCALE: 1:2500

\*\* SCALE WHEN PRINTED ON AN A0 PAGE  
XY COORDINATES DISPLAYED IN IRISH GRID COORDINATE SYSTEM

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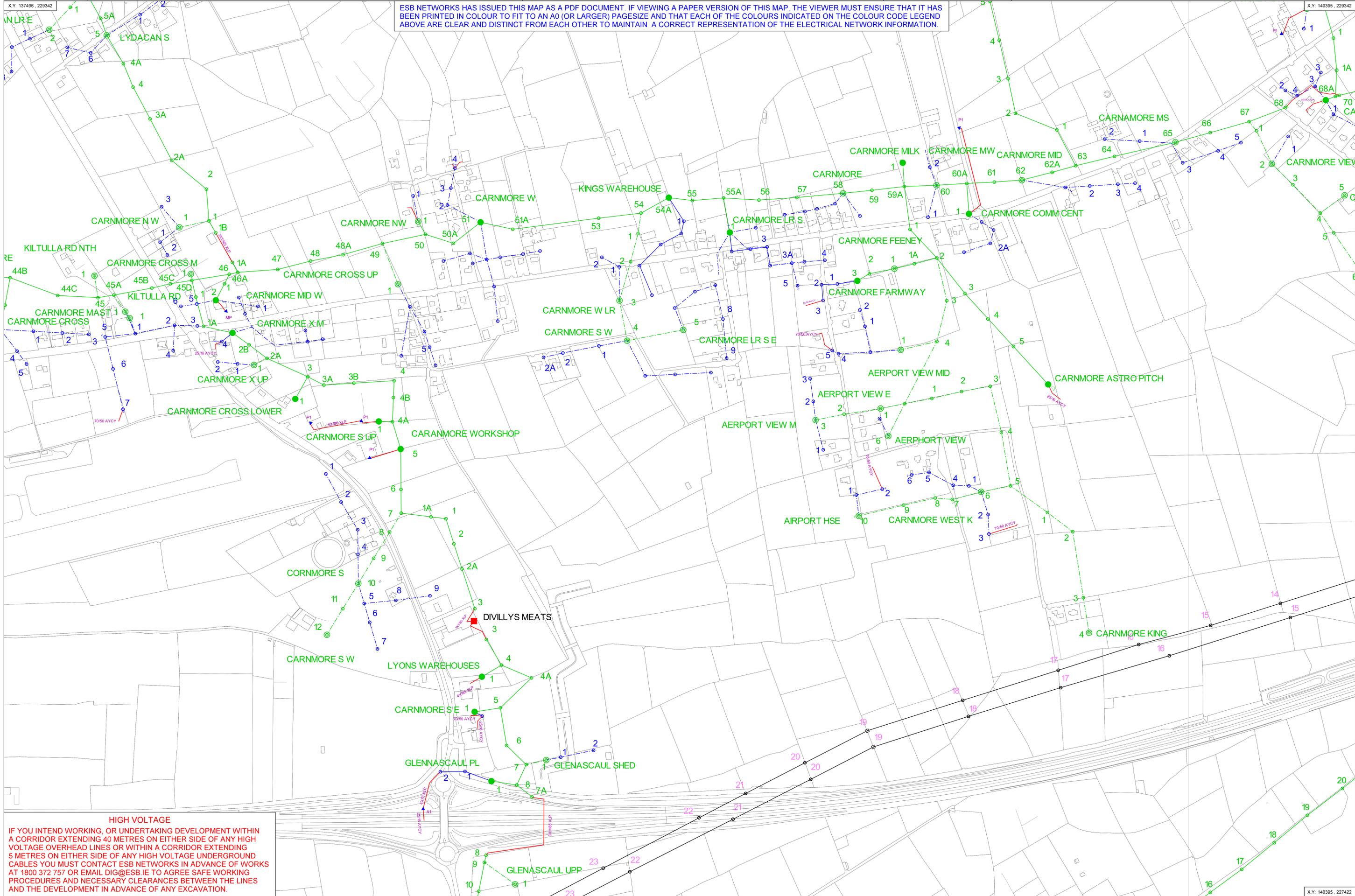
WARNING

THIS MAP INDICATES THE APPROXIMATE LOCATION OF ESB TRANSMISSION (400KV, 220KV, 110KV, 38KV) AND DISTRIBUTION (20KV, 10KV, 230V/400V) UNDERGROUND CABLES AND OVERHEAD LINES IN THE GENERAL AREA OF THE PROPOSED WORKS. ESB NETWORKS TAKES NO RESPONSIBILITY FOR THE ACCURACY OR COMPLETENESS OF THE MAP. IT IS THE USER'S RESPONSIBILITY TO INDEPENDENTLY VERIFY THE INFORMATION AND THE LOCATION OF UNDERGROUND CABLES AND OVERHEAD LINES. LOW VOLTAGE (230V/400V) SERVICE CABLES (E.G. HOUSE SERVICES, FACTORY/SHOP SERVICES, PUBLIC LIGHTING LAMP SERVICES, ETC) ARE NOT INCLUDED BUT THEIR PRESENCE SHOULD BE ANTICIPATED. THE DEPTHS OF UNDERGROUND CABLES MUST NEVER BE ASSUMED BEFORE ANY MECHANICAL EXCAVATION IS UNDERTAKEN. THE ACTUAL LOCATION OF ALL UNDERGROUND ELECTRICITY CABLES MUST BE ESTABLISHED AND VERIFIED ON THE SITE USING:

- (A) UP-TO-DATE MAP RECORDS;
- (B) CABLE LOCATOR EQUIPMENT OPERATED IN BOTH POWER AND RADIO MODES;
- (C) CAREFUL HAND DIGGING OF TRIAL HOLES USING "SAFE DIGGING PRACTICE".

REFER ALSO TO HSA CODE OF PRACTICE FOR AVOIDING DANGER FROM UNDERGROUND SERVICES.  
ESB TAKES NO RESPONSIBILITY FOR AND SHALL BEAR NO LIABILITY, HOWSOEVER ARISING, IN RELATION TO ANY DAMAGE, INJURY/DEATH OR LOSS OF SUPPLY AS A RESULT OF DAMAGE OR INTERFERENCE WITH ITS NETWORKS.

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**HIGH VOLTAGE**  
IF YOU INTEND WORKING, OR UNDERTAKING DEVELOPMENT WITHIN A CORRIDOR EXTENDING 40 METRES ON EITHER SIDE OF ANY HIGH VOLTAGE OVERHEAD LINES OR WITHIN A CORRIDOR EXTENDING 5 METRES ON EITHER SIDE OF ANY HIGH VOLTAGE UNDERGROUND CABLES YOU MUST CONTACT ESB NETWORKS IN ADVANCE OF WORKS AT 1800 372 757 OR EMAIL DIG@ESB.IE TO AGREE SAFE WORKING PROCEDURES AND NECESSARY CLEARANCES BETWEEN THE LINES AND THE DEVELOPMENT IN ADVANCE OF ANY EXCAVATION.







TITLE:  
20250512-070\_A0\_4

| COLOUR CODE: |  |
|--------------|--|
| BLACK        | - 38KV & HIGHER VOLTAGE OVERHEAD LINES                 |
| GREEN        | - MV(10KV/20KV) OVERHEAD LINES                         |
| BLUE         | - LV (400V/230V) OVERHEAD LINES                        |
| CYAN         | - 38KV & HIGHER VOLTAGE UNDERGROUND CABLE ROUTES       |
| RED          | - MV/LV (10KV/20KV/400V/230V) UNDERGROUND CABLE ROUTES |

DATE: 12-May-2025

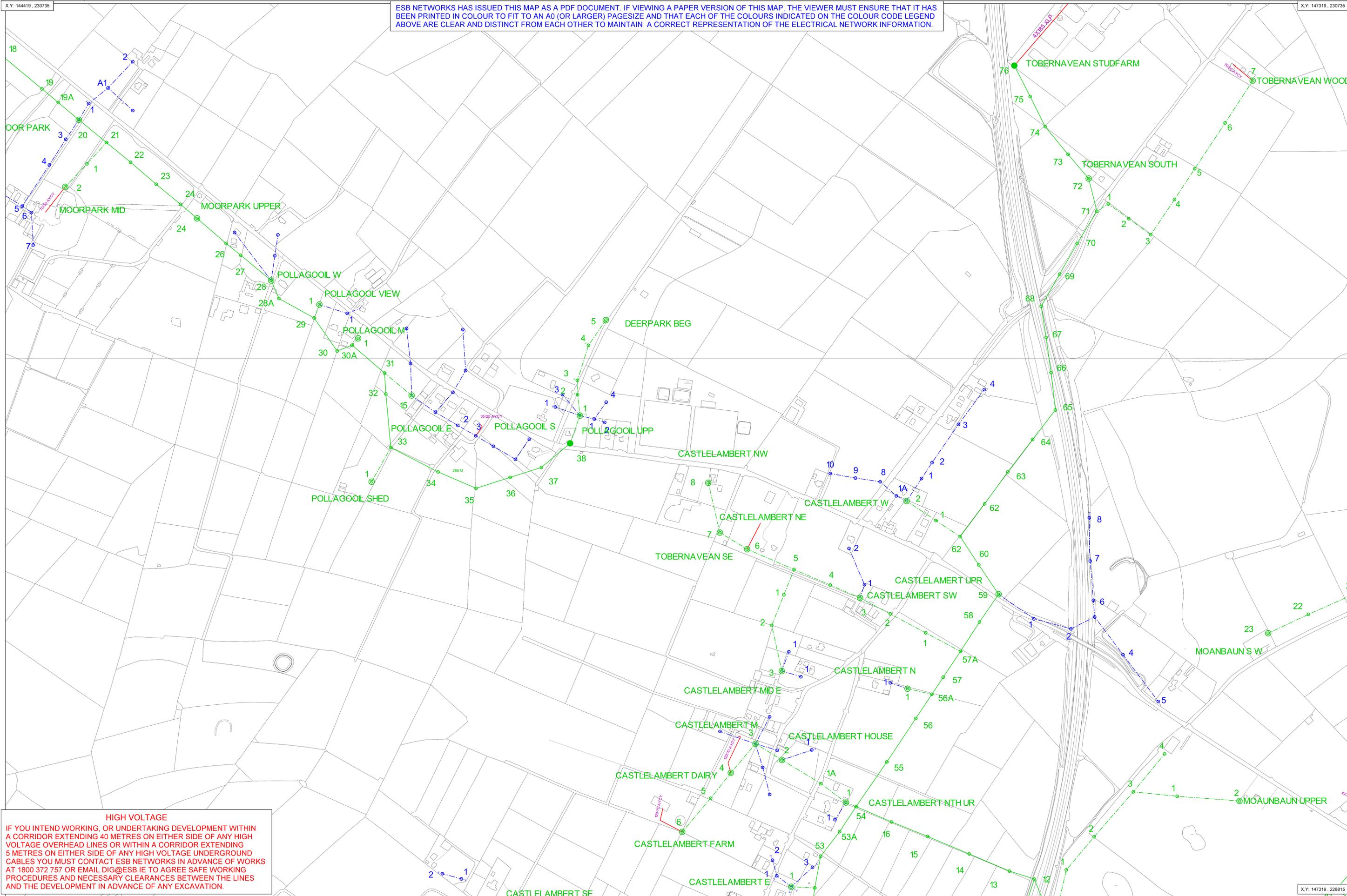
\*\* SCALE: 1:2500

\*\* SCALE WHEN PRINTED ON AN A0 PAGE  
XY COORDINATES DISPLAYED IN IRISH GRID COORDINATE SYSTEM

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X,Y: 144419, 230735

X,Y: 147319, 230735

X,Y: 147319, 228815



TITLE:  
20250512-070\_A0\_5

COLOUR CODE:

|       |  |
|-------|--|
| BLACK | - 38KV & HIGHER VOLTAGE OVERHEAD LINES                 |
| GREEN | - MV(10KV/20KV) OVERHEAD LINES                         |
| BLUE  | - LV (400V/230V) OVERHEAD LINES                        |
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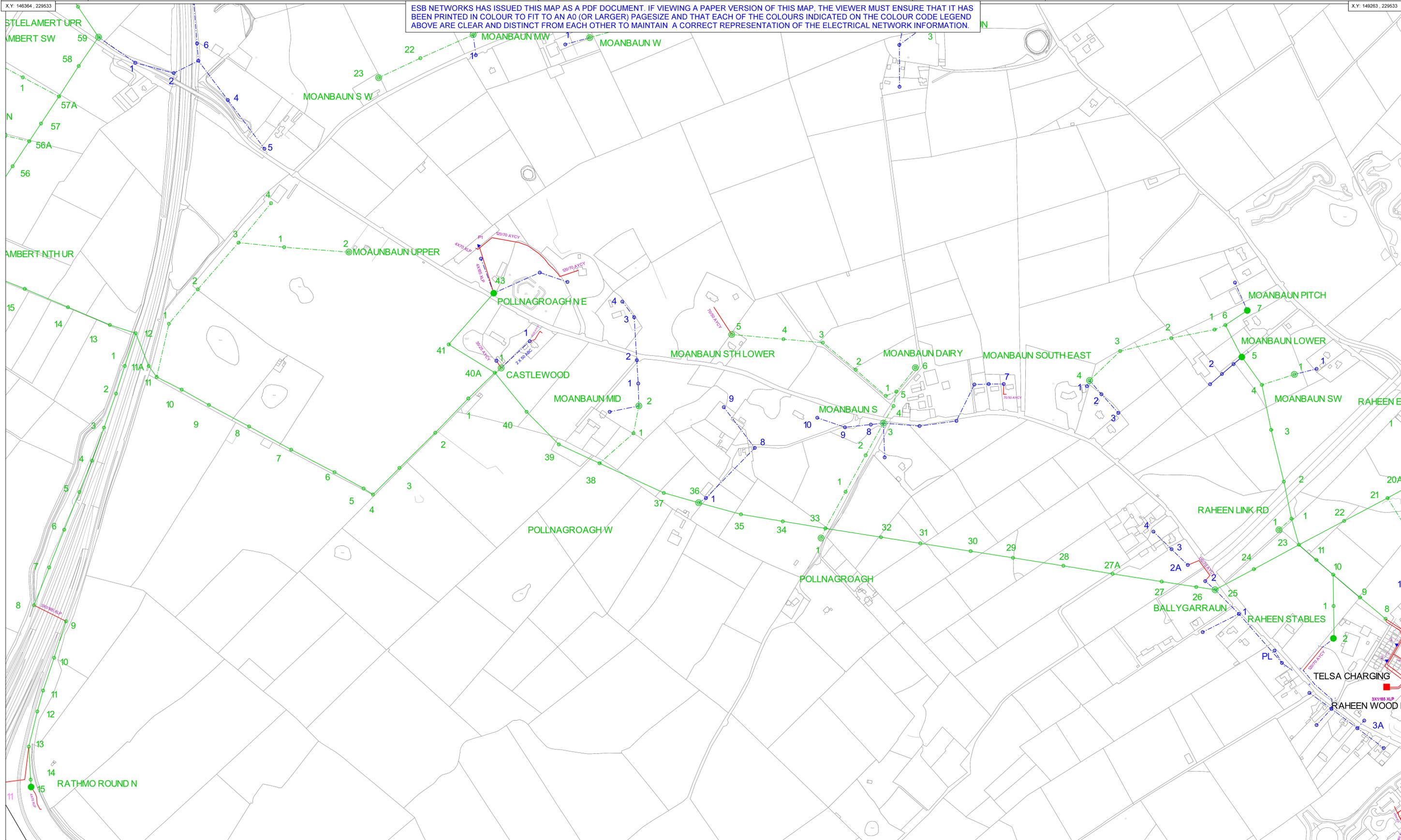
DATE: 12-May-2025

\*\* SCALE: 1:2500

\*\* SCALE WHEN PRINTED ON AN A0 PAGE  
XY COORDINATES DISPLAYED IN IRISH GRID COORDINATE SYSTEM

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TITLE:  
20250512-070\_A0\_6

| COLOUR CODE: |  |
|--------------|--|
| BLACK        | - 38KV & HIGHER VOLTAGE OVERHEAD LINES                 |
| GREEN        | - MV(10KV/20KV) OVERHEAD LINES                         |
| BLUE         | - LV (400V/230V) OVERHEAD LINES                        |
| CYAN         | - 38KV & HIGHER VOLTAGE UNDERGROUND CABLE ROUTES       |
| RED          | - MV/LV (10KV/20KV/400V/230V) UNDERGROUND CABLE ROUTES |

DATE: 12-May-2025

\*\* SCALE: 1:2500

\*\* SCALE WHEN PRINTED ON AN A0 PAGE  
XY COORDINATES DISPLAYED IN IRISH GRID COORDINATE SYSTEM

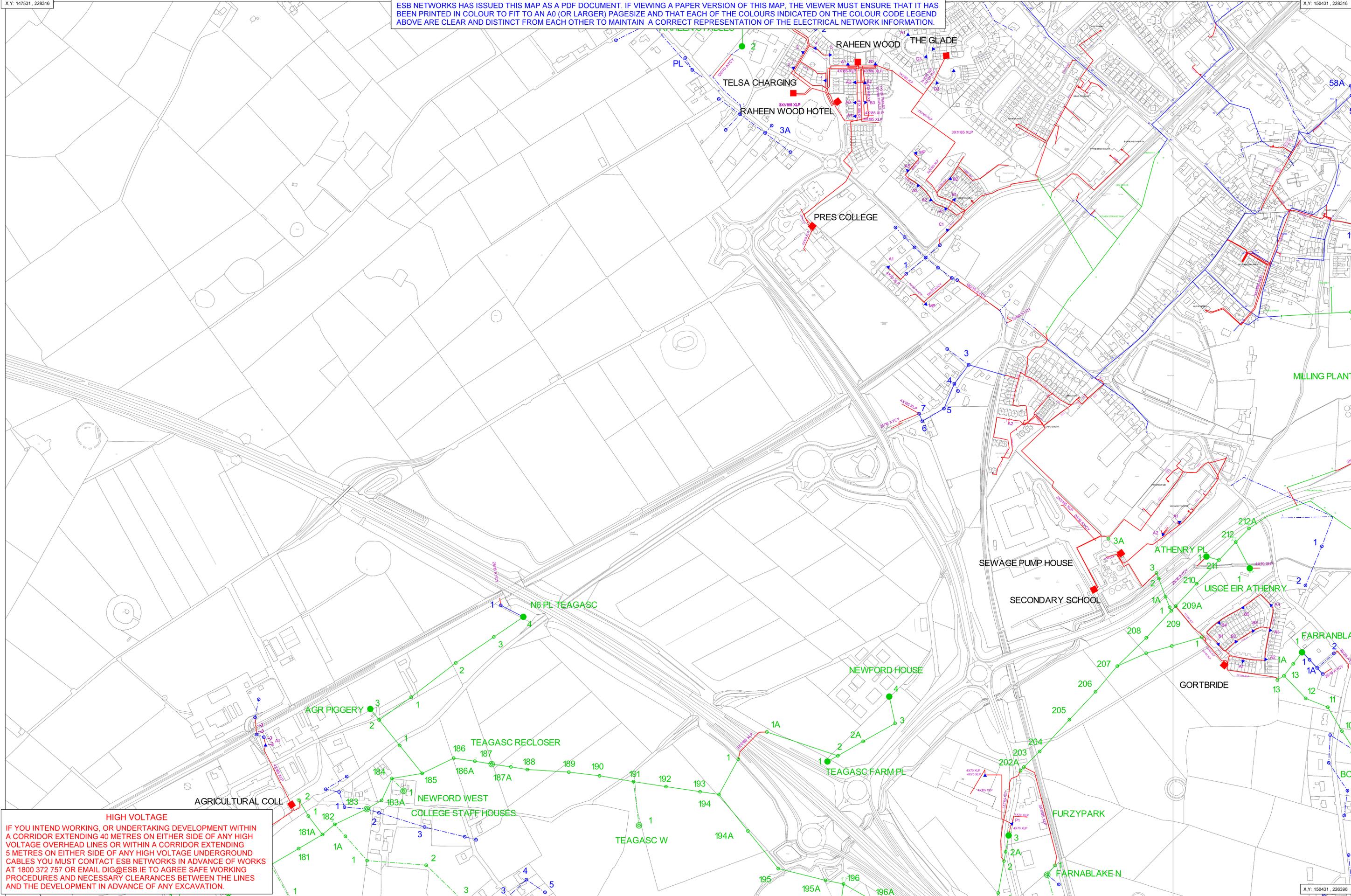
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X,Y: 147531, 228316

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X,Y: 150431, 228316



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X,Y: 150431, 228316



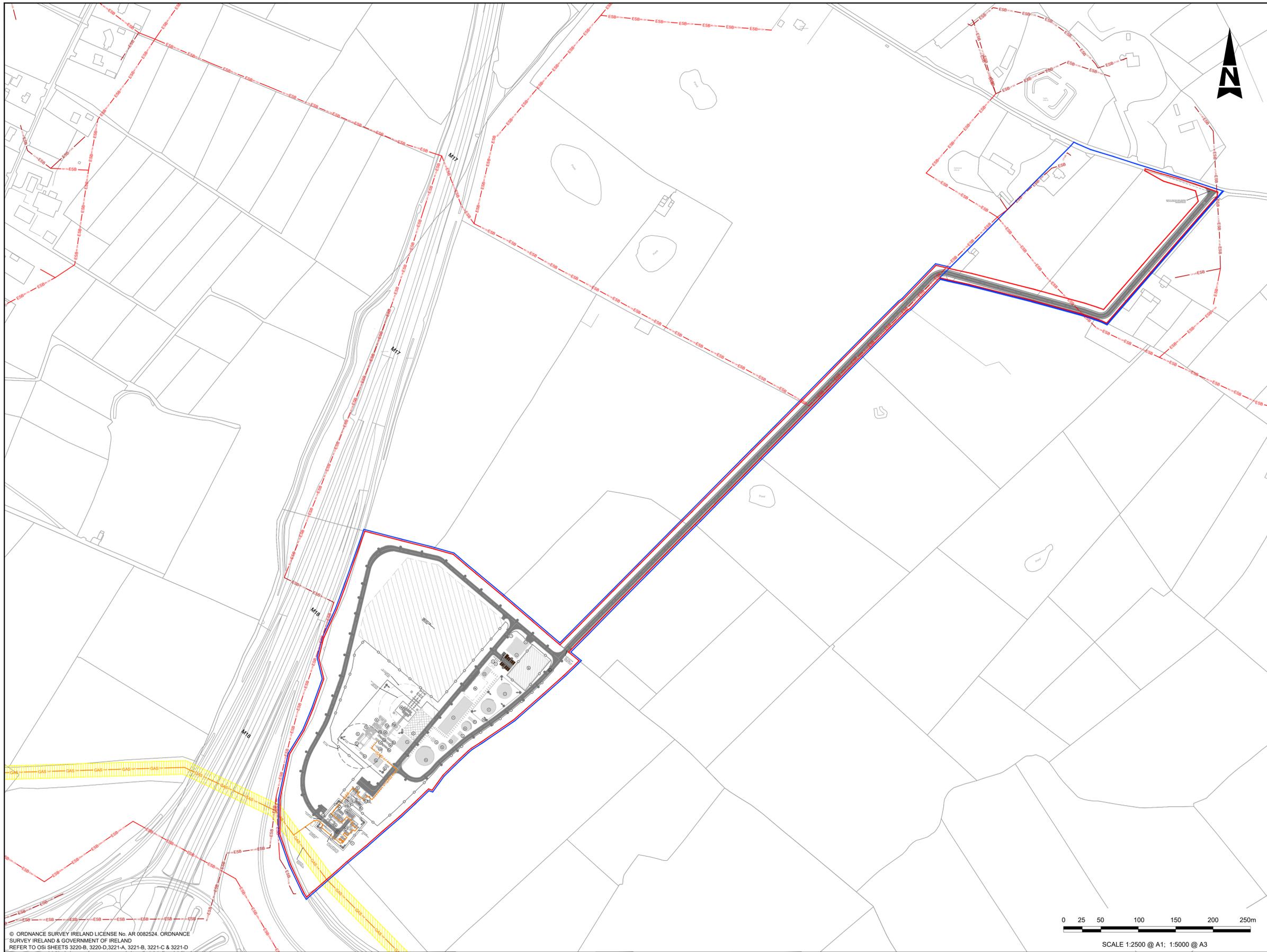




A1

DO NOT SCALE

File: PEK3-ATK-ZZ-01-DR-CE-902711.dwg  
Date: Feb 09, 2026 - 12:04pm  
Plotted by: DDMH1347



- GENERAL NOTES**
1. ALL DIMENSIONS ARE IN METERS UNLESS NOTED OTHERWISE
  2. ONLY WRITTEN DIMENSIONS SHALL BE USED. NO DIMENSIONS SHALL BE SCALED FROM THE DRAWINGS
  3. ALL LEVELS ARE IN METERS AND ARE TO MALIN HEAD DATUM
  4. ALL COORDINATES ARE IN METERS AND ARE TO IRISH TRANSVERSE MERCATOR
  5. DRAWINGS ARE TO BE READ IN CONJUNCTION WITH THE SPECIFICATION
  6. THIS DRAWING IS TO BE USED ONLY FOR THE PURPOSES OF THE PLANNING APPLICATION AND IS SUBJECT TO DETAILED DESIGN.

- LEGEND:**
- PROJECT BOUNDARY FOR PLANNING
  - LAND OWNERSHIP BOUNDARY
  - ESB LV UNDERGROUND
  - ESB MV UNDERGROUND
  - ESB MV OVERHEAD
  - ESB 220KV OVERHEAD
  - GAS
  - WAYLEAVE

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0 25 50 100 150 200 250m  
SCALE 1:2500 @ A1; 1:5000 @ A3

Purpose **PLANNING**

Title **EXISTING ESB INFRASTRUCUTRE**

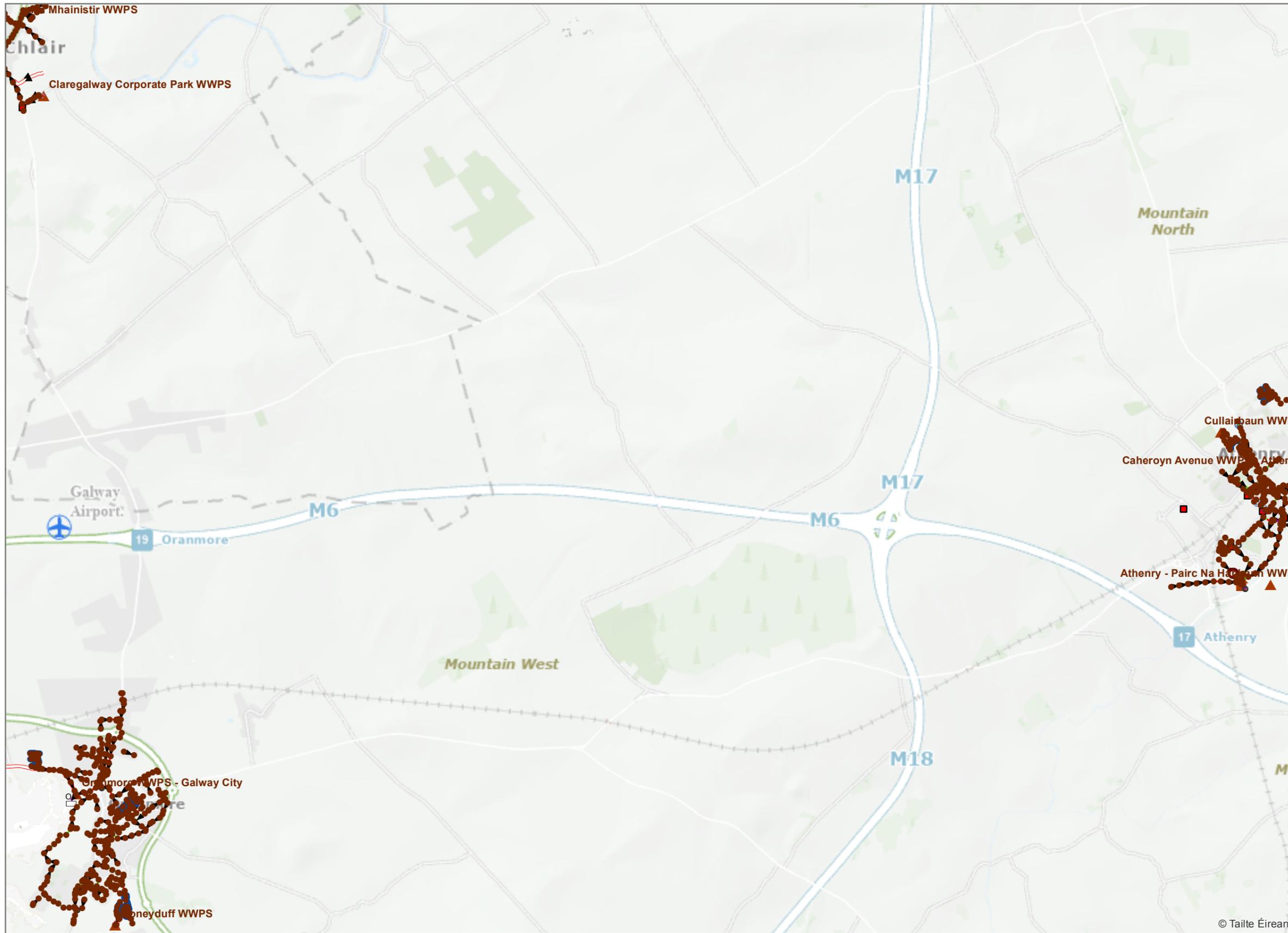
| Rev | Description         | By | Date     | Chk'd | Auth |
|-----|---------------------|----|----------|-------|------|
| 0   | ISSUED FOR PLANNING | PS | 01.12.25 | ND    | AJB  |

**AtkinsRéalis**  
DUBLIN | CORK | GALWAY | DUNDALK  
ATKINS HOUSE, 150 AIRSIDE BUSINESS PARK,  
SWORDS, DUBLIN, K67 K5W4.  
Tel : +353 1 810 8000 Email : info.ie@atkinsrealis.com

**Bord Gáis Energy**  
Project **CASHLA PEAKER PLANT**  
Rathmorrisy and Pollnagroagh  
(Townlands), Atheryn, Co. Galway.

| Original Scale | Design/Drawn | Checked | Authorized |
|----------------|--------------|---------|------------|
| 1:2500 at A1   | PS           | ND      | AJB        |
| Date           | 01.12.25     | Date    | 01.12.25   |
| Date           | 01.12.25     | Date    | 01.12.25   |

| Status | Drawing Number              | Rev |
|--------|-----------------------------|-----|
| A2     | PEK3-ATK-ZZ-01-DR-CE-902711 | 0   |



- Backdrop
- Other; Unknown
- Sewer Discharge Points**
- Overflow
- Other; Unknown
- Sewer Inlets**
- ⊕ Gully
- Other; Unknown
- Sewer Fittings**
- Vent/Col
- Other; Unknown
- Sewer Mains (Irish Water)**
- Gravity - Combined
- Gravity - Foul
- Gravity - Overflow
- Gravity - Unknown
- Pumping - Foul
- Sewer Mains (Private)**
- Gravity - Foul
- Pumping - Foul
- Sewer Lateral Lines**
- Sewer Lateral Lines
- Pump Station**
- ▲ Pump Station
- Waste Water Treatment Plant**
- 🏠 Waste Water Treatment Plant



Coordinate System: TM65 Irish Grid  
Projection: Transverse Mercator

Scale @ A3: 1:40,000

Drawing No.: IW-AGG-2023-000

Drawn By: RG

Checked By: <Add Name>

Approved By: <Add Name>

Drawn Date: 01/05/2025

Checked Date: <dd/mm/yyyy>

Approved Date: <dd/mm/yyyy>



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## Sewer Network Athenry-Oranmore, Co. Galway

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# Appendix B. Met Eireann Rainfall Data



Met Eireann  
Return Period Rainfall Depths for sliding Durations  
Irish Grid: Easting: 146600, Northing: 228137,

| DURATION | Interval |        | Years  |        |        |        |        |        |        |        |        |        |        |
|----------|----------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|
|          | 6months, | 1year, | 2,     | 3,     | 4,     | 5,     | 10,    | 20,    | 30,    | 50,    | 75,    | 100,   | 120,   |
| 5 mins   | 2.7,     | 3.7,   | 4.2,   | 4.9,   | 5.4,   | 5.8,   | 7.1,   | 8.4,   | 9.3,   | 10.5,  | 11.6,  | 12.5,  | 13.0,  |
| 10 mins  | 3.8,     | 5.1,   | 5.8,   | 6.9,   | 7.6,   | 8.1,   | 9.8,   | 11.7,  | 13.0,  | 14.7,  | 16.2,  | 17.4,  | 18.1,  |
| 15 mins  | 4.4,     | 6.0,   | 6.9,   | 8.1,   | 8.9,   | 9.5,   | 11.6,  | 13.8,  | 15.3,  | 17.3,  | 19.1,  | 20.4,  | 21.3,  |
| 30 mins  | 5.9,     | 7.9,   | 8.9,   | 10.4,  | 11.4,  | 12.2,  | 14.7,  | 17.4,  | 19.1,  | 21.5,  | 23.6,  | 25.3,  | 26.3,  |
| 1 hours  | 7.8,     | 10.3,  | 11.6,  | 13.4,  | 14.7,  | 15.6,  | 18.6,  | 21.8,  | 23.9,  | 26.8,  | 29.3,  | 31.2,  | 32.5,  |
| 2 hours  | 10.3,    | 13.4,  | 15.0,  | 17.3,  | 18.8,  | 19.9,  | 23.6,  | 27.5,  | 30.0,  | 33.4,  | 36.4,  | 38.6,  | 40.1,  |
| 3 hours  | 12.1,    | 15.6,  | 17.4,  | 20.0,  | 21.7,  | 23.0,  | 27.1,  | 31.4,  | 34.2,  | 38.0,  | 41.2,  | 43.7,  | 45.3,  |
| 4 hours  | 13.6,    | 17.5,  | 19.4,  | 22.2,  | 24.1,  | 25.5,  | 29.9,  | 34.6,  | 37.5,  | 41.6,  | 45.1,  | 47.7,  | 49.5,  |
| 6 hours  | 16.0,    | 20.4,  | 22.6,  | 25.8,  | 27.9,  | 29.4,  | 34.3,  | 39.5,  | 42.8,  | 47.3,  | 51.1,  | 54.0,  | 55.9,  |
| 9 hours  | 18.8,    | 23.8,  | 26.3,  | 29.9,  | 32.2,  | 34.0,  | 39.4,  | 45.2,  | 48.8,  | 53.8,  | 58.0,  | 61.2,  | 63.3,  |
| 12 hours | 21.1,    | 26.6,  | 29.3,  | 33.2,  | 35.7,  | 37.6,  | 43.5,  | 49.7,  | 53.6,  | 58.9,  | 63.4,  | 66.8,  | 69.0,  |
| 18 hours | 24.9,    | 31.1,  | 34.2,  | 38.5,  | 41.3,  | 43.4,  | 49.9,  | 56.8,  | 61.1,  | 67.0,  | 71.9,  | 75.6,  | 78.1,  |
| 24 hours | 27.9,    | 34.7,  | 38.0,  | 42.8,  | 45.8,  | 48.1,  | 55.1,  | 62.5,  | 67.1,  | 73.3,  | 78.6,  | 82.6,  | 85.2,  |
| 2 days   | 36.3,    | 44.4,  | 48.2,  | 53.7,  | 57.2,  | 59.8,  | 67.8,  | 76.1,  | 81.2,  | 88.1,  | 93.9,  | 98.2,  | 101.0, |
| 3 days   | 43.5,    | 52.5,  | 56.9,  | 62.9,  | 66.8,  | 69.6,  | 78.4,  | 87.5,  | 93.1,  | 100.5, | 106.7, | 111.4, | 114.4, |
| 4 days   | 49.9,    | 59.8,  | 64.6,  | 71.2,  | 75.4,  | 78.5,  | 88.0,  | 97.7,  | 103.7, | 111.6, | 118.3, | 123.2, | 126.4, |
| 6 days   | 61.7,    | 73.1,  | 78.6,  | 86.1,  | 90.9,  | 94.4,  | 105.1, | 116.0, | 122.7, | 131.5, | 138.8, | 144.3, | 147.8, |
| 8 days   | 72.4,    | 85.2,  | 91.3,  | 99.7,  | 104.9, | 108.8, | 120.5, | 132.5, | 139.8, | 149.3, | 157.3, | 163.2, | 167.1, |
| 10 days  | 82.6,    | 96.6,  | 103.2, | 112.3, | 118.0, | 122.3, | 135.0, | 147.8, | 155.7, | 165.9, | 174.5, | 180.8, | 184.9, |
| 12 days  | 92.3,    | 107.5, | 114.6, | 124.4, | 130.5, | 135.0, | 148.6, | 162.4, | 170.7, | 181.6, | 190.7, | 197.3, | 201.7, |
| 16 days  | 110.9,   | 128.1, | 136.2, | 147.3, | 154.1, | 159.2, | 174.4, | 189.7, | 198.9, | 211.0, | 221.0, | 228.3, | 233.1, |
| 20 days  | 128.6,   | 147.8, | 156.8, | 168.9, | 176.5, | 182.0, | 198.7, | 215.4, | 225.4, | 238.5, | 249.4, | 257.3, | 262.5, |
| 25 days  | 150.1,   | 171.5, | 181.4, | 194.9, | 203.2, | 209.3, | 227.6, | 245.9, | 256.9, | 271.2, | 283.0, | 291.6, | 297.2, |

NOTES:

These values are derived from a Depth Duration Frequency (DDF) Model update 2023

For details refer to:

'Mateus C., and Coonan, B. 2023. Estimation of point rainfall frequencies in Ireland. Technical Note No. 68. Met Eireann',

Available for download at:

<http://hdl.handle.net/2262/102417>

# Appendix C. Storm sewer calculations



**Design Settings**

|                       |                      |                                      |               |
|-----------------------|----------------------|--------------------------------------|---------------|
| Rainfall Methodology  | FSR                  | Maximum Time of Concentration (mins) | 30.00         |
| Return Period (years) | 5                    | Maximum Rainfall (mm/hr)             | 250.0         |
| Additional Flow (%)   | 0                    | Minimum Velocity (m/s)               | 1.00          |
| FSR Region            | Scotland and Ireland | Connection Type                      | Level Soffits |
| M5-60 (mm)            | 15.600               | Minimum Backdrop Height (m)          | 0.200         |
| Ratio-R               | 0.260                | Preferred Cover Depth (m)            | 1.200         |
| CV                    | 1.000                | Include Intermediate Ground          | ✓             |
| Time of Entry (mins)  | 5.00                 | Enforce best practice design rules   | x             |

**Nodes**

| Name   | Area (ha) | T of E (mins) | Cover Level (m) | Diameter (mm) | Easting (m) | Northing (m) | Depth (m) |
|--------|-----------|---------------|-----------------|---------------|-------------|--------------|-----------|
| 3      | 0.077     | 5.00          | 57.465          |               | 546483.757  | 728254.957   | 1.050     |
| 1      | 0.033     | 5.00          | 57.013          |               | 546518.316  | 728237.837   | 1.050     |
| 4      | 0.053     | 5.00          | 57.383          | 1200          | 546468.272  | 728188.687   | 2.049     |
| 5      | 0.056     | 5.00          | 56.858          |               | 546441.692  | 728116.310   | 2.117     |
| 6      | 0.029     | 5.00          | 56.451          |               | 546417.414  | 728068.171   | 2.125     |
| 7      | 0.059     | 5.00          | 56.139          |               | 546415.612  | 728029.722   | 2.109     |
| 8      | 0.024     | 5.00          | 56.061          |               | 546427.121  | 728007.333   | 2.225     |
| 12     |           |               | 56.056          | 1200          | 546420.387  | 727981.144   | 2.066     |
| 15     |           |               | 56.722          | 1200          | 546475.478  | 728048.112   | 3.446     |
| 16     | 0.028     | 5.00          | 56.838          | 1200          | 546447.690  | 728094.346   | 1.350     |
| 17     | 0.014     | 5.00          | 56.493          | 1200          | 546509.135  | 728042.209   | 1.811     |
| 21     | 0.046     | 5.00          | 56.505          | 1200          | 546501.650  | 728026.108   | 3.717     |
| 22     | 0.058     | 5.00          | 56.283          | 1200          | 546529.759  | 728059.174   | 3.619     |
| 23     | 0.063     | 5.00          | 55.706          | 1200          | 546586.686  | 728127.419   | 3.296     |
| 59     | 0.065     | 5.00          | 55.236          | 1200          | 546631.348  | 728179.844   | 3.053     |
| 37     | 0.024     | 5.00          | 57.090          |               | 546523.011  | 728254.559   | 1.050     |
| 38     | 0.060     | 5.00          | 57.283          | 1200          | 546490.532  | 728274.309   | 1.623     |
| 39     | 0.085     | 5.00          | 56.603          | 1200          | 546509.418  | 728340.613   | 1.634     |
| 41     | 0.082     | 5.00          | 56.052          | 1200          | 546588.817  | 728333.114   | 1.976     |
| 2      |           |               | 57.352          | 1200          | 546477.322  | 728190.302   | 1.947     |
| 46     | 0.008     | 5.00          | 53.906          | 1200          | 546684.416  | 728258.568   | 1.668     |
| 55     | 0.051     | 5.00          | 53.664          | 1200          | 546685.671  | 728246.559   | 3.008     |
| 60     | 0.017     | 5.00          | 54.080          | 1200          | 546669.723  | 728226.416   | 3.529     |
| 49     | 0.050     | 5.00          | 55.829          | 1200          | 546572.792  | 728052.771   | 1.664     |
| 50     | 0.056     | 5.00          | 55.212          | 1200          | 546624.464  | 728100.273   | 1.560     |
| 51     | 0.048     | 5.00          | 54.543          | 1200          | 546696.092  | 728152.365   | 2.121     |
| 40     | 0.044     | 5.00          | 57.033          |               | 546526.008  | 728258.431   | 1.050     |
| 53     | 0.044     | 5.00          | 52.995          | 1200          | 546745.329  | 728206.618   | 1.775     |
| 68     |           | 5.00          | 51.108          | 1200          | 546721.109  | 728183.949   | 0.680     |
| 54     | 0.016     | 5.00          | 53.563          | 1200          | 546695.858  | 728245.794   | 2.869     |
| 68_OUT |           |               | 51.108          | 1200          | 546723.869  | 728181.369   | 0.717     |
| 67     |           |               | 52.980          | 1200          | 546695.996  | 728204.581   | 2.543     |
| 67_OUT | 0.057     |               | 51.108          | 1200          | 546698.578  | 728202.431   | 0.680     |
| 10     | 0.026     | 5.00          | 56.308          | 1200          | 546489.685  | 727969.396   | 0.900     |
| 11     | 0.017     | 5.00          | 55.306          | 1200          | 546458.111  | 727942.365   | 0.900     |
| 48     |           |               | 55.982          | 1200          | 546560.006  | 728047.986   | 1.589     |
| 47     | 0.022     | 5.00          | 56.176          | 1200          | 546541.540  | 728058.978   | 1.425     |
| 52     | 0.018     | 5.00          | 53.102          | 1200          | 546742.466  | 728197.796   | 1.575     |
| 25     | 1.062     | 5.00          | 56.425          | 1200          | 546515.102  | 728044.830   | 1.725     |
| 26     |           |               | 55.911          | 1200          | 546568.842  | 728108.690   | 1.725     |

**Nodes**

| Name   | Area (ha) | T of E (mins) | Cover Level (m) | Diameter (mm) | Easting (m) | Northing (m) | Depth (m) |
|--------|-----------|---------------|-----------------|---------------|-------------|--------------|-----------|
| 27     |           |               | 55.329          | 1500          | 546624.649  | 728174.829   | 1.725     |
| 30     |           |               | 55.259          | 1500          | 546626.506  | 728170.450   | 2.184     |
| 28     | 0.156     | 5.00          | 56.283          | 1200          | 546526.572  | 728052.622   | 1.500     |
| 29     | 0.078     | 5.00          | 55.784          | 1200          | 546577.586  | 728114.511   | 1.500     |
| 36     |           |               | 55.213          | 1500          | 546630.862  | 728175.555   | 4.146     |
| 36_OUT |           |               | 55.385          | 1200          | 546635.223  | 728171.525   | 4.330     |
| 35     |           |               | 54.081          | 1200          | 546669.037  | 728222.328   | 2.386     |
| 42     |           |               | 56.176          | 1200          | 546591.384  | 728341.483   | 2.152     |
| 24     | 0.117     | 5.00          | 55.303          | 1500          | 546624.981  | 728172.351   | 3.062     |
| 34     |           |               | 53.605          | 1200          | 546681.560  | 728224.386   | 1.825     |
| 31     | 0.043     | 5.00          | 53.217          | 1200          | 546700.336  | 728210.039   | 0.750     |
| 32     | 0.006     | 5.00          | 53.225          | 1200          | 546715.293  | 728228.218   | 0.993     |
| 33     | 0.057     | 5.00          | 53.518          | 1200          | 546696.736  | 728242.848   | 1.597     |
| 66     |           |               | 53.672          | 1200          | 546677.753  | 728219.758   | 3.156     |
| 44     |           |               | 54.341          |               | 546645.968  | 728303.279   | 1.103     |
| 43     |           |               | 56.605          |               | 546605.537  | 728337.243   | 2.695     |
| 45     |           |               | 53.633          | 1200          | 546690.672  | 728265.595   | 1.323     |
| 18     | 0.055     | 5.00          | 56.512          | 1200          | 546506.789  | 728039.440   | 1.866     |
| 9      |           |               | 56.045          | 1200          | 546433.927  | 728015.493   | 2.291     |
| 14     |           |               | 55.981          | 1200          | 546442.581  | 728008.872   | 2.311     |
| 13     |           |               | 56.010          | 1200          | 546428.017  | 727990.813   | 2.190     |
| 61     | 0.007     | 5.00          | 53.608          | 450           | 546679.614  | 728199.691   | 0.700     |
| 62     |           |               | 53.874          | 450           | 546673.333  | 728204.719   | 1.092     |
| 64     |           |               | 53.892          | 1200          | 546678.561  | 728211.123   | 1.159     |
| 63     | 0.009     | 5.00          | 53.660          | 450           | 546684.743  | 728206.020   | 0.700     |

**Links**

| Name | US Node | DS Node | Length (m) | ks (mm) / n | US IL (m) | DS IL (m) | Fall (m) | Slope (1:X) | Dia (mm) | T of C (mins) | Rain (mm/hr) |
|------|---------|---------|------------|-------------|-----------|-----------|----------|-------------|----------|---------------|--------------|
| 1    | 1       | 2       | 62.781     | 1.500       | 55.963    | 55.480    | 0.483    | 130.0       | 150      | 6.36          | 51.8         |
| 2    | 2       | 4       | 9.193      | 0.600       | 55.405    | 55.334    | 0.071    | 130.0       | 225      | 6.50          | 51.3         |
| 3    | 3       | 4       | 68.055     | 1.500       | 56.415    | 55.334    | 1.081    | 63.0        | 150      | 6.03          | 52.9         |
| 4    | 4       | 5       | 77.150     | 1.500       | 55.334    | 54.741    | 0.593    | 130.0       | 150      | 8.17          | 46.7         |
| 5    | 5       | 6       | 53.921     | 1.500       | 54.741    | 54.326    | 0.415    | 130.0       | 150      | 9.34          | 44.1         |
| 6    | 6       | 7       | 38.493     | 1.500       | 54.326    | 54.030    | 0.296    | 130.0       | 150      | 10.18         | 42.4         |
| 7    | 7       | 8       | 25.174     | 1.500       | 54.030    | 53.836    | 0.194    | 130.0       | 150      | 10.73         | 41.4         |
| 8    | 8       | 9       | 10.626     | 1.500       | 53.836    | 53.754    | 0.082    | 130.0       | 150      | 10.96         | 41.0         |

| Name | Vel (m/s) | Cap (l/s) | Flow (l/s) | US Depth (m) | DS Depth (m) | Σ Area (ha) | Σ Add Inflow (l/s) | Pro Depth (mm) | Pro Velocity (m/s) |
|------|-----------|-----------|------------|--------------|--------------|-------------|--------------------|----------------|--------------------|
| 1    | 0.767     | 13.6      | 6.2        | 0.900        | 1.722        | 0.033       | 0.0                | 71             | 0.750              |
| 2    | 1.145     | 45.5      | 6.2        | 1.722        | 1.824        | 0.033       | 0.0                | 56             | 0.805              |
| 3    | 1.105     | 19.5      | 14.7       | 0.900        | 1.899        | 0.077       | 0.0                | 98             | 1.216              |
| 4    | 0.767     | 13.6      | 27.6       | 1.899        | 1.967        | 0.163       | 0.0                | 150            | 0.782              |
| 5    | 0.767     | 13.6      | 35.0       | 1.967        | 1.975        | 0.220       | 0.0                | 150            | 0.782              |
| 6    | 0.767     | 13.6      | 38.1       | 1.975        | 1.959        | 0.249       | 0.0                | 150            | 0.782              |
| 7    | 0.767     | 13.6      | 46.0       | 1.959        | 2.075        | 0.308       | 0.0                | 150            | 0.782              |
| 8    | 0.767     | 13.6      | 49.1       | 2.075        | 2.141        | 0.332       | 0.0                | 150            | 0.782              |

Links

| Name | US Node | DS Node | Length (m) | ks (mm) / n | US IL (m) | DS IL (m) | Fall (m) | Slope (1:X) | Dia (mm) | T of C (mins) | Rain (mm/hr) |
|------|---------|---------|------------|-------------|-----------|-----------|----------|-------------|----------|---------------|--------------|
| 9    | 9       | 14      | 10.896     | 1.500       | 53.754    | 53.670    | 0.084    | 130.0       | 150      | 11.19         | 40.6         |
| 10   | 10      | 11      | 41.564     | 1.500       | 55.408    | 54.406    | 1.002    | 41.5        | 150      | 5.51          | 54.7         |
| 11   | 11      | 12      | 54.103     | 0.600       | 54.406    | 53.990    | 0.416    | 130.0       | 150      | 6.53          | 51.2         |
| 12   | 12      | 13      | 12.317     | 1.500       | 53.990    | 53.895    | 0.095    | 130.0       | 150      | 6.80          | 50.4         |
| 13   | 13      | 14      | 23.200     | 1.500       | 53.820    | 53.670    | 0.150    | 154.7       | 225      | 7.22          | 49.2         |
| 14   | 14      | 15      | 51.209     | 1.500       | 53.670    | 53.276    | 0.394    | 130.0       | 150      | 12.31         | 38.8         |
| 15   | 15      | 21      | 34.193     | 0.600       | 53.276    | 53.013    | 0.263    | 130.0       | 150      | 12.95         | 37.8         |
| 16   | 16      | 17      | 80.603     | 1.500       | 55.488    | 54.682    | 0.806    | 100.0       | 150      | 6.53          | 51.2         |
| 17   | 17      | 18      | 3.630      | 1.500       | 54.682    | 54.646    | 0.036    | 100.0       | 150      | 6.60          | 51.0         |
| 18   | 18      | 21      | 14.288     | 0.600       | 54.646    | 54.503    | 0.143    | 100.0       | 150      | 6.84          | 50.3         |
| 21   | 21      | 22      | 43.401     | 0.600       | 52.788    | 52.664    | 0.124    | 350.0       | 375      | 13.71         | 36.8         |
| 22   | 22      | 23      | 88.873     | 0.600       | 52.664    | 52.410    | 0.254    | 350.0       | 375      | 15.24         | 34.9         |
| 23   | 23      | 24      | 59.037     | 0.600       | 52.410    | 52.241    | 0.169    | 350.0       | 375      | 16.27         | 33.8         |
| 24   | 24      | 36      | 6.697      | 0.600       | 52.241    | 52.203    | 0.038    | 175.0       | 375      | 16.35         | 33.7         |
| 25   | 25      | 26      | 83.463     | 0.600       | 54.700    | 54.186    | 0.514    | 162.4       | 525      | 5.79          | 53.7         |
| 26   | 26      | 27      | 86.541     | 0.600       | 54.186    | 53.604    | 0.582    | 148.7       | 525      | 6.58          | 51.1         |
| 27   | 27      | 36      | 6.255      | 0.600       | 53.604    | 53.488    | 0.116    | 53.9        | 525      | 6.61          | 51.0         |
| 28   | 28      | 29      | 80.204     | 0.600       | 54.783    | 54.284    | 0.499    | 160.7       | 300      | 6.08          | 52.7         |
| 29   | 29      | 30      | 74.312     | 0.600       | 54.284    | 53.075    | 1.209    | 61.5        | 300      | 6.70          | 50.7         |
| 30   | 30      | 36      | 6.711      | 0.600       | 53.075    | 53.010    | 0.065    | 103.2       | 300      | 6.77          | 50.5         |
| 31   | 31      | 32      | 23.541     | 0.600       | 52.467    | 52.232    | 0.235    | 100.0       | 150      | 5.39          | 55.1         |
| 32   | 32      | 33      | 23.630     | 0.600       | 52.232    | 51.996    | 0.236    | 100.0       | 150      | 5.78          | 53.7         |
| 33   | 33      | 34      | 23.899     | 0.600       | 51.921    | 51.780    | 0.141    | 170.0       | 225      | 6.18          | 52.4         |

| Name | Vel (m/s) | Cap (l/s) | Flow (l/s) | US Depth (m) | DS Depth (m) | Σ Area (ha) | Σ Add Inflow (l/s) | Pro Depth (mm) | Pro Velocity (m/s) |
|------|-----------|-----------|------------|--------------|--------------|-------------|--------------------|----------------|--------------------|
| 9    | 0.767     | 13.6      | 48.7       | 2.141        | 2.161        | 0.332       | 0.0                | 150            | 0.782              |
| 10   | 1.363     | 24.1      | 5.2        | 0.750        | 0.750        | 0.026       | 0.0                | 47             | 1.081              |
| 11   | 0.880     | 15.5      | 7.9        | 0.750        | 1.916        | 0.043       | 0.0                | 76             | 0.884              |
| 12   | 0.767     | 13.6      | 7.8        | 1.916        | 1.965        | 0.043       | 0.0                | 82             | 0.795              |
| 13   | 0.922     | 36.7      | 7.6        | 1.965        | 2.086        | 0.043       | 0.0                | 70             | 0.729              |
| 14   | 0.767     | 13.6      | 52.5       | 2.161        | 3.296        | 0.375       | 0.0                | 150            | 0.782              |
| 15   | 0.880     | 15.5      | 51.2       | 3.296        | 3.342        | 0.375       | 0.0                | 150            | 0.896              |
| 16   | 0.876     | 15.5      | 5.2        | 1.200        | 1.661        | 0.028       | 0.0                | 60             | 0.789              |
| 17   | 0.876     | 15.5      | 7.8        | 1.661        | 1.716        | 0.042       | 0.0                | 75             | 0.877              |
| 18   | 1.005     | 17.8      | 17.6       | 1.716        | 1.852        | 0.097       | 0.0                | 122            | 1.142              |
| 21   | 0.963     | 106.3     | 68.8       | 3.342        | 3.244        | 0.518       | 0.0                | 220            | 1.022              |
| 22   | 0.963     | 106.3     | 72.6       | 3.244        | 2.921        | 0.576       | 0.0                | 228            | 1.033              |
| 23   | 0.963     | 106.3     | 77.9       | 2.921        | 2.687        | 0.639       | 0.0                | 239            | 1.048              |
| 24   | 1.366     | 150.9     | 91.9       | 2.687        | 2.635        | 0.755       | 0.0                | 211            | 1.430              |
| 25   | 1.755     | 379.9     | 205.9      | 1.200        | 1.200        | 1.062       | 0.0                | 276            | 1.788              |
| 26   | 1.834     | 397.1     | 196.1      | 1.200        | 1.200        | 1.062       | 0.0                | 261            | 1.829              |
| 27   | 3.055     | 661.2     | 195.7      | 1.200        | 1.200        | 1.062       | 0.0                | 195            | 2.677              |
| 28   | 1.237     | 87.5      | 29.8       | 1.200        | 1.200        | 0.156       | 0.0                | 120            | 1.122              |
| 29   | 2.009     | 142.0     | 43.0       | 1.200        | 1.884        | 0.234       | 0.0                | 113            | 1.767              |
| 30   | 1.547     | 109.3     | 42.8       | 1.884        | 1.903        | 0.234       | 0.0                | 130            | 1.456              |
| 31   | 1.005     | 17.8      | 8.6        | 0.600        | 0.843        | 0.043       | 0.0                | 74             | 0.996              |
| 32   | 1.005     | 17.8      | 9.6        | 0.843        | 1.372        | 0.049       | 0.0                | 78             | 1.022              |
| 33   | 1.000     | 39.7      | 20.1       | 1.372        | 1.600        | 0.106       | 0.0                | 114            | 1.004              |

Links

| Name | US Node | DS Node | Length (m) | ks (mm) / n | US IL (m) | DS IL (m) | Fall (m) | Slope (1:X) | Dia (mm) | T of C (mins) | Rain (mm/hr) |
|------|---------|---------|------------|-------------|-----------|-----------|----------|-------------|----------|---------------|--------------|
| 34   | 34      | 35      | 12.691     | 0.600       | 51.780    | 51.695    | 0.085    | 150.0       | 225      | 6.38          | 51.7         |
| 35   | 35      | 36      | 60.374     | 0.600       | 51.695    | 51.292    | 0.403    | 149.8       | 225      | 7.32          | 48.9         |
| 36   | 36      | 36_OUT  | 5.938      | 0.600       | 51.067    | 51.055    | 0.012    | 500.0       | 525      | 16.45         | 33.6         |
| 37   | 37      | 38      | 38.012     | 1.500       | 56.040    | 55.660    | 0.380    | 100.0       | 150      | 5.72          | 53.9         |
| 38   | 38      | 39      | 69.067     | 1.500       | 55.660    | 54.969    | 0.691    | 100.0       | 150      | 7.04          | 49.7         |
| 39   | 39      | 41      | 81.848     | 1.500       | 54.969    | 54.151    | 0.818    | 100.0       | 150      | 8.60          | 45.7         |
| 40   | 40      | 41      | 97.583     | 1.500       | 55.983    | 54.151    | 1.832    | 53.3        | 150      | 6.35          | 51.8         |
| 41   | 41      | 42      | 8.759      | 1.500       | 54.076    | 54.024    | 0.052    | 170.0       | 225      | 8.76          | 45.3         |
| 42   | 42      | 43      | 14.774     | 1.500       | 54.024    | 53.910    | 0.114    | 130.0       | 150      | 9.08          | 44.6         |
| 43   | 43      | 44      | 52.804     | 1.500       | 53.910    | 53.238    | 0.672    | 78.6        | 150      | 9.97          | 42.8         |
| 44   | 44      | 45      | 58.468     | 1.500       | 53.238    | 52.385    | 0.853    | 68.5        | 150      | 10.89         | 41.1         |
| 45   | 45      | 46      | 9.408      | 1.500       | 52.310    | 52.238    | 0.072    | 130.0       | 225      | 11.05         | 40.8         |
| 46   | 46      | 55      | 12.074     | 0.600       | 52.238    | 52.145    | 0.093    | 130.0       | 225      | 11.22         | 40.5         |
| 47   | 47      | 48      | 21.490     | 0.600       | 54.751    | 54.393    | 0.358    | 60.0        | 225      | 5.21          | 55.8         |
| 48   | 48      | 49      | 13.652     | 0.600       | 54.393    | 54.165    | 0.228    | 60.0        | 225      | 5.35          | 55.3         |
| 49   | 49      | 50      | 70.399     | 1.500       | 54.198    | 53.652    | 0.546    | 128.9       | 225      | 6.51          | 51.3         |
| 50   | 50      | 51      | 88.595     | 1.500       | 53.652    | 52.572    | 1.080    | 82.0        | 225      | 7.67          | 48.0         |
| 51   | 51      | 52      | 64.994     | 1.500       | 52.422    | 51.527    | 0.895    | 72.6        | 375      | 8.25          | 46.5         |
| 52   | 52      | 53      | 9.279      | 0.600       | 51.527    | 51.220    | 0.307    | 30.2        | 375      | 8.29          | 46.4         |
| 53   | 53      | 54      | 63.104     | 0.600       | 51.220    | 50.694    | 0.526    | 120.0       | 375      | 8.93          | 45.0         |
| 54   | 54      | 55      | 10.216     | 1.500       | 50.694    | 50.660    | 0.034    | 300.0       | 375      | 9.12          | 44.6         |
| 55   | 55      | 60      | 25.692     | 0.600       | 50.656    | 50.551    | 0.105    | 244.7       | 375      | 11.60         | 39.9         |
| 24a  | 24      | 59      | 9.833      | 0.600       | 52.241    | 52.183    | 0.058    | 170.0       | 375      | 5.12          | 56.2         |
| 27a  | 27      | 59      | 8.368      | 0.600       | 53.604    | 53.588    | 0.016    | 520.0       | 525      | 5.14          | 56.1         |

| Name | Vel (m/s) | Cap (l/s) | Flow (l/s) | US Depth (m) | DS Depth (m) | Σ Area (ha) | Σ Add Inflow (l/s) | Pro Depth (mm) | Pro Velocity (m/s) |
|------|-----------|-----------|------------|--------------|--------------|-------------|--------------------|----------------|--------------------|
| 34   | 1.065     | 42.3      | 19.9       | 1.600        | 2.161        | 0.106       | 0.0                | 109            | 1.049              |
| 35   | 1.066     | 42.4      | 18.8       | 2.161        | 3.696        | 0.106       | 0.0                | 105            | 1.035              |
| 36   | 0.995     | 215.3     | 261.8      | 3.621        | 3.805        | 2.158       | 0.0                | 525            | 1.004              |
| 37   | 0.876     | 15.5      | 4.7        | 0.900        | 1.473        | 0.024       | 0.0                | 57             | 0.765              |
| 38   | 0.876     | 15.5      | 15.1       | 1.473        | 1.484        | 0.084       | 0.0                | 120            | 0.999              |
| 39   | 0.876     | 15.5      | 28.0       | 1.484        | 1.751        | 0.169       | 0.0                | 150            | 0.893              |
| 40   | 1.202     | 21.2      | 8.2        | 0.900        | 1.751        | 0.044       | 0.0                | 65             | 1.124              |
| 41   | 0.879     | 35.0      | 48.4       | 1.751        | 1.927        | 0.295       | 0.0                | 225            | 0.896              |
| 42   | 0.767     | 13.6      | 47.6       | 2.002        | 2.545        | 0.295       | 0.0                | 150            | 0.782              |
| 43   | 0.989     | 17.5      | 45.7       | 2.545        | 0.953        | 0.295       | 0.0                | 150            | 1.008              |
| 44   | 1.059     | 18.7      | 43.8       | 0.953        | 1.098        | 0.295       | 0.0                | 150            | 1.079              |
| 45   | 1.006     | 40.0      | 43.6       | 1.098        | 1.443        | 0.295       | 0.0                | 225            | 1.025              |
| 46   | 1.145     | 45.5      | 44.4       | 1.443        | 1.294        | 0.304       | 0.0                | 181            | 1.299              |
| 47   | 1.691     | 67.2      | 4.5        | 1.200        | 1.364        | 0.022       | 0.0                | 39             | 0.967              |
| 48   | 1.691     | 67.2      | 4.4        | 1.364        | 1.439        | 0.022       | 0.0                | 39             | 0.967              |
| 49   | 1.010     | 40.2      | 13.4       | 1.406        | 1.335        | 0.072       | 0.0                | 89             | 0.908              |
| 50   | 1.268     | 50.4      | 22.2       | 1.335        | 1.746        | 0.128       | 0.0                | 104            | 1.226              |
| 51   | 1.883     | 207.9     | 29.6       | 1.746        | 1.200        | 0.176       | 0.0                | 96             | 1.342              |
| 52   | 3.306     | 365.1     | 32.6       | 1.200        | 1.400        | 0.195       | 0.0                | 75             | 2.076              |
| 53   | 1.653     | 182.5     | 38.7       | 1.400        | 2.494        | 0.238       | 0.0                | 117            | 1.323              |
| 54   | 0.924     | 102.0     | 40.9       | 2.494        | 2.629        | 0.254       | 0.0                | 165            | 0.874              |
| 55   | 1.154     | 127.4     | 87.7       | 2.633        | 3.154        | 0.609       | 0.0                | 229            | 1.240              |
| 24a  | 1.386     | 153.1     | 0.0        | 2.687        | 2.678        | 0.000       | 0.0                | 0              | 0.000              |
| 27a  | 0.975     | 211.1     | 0.0        | 1.200        | 1.123        | 0.000       | 0.0                | 0              | 0.000              |

Links

| Name | US Node | DS Node | Length (m) | ks (mm) / n | US IL (m) | DS IL (m) | Fall (m) | Slope (1:X) | Dia (mm) | T of C (mins) | Rain (mm/hr) |
|------|---------|---------|------------|-------------|-----------|-----------|----------|-------------|----------|---------------|--------------|
| 30a  | 30      | 59      | 10.579     | 0.600       | 53.075    | 52.899    | 0.176    | 60.0        | 300      | 5.09          | 56.3         |
| 59   | 59      | 60      | 60.346     | 0.600       | 52.183    | 51.843    | 0.340    | 177.5       | 375      | 5.88          | 53.4         |
| 60   | 60      | 66      | 10.433     | 0.600       | 50.551    | 50.516    | 0.035    | 300.2       | 375      | 11.76         | 39.6         |
| 61   | 61      | 62      | 8.045      | 0.600       | 52.908    | 52.828    | 0.080    | 100.0       | 100      | 5.17          | 56.0         |
| 62   | 62      | 64      | 8.267      | 0.600       | 52.782    | 52.733    | 0.049    | 170.0       | 225      | 5.31          | 55.4         |
| 63   | 63      | 64      | 8.017      | 0.600       | 52.960    | 52.858    | 0.102    | 78.6        | 100      | 5.15          | 56.1         |
| 64   | 64      | 66      | 8.673      | 0.600       | 52.733    | 52.547    | 0.186    | 46.6        | 225      | 5.39          | 55.1         |
| 34a  | 34      | 66      | 5.993      | 0.600       | 51.780    | 51.720    | 0.060    | 100.0       | 225      | 5.08          | 56.4         |
| 66   | 66      | 67      | 23.732     | 0.600       | 50.516    | 50.437    | 0.079    | 300.2       | 375      | 12.14         | 39.0         |
| 67   | 67      | 67_OUT  | 3.360      | 0.600       | 50.437    | 50.428    | 0.009    | 373.3       | 375      | 12.20         | 38.9         |
| 68   | 68      | 68_OUT  | 3.778      | 0.600       | 50.428    | 50.391    | 0.037    | 102.1       | 225      | 5.05          | 56.5         |

| Name | Vel (m/s) | Cap (l/s) | Flow (l/s) | US Depth (m) | DS Depth (m) | Σ Area (ha) | Σ Add Inflow (l/s) | Pro Depth (mm) | Pro Velocity (m/s) |
|------|-----------|-----------|------------|--------------|--------------|-------------|--------------------|----------------|--------------------|
| 30a  | 2.033     | 143.7     | 0.0        | 1.884        | 2.037        | 0.000       | 0.0                | 0              | 0.000              |
| 59   | 1.357     | 149.8     | 12.5       | 2.678        | 1.862        | 0.065       | 0.0                | 73             | 0.835              |
| 60   | 1.040     | 114.9     | 98.9       | 3.154        | 2.781        | 0.691       | 0.0                | 269            | 1.164              |
| 61   | 0.769     | 6.0       | 1.5        | 0.600        | 0.946        | 0.007       | 0.0                | 34             | 0.637              |
| 62   | 1.000     | 39.7      | 1.5        | 0.867        | 0.934        | 0.007       | 0.0                | 29             | 0.477              |
| 63   | 0.869     | 6.8       | 1.7        | 0.600        | 0.934        | 0.009       | 0.0                | 35             | 0.729              |
| 64   | 1.920     | 76.3      | 3.2        | 0.934        | 0.900        | 0.016       | 0.0                | 31             | 0.956              |
| 34a  | 1.307     | 52.0      | 0.0        | 1.600        | 1.727        | 0.000       | 0.0                | 0              | 0.000              |
| 66   | 1.040     | 114.9     | 99.7       | 2.781        | 2.168        | 0.707       | 0.0                | 271            | 1.166              |
| 67   | 0.932     | 102.9     | 99.5       | 2.168        | 0.305        | 0.707       | 0.0                | 298            | 1.055              |
| 68   | 1.293     | 51.4      | 0.0        | 0.455        | 0.492        | 0.000       | 0.0                | 0              | 0.000              |

Pipeline Schedule

| Link | Length (m) | Slope (1:X) | Dia (mm) | Link Type    | US CL (m) | US IL (m) | US Depth (m) | DS CL (m) | DS IL (m) | DS Depth (m) |
|------|------------|-------------|----------|--------------|-----------|-----------|--------------|-----------|-----------|--------------|
| 1    | 62.781     | 130.0       | 150      | Filterdrain  | 57.013    | 55.963    | 0.900        | 57.352    | 55.480    | 1.722        |
| 2    | 9.193      | 130.0       | 225      | Carrierdrain | 57.352    | 55.405    | 1.722        | 57.383    | 55.334    | 1.824        |
| 3    | 68.055     | 63.0        | 150      | Filterdrain  | 57.465    | 56.415    | 0.900        | 57.383    | 55.334    | 1.899        |
| 4    | 77.150     | 130.0       | 150      | Filterdrain  | 57.383    | 55.334    | 1.899        | 56.858    | 54.741    | 1.967        |
| 5    | 53.921     | 130.0       | 150      | Filterdrain  | 56.858    | 54.741    | 1.967        | 56.451    | 54.326    | 1.975        |
| 6    | 38.493     | 130.0       | 150      | Filterdrain  | 56.451    | 54.326    | 1.975        | 56.139    | 54.030    | 1.959        |
| 7    | 25.174     | 130.0       | 150      | Filterdrain  | 56.139    | 54.030    | 1.959        | 56.061    | 53.836    | 2.075        |
| 8    | 10.626     | 130.0       | 150      | Filterdrain  | 56.061    | 53.836    | 2.075        | 56.045    | 53.754    | 2.141        |
| 9    | 10.896     | 130.0       | 150      | Filterdrain  | 56.045    | 53.754    | 2.141        | 55.981    | 53.670    | 2.161        |

| Link | US Node | Dia (mm) | Node Type | MH Type   | DS Node | Dia (mm) | Node Type | MH Type   |
|------|---------|----------|-----------|-----------|---------|----------|-----------|-----------|
| 1    | 1       |          | Junction  |           | 2       | 1200     | Manhole   | Adoptable |
| 2    | 2       | 1200     | Manhole   | Adoptable | 4       | 1200     | Manhole   | Adoptable |
| 3    | 3       |          | Junction  |           | 4       | 1200     | Manhole   | Adoptable |
| 4    | 4       | 1200     | Manhole   | Adoptable | 5       |          | Junction  |           |
| 5    | 5       |          | Junction  |           | 6       |          | Junction  |           |
| 6    | 6       |          | Junction  |           | 7       |          | Junction  |           |
| 7    | 7       |          | Junction  |           | 8       |          | Junction  |           |
| 8    | 8       |          | Junction  |           | 9       | 1200     | Manhole   | Adoptable |
| 9    | 9       | 1200     | Manhole   | Adoptable | 14      | 1200     | Manhole   | Adoptable |

**Pipeline Schedule**

| Link | Length (m) | Slope (1:X) | Dia (mm) | Link Type    | US CL (m) | US IL (m) | US Depth (m) | DS CL (m) | DS IL (m) | DS Depth (m) |
|------|------------|-------------|----------|--------------|-----------|-----------|--------------|-----------|-----------|--------------|
| 10   | 41.564     | 41.5        | 150      | Filterdrain  | 56.308    | 55.408    | 0.750        | 55.306    | 54.406    | 0.750        |
| 11   | 54.103     | 130.0       | 150      | Carrierdrain | 55.306    | 54.406    | 0.750        | 56.056    | 53.990    | 1.916        |
| 12   | 12.317     | 130.0       | 150      | Filterdrain  | 56.056    | 53.990    | 1.916        | 56.010    | 53.895    | 1.965        |
| 13   | 23.200     | 154.7       | 225      | Filterdrain  | 56.010    | 53.820    | 1.965        | 55.981    | 53.670    | 2.086        |
| 14   | 51.209     | 130.0       | 150      | Filterdrain  | 55.981    | 53.670    | 2.161        | 56.722    | 53.276    | 3.296        |
| 15   | 34.193     | 130.0       | 150      | Carrierdrain | 56.722    | 53.276    | 3.296        | 56.505    | 53.013    | 3.342        |
| 16   | 80.603     | 100.0       | 150      | Filterdrain  | 56.838    | 55.488    | 1.200        | 56.493    | 54.682    | 1.661        |
| 17   | 3.630      | 100.0       | 150      | Filterdrain  | 56.493    | 54.682    | 1.661        | 56.512    | 54.646    | 1.716        |
| 18   | 14.288     | 100.0       | 150      | Carrierdrain | 56.512    | 54.646    | 1.716        | 56.505    | 54.503    | 1.852        |
| 21   | 43.401     | 350.0       | 375      | Carrierdrain | 56.505    | 52.788    | 3.342        | 56.283    | 52.664    | 3.244        |
| 22   | 88.873     | 350.0       | 375      | Carrierdrain | 56.283    | 52.664    | 3.244        | 55.706    | 52.410    | 2.921        |
| 23   | 59.037     | 350.0       | 375      | Carrierdrain | 55.706    | 52.410    | 2.921        | 55.303    | 52.241    | 2.687        |
| 24   | 6.697      | 175.0       | 375      | Carrierdrain | 55.303    | 52.241    | 2.687        | 55.213    | 52.203    | 2.635        |
| 25   | 83.463     | 162.4       | 525      | Carrierdrain | 56.425    | 54.700    | 1.200        | 55.911    | 54.186    | 1.200        |
| 26   | 86.541     | 148.7       | 525      | Carrierdrain | 55.911    | 54.186    | 1.200        | 55.329    | 53.604    | 1.200        |
| 27   | 6.255      | 53.9        | 525      | Carrierdrain | 55.329    | 53.604    | 1.200        | 55.213    | 53.488    | 1.200        |
| 28   | 80.204     | 160.7       | 300      | Carrierdrain | 56.283    | 54.783    | 1.200        | 55.784    | 54.284    | 1.200        |
| 29   | 74.312     | 61.5        | 300      | Carrierdrain | 55.784    | 54.284    | 1.200        | 55.259    | 53.075    | 1.884        |
| 30   | 6.711      | 103.2       | 300      | Carrierdrain | 55.259    | 53.075    | 1.884        | 55.213    | 53.010    | 1.903        |
| 31   | 23.541     | 100.0       | 150      | Carrierdrain | 53.217    | 52.467    | 0.600        | 53.225    | 52.232    | 0.843        |
| 32   | 23.630     | 100.0       | 150      | Carrierdrain | 53.225    | 52.232    | 0.843        | 53.518    | 51.996    | 1.372        |
| 33   | 23.899     | 170.0       | 225      | Carrierdrain | 53.518    | 51.921    | 1.372        | 53.605    | 51.780    | 1.600        |
| 34   | 12.691     | 150.0       | 225      | Carrierdrain | 53.605    | 51.780    | 1.600        | 54.081    | 51.695    | 2.161        |
| 35   | 60.374     | 149.8       | 225      | Carrierdrain | 54.081    | 51.695    | 2.161        | 55.213    | 51.292    | 3.696        |

| Link | US Node | Dia (mm) | Node Type | MH Type   | DS Node | Dia (mm) | Node Type | MH Type   |
|------|---------|----------|-----------|-----------|---------|----------|-----------|-----------|
| 10   | 10      | 1200     | Manhole   | Adoptable | 11      | 1200     | Manhole   | Adoptable |
| 11   | 11      | 1200     | Manhole   | Adoptable | 12      | 1200     | Manhole   | Adoptable |
| 12   | 12      | 1200     | Manhole   | Adoptable | 13      | 1200     | Manhole   | Adoptable |
| 13   | 13      | 1200     | Manhole   | Adoptable | 14      | 1200     | Manhole   | Adoptable |
| 14   | 14      | 1200     | Manhole   | Adoptable | 15      | 1200     | Manhole   | Adoptable |
| 15   | 15      | 1200     | Manhole   | Adoptable | 21      | 1200     | Manhole   | Adoptable |
| 16   | 16      | 1200     | Manhole   | Adoptable | 17      | 1200     | Manhole   | Adoptable |
| 17   | 17      | 1200     | Manhole   | Adoptable | 18      | 1200     | Manhole   | Adoptable |
| 18   | 18      | 1200     | Manhole   | Adoptable | 21      | 1200     | Manhole   | Adoptable |
| 21   | 21      | 1200     | Manhole   | Adoptable | 22      | 1200     | Manhole   | Adoptable |
| 22   | 22      | 1200     | Manhole   | Adoptable | 23      | 1200     | Manhole   | Adoptable |
| 23   | 23      | 1200     | Manhole   | Adoptable | 24      | 1500     | Manhole   | Adoptable |
| 24   | 24      | 1500     | Manhole   | Adoptable | 36      | 1500     | Manhole   | Adoptable |
| 25   | 25      | 1200     | Manhole   | Adoptable | 26      | 1200     | Manhole   | Adoptable |
| 26   | 26      | 1200     | Manhole   | Adoptable | 27      | 1500     | Manhole   | Adoptable |
| 27   | 27      | 1500     | Manhole   | Adoptable | 36      | 1500     | Manhole   | Adoptable |
| 28   | 28      | 1200     | Manhole   | Adoptable | 29      | 1200     | Manhole   | Adoptable |
| 29   | 29      | 1200     | Manhole   | Adoptable | 30      | 1500     | Manhole   | Adoptable |
| 30   | 30      | 1500     | Manhole   | Adoptable | 36      | 1500     | Manhole   | Adoptable |
| 31   | 31      | 1200     | Manhole   | Adoptable | 32      | 1200     | Manhole   | Adoptable |
| 32   | 32      | 1200     | Manhole   | Adoptable | 33      | 1200     | Manhole   | Adoptable |
| 33   | 33      | 1200     | Manhole   | Adoptable | 34      | 1200     | Manhole   | Adoptable |
| 34   | 34      | 1200     | Manhole   | Adoptable | 35      | 1200     | Manhole   | Adoptable |
| 35   | 35      | 1200     | Manhole   | Adoptable | 36      | 1500     | Manhole   | Adoptable |

**Pipeline Schedule**

| Link | Length (m) | Slope (1:X) | Dia (mm) | Link Type    | US CL (m) | US IL (m) | US Depth (m) | DS CL (m) | DS IL (m) | DS Depth (m) |
|------|------------|-------------|----------|--------------|-----------|-----------|--------------|-----------|-----------|--------------|
| 36   | 5.938      | 500.0       | 525      | Carrierdrain | 55.213    | 51.067    | 3.621        | 55.385    | 51.055    | 3.805        |
| 37   | 38.012     | 100.0       | 150      | Filterdrain  | 57.090    | 56.040    | 0.900        | 57.283    | 55.660    | 1.473        |
| 38   | 69.067     | 100.0       | 150      | Filterdrain  | 57.283    | 55.660    | 1.473        | 56.603    | 54.969    | 1.484        |
| 39   | 81.848     | 100.0       | 150      | Filterdrain  | 56.603    | 54.969    | 1.484        | 56.052    | 54.151    | 1.751        |
| 40   | 97.583     | 53.3        | 150      | Filterdrain  | 57.033    | 55.983    | 0.900        | 56.052    | 54.151    | 1.751        |
| 41   | 8.759      | 170.0       | 225      | Carrierdrain | 56.052    | 54.076    | 1.751        | 56.176    | 54.024    | 1.927        |
| 42   | 14.774     | 130.0       | 150      | Filterdrain  | 56.176    | 54.024    | 2.002        | 56.605    | 53.910    | 2.545        |
| 43   | 52.804     | 78.6        | 150      | Filterdrain  | 56.605    | 53.910    | 2.545        | 54.341    | 53.238    | 0.953        |
| 44   | 58.468     | 68.5        | 150      | Filterdrain  | 54.341    | 53.238    | 0.953        | 53.633    | 52.385    | 1.098        |
| 45   | 9.408      | 130.0       | 225      | Filterdrain  | 53.633    | 52.310    | 1.098        | 53.906    | 52.238    | 1.443        |
| 46   | 12.074     | 130.0       | 225      | Carrierdrain | 53.906    | 52.238    | 1.443        | 53.664    | 52.145    | 1.294        |
| 47   | 21.490     | 60.0        | 225      | Carrierdrain | 56.176    | 54.751    | 1.200        | 55.982    | 54.393    | 1.364        |
| 48   | 13.652     | 60.0        | 225      | Carrierdrain | 55.982    | 54.393    | 1.364        | 55.829    | 54.165    | 1.439        |
| 49   | 70.399     | 128.9       | 225      | Filterdrain  | 55.829    | 54.198    | 1.406        | 55.212    | 53.652    | 1.335        |
| 50   | 88.595     | 82.0        | 225      | Filterdrain  | 55.212    | 53.652    | 1.335        | 54.543    | 52.572    | 1.746        |
| 51   | 64.994     | 72.6        | 375      | Filterdrain  | 54.543    | 52.422    | 1.746        | 53.102    | 51.527    | 1.200        |
| 52   | 9.279      | 30.2        | 375      | Carrierdrain | 53.102    | 51.527    | 1.200        | 52.995    | 51.220    | 1.400        |
| 53   | 63.104     | 120.0       | 375      | Filterdrain  | 52.995    | 51.220    | 1.400        | 53.563    | 50.694    | 2.494        |
| 54   | 10.216     | 300.0       | 375      | Filterdrain  | 53.563    | 50.694    | 2.494        | 53.664    | 50.660    | 2.629        |
| 55   | 25.692     | 244.7       | 375      | Carrierdrain | 53.664    | 50.656    | 2.633        | 54.080    | 50.551    | 3.154        |
| 24a  | 9.833      | 170.0       | 375      | Carrierdrain | 55.303    | 52.241    | 2.687        | 55.236    | 52.183    | 2.678        |
| 27a  | 8.368      | 520.0       | 525      | Carrierdrain | 55.329    | 53.604    | 1.200        | 55.236    | 53.588    | 1.123        |
| 30a  | 10.579     | 60.0        | 300      | Carrierdrain | 55.259    | 53.075    | 1.884        | 55.236    | 52.899    | 2.037        |
| 59   | 60.346     | 177.5       | 375      | Carrierdrain | 55.236    | 52.183    | 2.678        | 54.080    | 51.843    | 1.862        |
| 60   | 10.433     | 300.2       | 375      | Carrierdrain | 54.080    | 50.551    | 3.154        | 53.672    | 50.516    | 2.781        |

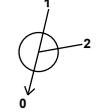
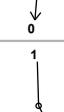
| Link | US Node | Dia (mm) | Node Type | MH Type   | DS Node | Dia (mm) | Node Type | MH Type   |
|------|---------|----------|-----------|-----------|---------|----------|-----------|-----------|
| 36   | 36      | 1500     | Manhole   | Adoptable | 36_OUT  | 1200     | Manhole   | Adoptable |
| 37   | 37      |          | Junction  |           | 38      | 1200     | Manhole   | Adoptable |
| 38   | 38      | 1200     | Manhole   | Adoptable | 39      | 1200     | Manhole   | Adoptable |
| 39   | 39      | 1200     | Manhole   | Adoptable | 41      | 1200     | Manhole   | Adoptable |
| 40   | 40      |          | Junction  |           | 41      | 1200     | Manhole   | Adoptable |
| 41   | 41      | 1200     | Manhole   | Adoptable | 42      | 1200     | Manhole   | Adoptable |
| 42   | 42      | 1200     | Manhole   | Adoptable | 43      |          | Junction  |           |
| 43   | 43      |          | Junction  |           | 44      |          | Junction  |           |
| 44   | 44      |          | Junction  |           | 45      | 1200     | Manhole   | Adoptable |
| 45   | 45      | 1200     | Manhole   | Adoptable | 46      | 1200     | Manhole   | Adoptable |
| 46   | 46      | 1200     | Manhole   | Adoptable | 55      | 1200     | Manhole   | Adoptable |
| 47   | 47      | 1200     | Manhole   | Adoptable | 48      | 1200     | Manhole   | Adoptable |
| 48   | 48      | 1200     | Manhole   | Adoptable | 49      | 1200     | Manhole   | Adoptable |
| 49   | 49      | 1200     | Manhole   | Adoptable | 50      | 1200     | Manhole   | Adoptable |
| 50   | 50      | 1200     | Manhole   | Adoptable | 51      | 1200     | Manhole   | Adoptable |
| 51   | 51      | 1200     | Manhole   | Adoptable | 52      | 1200     | Manhole   | Adoptable |
| 52   | 52      | 1200     | Manhole   | Adoptable | 53      | 1200     | Manhole   | Adoptable |
| 53   | 53      | 1200     | Manhole   | Adoptable | 54      | 1200     | Manhole   | Adoptable |
| 54   | 54      | 1200     | Manhole   | Adoptable | 55      | 1200     | Manhole   | Adoptable |
| 55   | 55      | 1200     | Manhole   | Adoptable | 60      | 1200     | Manhole   | Adoptable |
| 24a  | 24      | 1500     | Manhole   | Adoptable | 59      | 1200     | Manhole   | Adoptable |
| 27a  | 27      | 1500     | Manhole   | Adoptable | 59      | 1200     | Manhole   | Adoptable |
| 30a  | 30      | 1500     | Manhole   | Adoptable | 59      | 1200     | Manhole   | Adoptable |
| 59   | 59      | 1200     | Manhole   | Adoptable | 60      | 1200     | Manhole   | Adoptable |
| 60   | 60      | 1200     | Manhole   | Adoptable | 66      | 1200     | Manhole   | Adoptable |

**Pipeline Schedule**

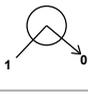
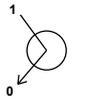
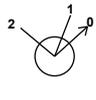
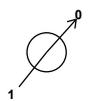
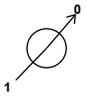
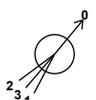
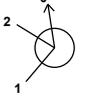
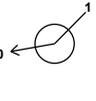
| Link | Length (m) | Slope (1:X) | Dia (mm) | Link Type    | US CL (m) | US IL (m) | US Depth (m) | DS CL (m) | DS IL (m) | DS Depth (m) |
|------|------------|-------------|----------|--------------|-----------|-----------|--------------|-----------|-----------|--------------|
| 61   | 8.045      | 100.0       | 100      | Carrierdrain | 53.608    | 52.908    | 0.600        | 53.874    | 52.828    | 0.946        |
| 62   | 8.267      | 170.0       | 225      | Carrierdrain | 53.874    | 52.782    | 0.867        | 53.892    | 52.733    | 0.934        |
| 63   | 8.017      | 78.6        | 100      | Carrierdrain | 53.660    | 52.960    | 0.600        | 53.892    | 52.858    | 0.934        |
| 64   | 8.673      | 46.6        | 225      | Carrierdrain | 53.892    | 52.733    | 0.934        | 53.672    | 52.547    | 0.900        |
| 34a  | 5.993      | 100.0       | 225      | Carrierdrain | 53.605    | 51.780    | 1.600        | 53.672    | 51.720    | 1.727        |
| 66   | 23.732     | 300.2       | 375      | Carrierdrain | 53.672    | 50.516    | 2.781        | 52.980    | 50.437    | 2.168        |
| 67   | 3.360      | 373.3       | 375      | Carrierdrain | 52.980    | 50.437    | 2.168        | 51.108    | 50.428    | 0.305        |
| 68   | 3.778      | 102.1       | 225      | Carrierdrain | 51.108    | 50.428    | 0.455        | 51.108    | 50.391    | 0.492        |

| Link | US Node | Dia (mm) | Node Type | MH Type   | DS Node | Dia (mm) | Node Type | MH Type   |
|------|---------|----------|-----------|-----------|---------|----------|-----------|-----------|
| 61   | 61      | 450      | Manhole   | Adoptable | 62      | 450      | Manhole   | Adoptable |
| 62   | 62      | 450      | Manhole   | Adoptable | 64      | 1200     | Manhole   | Adoptable |
| 63   | 63      | 450      | Manhole   | Adoptable | 64      | 1200     | Manhole   | Adoptable |
| 64   | 64      | 1200     | Manhole   | Adoptable | 66      | 1200     | Manhole   | Adoptable |
| 34a  | 34      | 1200     | Manhole   | Adoptable | 66      | 1200     | Manhole   | Adoptable |
| 66   | 66      | 1200     | Manhole   | Adoptable | 67      | 1200     | Manhole   | Adoptable |
| 67   | 67      | 1200     | Manhole   | Adoptable | 67_OUT  | 1200     | Manhole   | Adoptable |
| 68   | 68      | 1200     | Manhole   | Adoptable | 68_OUT  | 1200     | Manhole   | Adoptable |

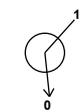
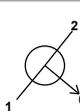
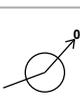
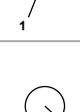
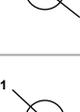
**Manhole Schedule**

| Node | Easting (m) | Northing (m) | CL (m) | Depth (m) | Dia (mm) | Connections  | Link | IL (m) | Dia (mm) |
|------|-------------|--------------|--------|-----------|----------|--|------|--------|----------|
| 3    | 546483.757  | 728254.957   | 57.465 | 1.050     |          |   |      |        |          |
|      |             |              |        |           |          | 0  | 3    | 56.415 | 150      |
| 1    | 546518.316  | 728237.837   | 57.013 | 1.050     |          |   |      |        |          |
|      |             |              |        |           |          | 0  | 1    | 55.963 | 150      |
| 4    | 546468.272  | 728188.687   | 57.383 | 2.049     | 1200     |  | 1    | 55.334 | 150      |
|      |             |              |        |           |          | 2  | 2    | 55.334 | 225      |
|      |             |              |        |           |          | 0  | 4    | 55.334 | 150      |
| 5    | 546441.692  | 728116.310   | 56.858 | 2.117     |          |  | 1    | 54.741 | 150      |
|      |             |              |        |           |          | 0  | 5    | 54.741 | 150      |
| 6    | 546417.414  | 728068.171   | 56.451 | 2.125     |          |  | 1    | 54.326 | 150      |
|      |             |              |        |           |          | 0  | 6    | 54.326 | 150      |
| 7    | 546415.612  | 728029.722   | 56.139 | 2.109     |          |  | 1    | 54.030 | 150      |
|      |             |              |        |           |          | 0  | 7    | 54.030 | 150      |
| 8    | 546427.121  | 728007.333   | 56.061 | 2.225     |          |  | 1    | 53.836 | 150      |
|      |             |              |        |           |          | 0  | 8    | 53.836 | 150      |

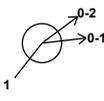
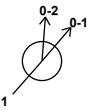
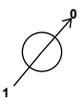
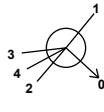
**Manhole Schedule**

| Node | Easting (m) | Northing (m) | CL (m) | Depth (m) | Dia (mm) | Connections  | Link  | IL (m) | Dia (mm) |
|------|-------------|--------------|--------|-----------|----------|--|-------|--------|----------|
| 12   | 546420.387  | 727981.144   | 56.056 | 2.066     | 1200     |    | 1 11  | 53.990 | 150      |
|      |             |              |        |           |          |  | 0 12  | 53.990 | 150      |
| 15   | 546475.478  | 728048.112   | 56.722 | 3.446     | 1200     |    | 1 14  | 53.276 | 150      |
|      |             |              |        |           |          |  | 0 15  | 53.276 | 150      |
| 16   | 546447.690  | 728094.346   | 56.838 | 1.350     | 1200     |    | 0 16  | 55.488 | 150      |
| 17   | 546509.135  | 728042.209   | 56.493 | 1.811     | 1200     |    | 1 16  | 54.682 | 150      |
|      |             |              |        |           |          |  | 0 17  | 54.682 | 150      |
| 21   | 546501.650  | 728026.108   | 56.505 | 3.717     | 1200     |    | 1 18  | 54.503 | 150      |
|      |             |              |        |           |          |  | 2 15  | 53.013 | 150      |
|      |             |              |        |           |          |  | 0 21  | 52.788 | 375      |
| 22   | 546529.759  | 728059.174   | 56.283 | 3.619     | 1200     |  | 1 21  | 52.664 | 375      |
|      |             |              |        |           |          |  | 0 22  | 52.664 | 375      |
| 23   | 546586.686  | 728127.419   | 55.706 | 3.296     | 1200     |  | 1 22  | 52.410 | 375      |
|      |             |              |        |           |          |  | 0 23  | 52.410 | 375      |
| 59   | 546631.348  | 728179.844   | 55.236 | 3.053     | 1200     |  | 1 30a | 52.899 | 300      |
|      |             |              |        |           |          |  | 2 27a | 53.588 | 525      |
|      |             |              |        |           |          |  | 3 24a | 52.183 | 375      |
|      |             |              |        |           |          |  | 0 59  | 52.183 | 375      |
| 37   | 546523.011  | 728254.559   | 57.090 | 1.050     |          |   | 0 37  | 56.040 | 150      |
| 38   | 546490.532  | 728274.309   | 57.283 | 1.623     | 1200     |  | 1 37  | 55.660 | 150      |
|      |             |              |        |           |          |  | 0 38  | 55.660 | 150      |
| 39   | 546509.418  | 728340.613   | 56.603 | 1.634     | 1200     |  | 1 38  | 54.969 | 150      |
|      |             |              |        |           |          |  | 0 39  | 54.969 | 150      |
| 41   | 546588.817  | 728333.114   | 56.052 | 1.976     | 1200     |  | 1 40  | 54.151 | 150      |
|      |             |              |        |           |          |  | 2 39  | 54.151 | 150      |
|      |             |              |        |           |          |  | 0 41  | 54.076 | 225      |
| 2    | 546477.322  | 728190.302   | 57.352 | 1.947     | 1200     |  | 1 1   | 55.480 | 150      |
|      |             |              |        |           |          |  | 0 2   | 55.405 | 225      |

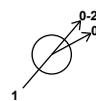
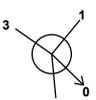
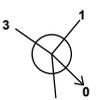
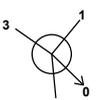
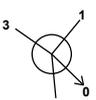
**Manhole Schedule**

| Node   | Easting (m) | Northing (m) | CL (m) | Depth (m) | Dia (mm) | Connections  | Link | IL (m) | Dia (mm) |
|--------|-------------|--------------|--------|-----------|----------|--|------|--------|----------|
| 46     | 546684.416  | 728258.568   | 53.906 | 1.668     | 1200     |    | 1 45 | 52.238 | 225      |
|        |             |              |        |           |          |  | 0 46 | 52.238 | 225      |
| 55     | 546685.671  | 728246.559   | 53.664 | 3.008     | 1200     |    | 1 54 | 50.660 | 375      |
|        |             |              |        |           |          |  | 2 46 | 52.145 | 225      |
|        |             |              |        |           |          |  | 0 55 | 50.656 | 375      |
| 60     | 546669.723  | 728226.416   | 54.080 | 3.529     | 1200     |    | 1 59 | 51.843 | 375      |
|        |             |              |        |           |          |  | 2 55 | 50.551 | 375      |
|        |             |              |        |           |          |  | 0 60 | 50.551 | 375      |
| 49     | 546572.792  | 728052.771   | 55.829 | 1.664     | 1200     |    | 1 48 | 54.165 | 225      |
|        |             |              |        |           |          |  | 0 49 | 54.198 | 225      |
| 50     | 546624.464  | 728100.273   | 55.212 | 1.560     | 1200     |    | 1 49 | 53.652 | 225      |
|        |             |              |        |           |          |  | 0 50 | 53.652 | 225      |
| 51     | 546696.092  | 728152.365   | 54.543 | 2.121     | 1200     |   | 1 50 | 52.572 | 225      |
|        |             |              |        |           |          |  | 0 51 | 52.422 | 375      |
| 40     | 546526.008  | 728258.431   | 57.033 | 1.050     |          |  | 0 40 | 55.983 | 150      |
| 53     | 546745.329  | 728206.618   | 52.995 | 1.775     | 1200     |  | 1 52 | 51.220 | 375      |
|        |             |              |        |           |          |  | 0 53 | 51.220 | 375      |
| 68     | 546721.109  | 728183.949   | 51.108 | 0.680     | 1200     |  | 0 68 | 50.428 | 225      |
| 54     | 546695.858  | 728245.794   | 53.563 | 2.869     | 1200     |  | 1 53 | 50.694 | 375      |
|        |             |              |        |           |          |  | 0 54 | 50.694 | 375      |
| 68_OUT | 546723.869  | 728181.369   | 51.108 | 0.717     | 1200     |  | 1 68 | 50.391 | 225      |
| 67     | 546695.996  | 728204.581   | 52.980 | 2.543     | 1200     |  | 1 66 | 50.437 | 375      |
|        |             |              |        |           |          |  | 0 67 | 50.437 | 375      |
| 67_OUT | 546698.578  | 728202.431   | 51.108 | 0.680     | 1200     |  | 1 67 | 50.428 | 375      |

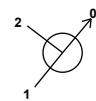
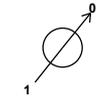
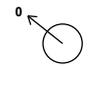
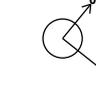
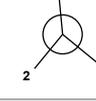
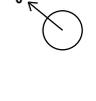
**Manhole Schedule**

| Node   | Easting (m) | Northing (m) | CL (m) | Depth (m) | Dia (mm) | Connections  | Link | IL (m) | Dia (mm) |
|--------|-------------|--------------|--------|-----------|----------|--|------|--------|----------|
| 10     | 546489.685  | 727969.396   | 56.308 | 0.900     | 1200     |    |      |        |          |
|        |             |              |        |           |          | 0  | 10   | 55.408 | 150      |
| 11     | 546458.111  | 727942.365   | 55.306 | 0.900     | 1200     |    |      |        |          |
|        |             |              |        |           |          | 0  | 11   | 54.406 | 150      |
|        |             |              |        |           |          | 1  | 47   | 54.393 | 225      |
| 48     | 546560.006  | 728047.986   | 55.982 | 1.589     | 1200     |    |      |        |          |
|        |             |              |        |           |          | 0  | 48   | 54.393 | 225      |
| 47     | 546541.540  | 728058.978   | 56.176 | 1.425     | 1200     |    |      |        |          |
|        |             |              |        |           |          | 0  | 47   | 54.751 | 225      |
| 52     | 546742.466  | 728197.796   | 53.102 | 1.575     | 1200     |   |      |        |          |
|        |             |              |        |           |          | 1  | 51   | 51.527 | 375      |
|        |             |              |        |           |          | 0  | 52   | 51.527 | 375      |
| 25     | 546515.102  | 728044.830   | 56.425 | 1.725     | 1200     |  |      |        |          |
|        |             |              |        |           |          | 0  | 25   | 54.700 | 525      |
| 26     | 546568.842  | 728108.690   | 55.911 | 1.725     | 1200     |  |      |        |          |
|        |             |              |        |           |          | 1  | 25   | 54.186 | 525      |
|        |             |              |        |           |          | 0  | 26   | 54.186 | 525      |
| 27     | 546624.649  | 728174.829   | 55.329 | 1.725     | 1500     |  |      |        |          |
|        |             |              |        |           |          | 1  | 26   | 53.604 | 525      |
|        |             |              |        |           |          | 0-1  | 27   | 53.604 | 525      |
|        |             |              |        |           |          | 0-2  | 27a  | 53.604 | 525      |
| 30     | 546626.506  | 728170.450   | 55.259 | 2.184     | 1500     |  |      |        |          |
|        |             |              |        |           |          | 1  | 29   | 53.075 | 300      |
|        |             |              |        |           |          | 0-1  | 30   | 53.075 | 300      |
|        |             |              |        |           |          | 0-2  | 30a  | 53.075 | 300      |
| 28     | 546526.572  | 728052.622   | 56.283 | 1.500     | 1200     |  |      |        |          |
|        |             |              |        |           |          | 0  | 28   | 54.783 | 300      |
| 29     | 546577.586  | 728114.511   | 55.784 | 1.500     | 1200     |  |      |        |          |
|        |             |              |        |           |          | 1  | 28   | 54.284 | 300      |
|        |             |              |        |           |          | 0  | 29   | 54.284 | 300      |
| 36     | 546630.862  | 728175.555   | 55.213 | 4.146     | 1500     |  |      |        |          |
|        |             |              |        |           |          | 1  | 35   | 51.292 | 225      |
|        |             |              |        |           |          | 2  | 30   | 53.010 | 300      |
|        |             |              |        |           |          | 3  | 27   | 53.488 | 525      |
|        |             |              |        |           |          | 4  | 24   | 52.203 | 375      |
|        |             |              |        |           |          | 0  | 36   | 51.067 | 525      |
| 36_OUT | 546635.223  | 728171.525   | 55.385 | 4.330     | 1200     |  |      |        |          |
|        |             |              |        |           |          | 1  | 36   | 51.055 | 525      |

**Manhole Schedule**

| Node | Easting (m) | Northing (m) | CL (m) | Depth (m) | Dia (mm) | Connections  | Link | IL (m) | Dia (mm) |
|------|-------------|--------------|--------|-----------|----------|--|------|--------|----------|
| 35   | 546669.037  | 728222.328   | 54.081 | 2.386     | 1200     | <br>1                  | 34   | 51.695 | 225      |
| 42   | 546591.384  | 728341.483   | 56.176 | 2.152     | 1200     | <br>0                  | 35   | 51.695 | 225      |
| 42   | 546591.384  | 728341.483   | 56.176 | 2.152     | 1200     | <br>1                  | 41   | 54.024 | 225      |
| 24   | 546624.981  | 728172.351   | 55.303 | 3.062     | 1500     | <br>0-2<br>0-1         | 23   | 52.241 | 375      |
| 34   | 546681.560  | 728224.386   | 53.605 | 1.825     | 1200     | <br>1                  | 24   | 52.241 | 375      |
| 34   | 546681.560  | 728224.386   | 53.605 | 1.825     | 1200     | <br>0-2                | 24a  | 52.241 | 375      |
| 34   | 546681.560  | 728224.386   | 53.605 | 1.825     | 1200     | <br>0-1<br>0-2         | 33   | 51.780 | 225      |
| 31   | 546700.336  | 728210.039   | 53.217 | 0.750     | 1200     | <br>0                  | 34   | 51.780 | 225      |
| 31   | 546700.336  | 728210.039   | 53.217 | 0.750     | 1200     | <br>0-2                | 34a  | 51.780 | 225      |
| 32   | 546715.293  | 728228.218   | 53.225 | 0.993     | 1200     | <br>0                | 31   | 52.467 | 150      |
| 32   | 546715.293  | 728228.218   | 53.225 | 0.993     | 1200     | <br>1                | 31   | 52.232 | 150      |
| 32   | 546715.293  | 728228.218   | 53.225 | 0.993     | 1200     | <br>0                | 32   | 52.232 | 150      |
| 33   | 546696.736  | 728242.848   | 53.518 | 1.597     | 1200     | <br>0                | 32   | 51.996 | 150      |
| 33   | 546696.736  | 728242.848   | 53.518 | 1.597     | 1200     | <br>1                | 33   | 51.921 | 225      |
| 66   | 546677.753  | 728219.758   | 53.672 | 3.156     | 1200     | <br>1<br>2<br>3<br>0 | 34a  | 51.720 | 225      |
| 66   | 546677.753  | 728219.758   | 53.672 | 3.156     | 1200     | <br>64               | 64   | 52.547 | 225      |
| 66   | 546677.753  | 728219.758   | 53.672 | 3.156     | 1200     | <br>60               | 60   | 50.516 | 375      |
| 66   | 546677.753  | 728219.758   | 53.672 | 3.156     | 1200     | <br>0                | 66   | 50.516 | 375      |
| 44   | 546645.968  | 728303.279   | 54.341 | 1.103     |          | <br>1                | 43   | 53.238 | 150      |
| 44   | 546645.968  | 728303.279   | 54.341 | 1.103     |          | <br>0                | 44   | 53.238 | 150      |
| 43   | 546605.537  | 728337.243   | 56.605 | 2.695     |          | <br>1                | 42   | 53.910 | 150      |
| 43   | 546605.537  | 728337.243   | 56.605 | 2.695     |          | <br>0                | 43   | 53.910 | 150      |
| 45   | 546690.672  | 728265.595   | 53.633 | 1.323     | 1200     | <br>1                | 44   | 52.385 | 150      |
| 45   | 546690.672  | 728265.595   | 53.633 | 1.323     | 1200     | <br>0                | 45   | 52.310 | 225      |
| 18   | 546506.789  | 728039.440   | 56.512 | 1.866     | 1200     | <br>1                | 17   | 54.646 | 150      |
| 18   | 546506.789  | 728039.440   | 56.512 | 1.866     | 1200     | <br>0                | 18   | 54.646 | 150      |
| 9    | 546433.927  | 728015.493   | 56.045 | 2.291     | 1200     | <br>1                | 8    | 53.754 | 150      |
| 9    | 546433.927  | 728015.493   | 56.045 | 2.291     | 1200     | <br>0                | 9    | 53.754 | 150      |

**Manhole Schedule**

| Node | Easting (m) | Northing (m) | CL (m) | Depth (m) | Dia (mm) | Connections  | Link         | IL (m)           | Dia (mm)   |
|------|-------------|--------------|--------|-----------|----------|--|--------------|------------------|------------|
| 14   | 546442.581  | 728008.872   | 55.981 | 2.311     | 1200     |    | 1 13<br>2 9  | 53.670<br>53.670 | 225<br>150 |
| 13   | 546428.017  | 727990.813   | 56.010 | 2.190     | 1200     |    | 1 12         | 53.895           | 150        |
| 61   | 546679.614  | 728199.691   | 53.608 | 0.700     | 450      |    | 0 61         | 52.908           | 100        |
| 62   | 546673.333  | 728204.719   | 53.874 | 1.092     | 450      |    | 1 61         | 52.828           | 100        |
| 64   | 546678.561  | 728211.123   | 53.892 | 1.159     | 1200     |   | 1 63<br>2 62 | 52.858<br>52.733 | 100<br>225 |
| 63   | 546684.743  | 728206.020   | 53.660 | 0.700     | 450      |  | 0 63         | 52.960           | 100        |

**Simulation Settings**

|                      |                      |   |        |
|----------------------|----------------------|---|--------|
| Rainfall Methodology | FSR                  | Analysis Speed                          | Normal |
| Rainfall Events      | Singular             | Skip Steady State                       | x      |
| FSR Region           | Scotland and Ireland | Drain Down Time (mins)                  | 1440   |
| M5-60 (mm)           | 15.600               | Additional Storage (m <sup>3</sup> /ha) | 0.0    |
| Ratio-R              | 0.260                | Starting Level (m)                      |        |
| Summer CV            | 1.000                | Check Discharge Rate(s)                 | x      |
| Winter CV            | 1.000                | Check Discharge Volume                  | x      |

**Storm Durations**

15 | 30 | 60 | 120 | 180 | 240 | 360 | 480 | 600 | 720 | 960 | 1440

| Return Period (years) | Climate Change (CC %) | Additional Area (A %) | Additional Flow (Q %) |
|-----------------------|-----------------------|-----------------------|-----------------------|
| 5                     | 20                    | 0                     | 0                     |
| 10                    | 20                    | 0                     | 0                     |
| 30                    | 20                    | 0                     | 0                     |
| 100                   | 20                    | 0                     | 0                     |

**Node 68 Infiltration Basin Storage Structure**

|                             |         |                                |        |
|-----------------------------|---------|--------------------------------|--------|
| Base Inf Coefficient (m/hr) | 0.21960 | Invert Level (m)               | 50.428 |
| Side Inf Coefficient (m/hr) | 0.21960 | Time to half empty (mins)      | 124    |
| Safety Factor               | 2.0     | Analyse flow through structure | x      |
| Porosity                    | 0.95    |                                |        |

**Inlets**  
67\_OUT

| Depth (m) | Area (m <sup>2</sup> ) | Inf Area (m <sup>2</sup> ) | Depth (m) | Area (m <sup>2</sup> ) | Inf Area (m <sup>2</sup> ) |
|-----------|------------------------|----------------------------|-----------|------------------------|----------------------------|
| 0.000     | 1233.0                 | 1300.0                     | 0.680     | 1500.0                 | 1499.8                     |

**Node 36 OUT Depth/Area Storage Structure**

|                             |         |               |      |                           |        |
|-----------------------------|---------|---------------|------|---------------------------|--------|
| Base Inf Coefficient (m/hr) | 0.00000 | Safety Factor | 2.0  | Invert Level (m)          | 51.055 |
| Side Inf Coefficient (m/hr) | 0.00000 | Porosity      | 1.00 | Time to half empty (mins) | 0      |

| Depth (m) | Area (m <sup>2</sup> ) | Inf Area (m <sup>2</sup> ) | Depth (m) | Area (m <sup>2</sup> ) | Inf Area (m <sup>2</sup> ) | Depth (m) | Area (m <sup>2</sup> ) | Inf Area (m <sup>2</sup> ) | Depth (m) | Area (m <sup>2</sup> ) | Inf Area (m <sup>2</sup> ) |
|-----------|------------------------|----------------------------|-----------|------------------------|----------------------------|-----------|------------------------|----------------------------|-----------|------------------------|----------------------------|
| 0.000     | 492.0                  | 0.0                        | 3.560     | 492.0                  | 0.0                        | 3.561     | 0.0                    | 0.0                        | 4.330     | 0.0                    | 0.0                        |

**Node 6 Link Surround Storage Structure**

|                             |         |                           |        |                |          |
|-----------------------------|---------|---------------------------|--------|----------------|----------|
| Base Inf Coefficient (m/hr) | 0.21960 | Porosity                  | 0.30   | Link           | 5        |
| Side Inf Coefficient (m/hr) | 0.21960 | Invert Level (m)          | 54.326 | Surround Shape | (Trench) |
| Safety Factor               | 2.0     | Time to half empty (mins) | 41     | Diameter (mm)  | 450      |

**Node 7 Link Surround Storage Structure**

|                             |         |                           |        |                |          |
|-----------------------------|---------|---------------------------|--------|----------------|----------|
| Base Inf Coefficient (m/hr) | 0.21960 | Porosity                  | 0.30   | Link           | 6        |
| Side Inf Coefficient (m/hr) | 0.21960 | Invert Level (m)          | 54.030 | Surround Shape | (Trench) |
| Safety Factor               | 2.0     | Time to half empty (mins) | 47     | Diameter (mm)  | 450      |

**Node 8 Link Surround Storage Structure**

|                             |         |                           |        |                |          |
|-----------------------------|---------|---------------------------|--------|----------------|----------|
| Base Inf Coefficient (m/hr) | 0.21960 | Porosity                  | 0.30   | Link           | 7        |
| Side Inf Coefficient (m/hr) | 0.21960 | Invert Level (m)          | 53.836 | Surround Shape | (Trench) |
| Safety Factor               | 2.0     | Time to half empty (mins) | 46     | Diameter (mm)  | 450      |

**Node 11 Link Surround Storage Structure**

|                             |         |                           |        |                |          |
|-----------------------------|---------|---------------------------|--------|----------------|----------|
| Base Inf Coefficient (m/hr) | 0.21960 | Porosity                  | 0.30   | Link           | 10       |
| Side Inf Coefficient (m/hr) | 0.21960 | Invert Level (m)          | 54.406 | Surround Shape | (Trench) |
| Safety Factor               | 2.0     | Time to half empty (mins) | 1      | Diameter (mm)  | 450      |

**Node 17 Link Surround Storage Structure**

|                             |         |                           |        |                |          |
|-----------------------------|---------|---------------------------|--------|----------------|----------|
| Base Inf Coefficient (m/hr) | 0.21960 | Porosity                  | 0.30   | Link           | 16       |
| Side Inf Coefficient (m/hr) | 0.21960 | Invert Level (m)          | 54.682 | Surround Shape | (Trench) |
| Safety Factor               | 2.0     | Time to half empty (mins) | 4      | Diameter (mm)  | 450      |

**Node 38 Link Surround Storage Structure**

|                             |         |                           |        |                |          |
|-----------------------------|---------|---------------------------|--------|----------------|----------|
| Base Inf Coefficient (m/hr) | 0.21960 | Porosity                  | 0.30   | Link           | 37       |
| Side Inf Coefficient (m/hr) | 0.21960 | Invert Level (m)          | 55.660 | Surround Shape | (Trench) |
| Safety Factor               | 2.0     | Time to half empty (mins) | 17     | Diameter (mm)  | 450      |

**Node 39 Link Surround Storage Structure**

|                             |         |                           |        |                |          |
|-----------------------------|---------|---------------------------|--------|----------------|----------|
| Base Inf Coefficient (m/hr) | 0.21960 | Porosity                  | 0.30   | Link           | 38       |
| Side Inf Coefficient (m/hr) | 0.21960 | Invert Level (m)          | 54.969 | Surround Shape | (Trench) |
| Safety Factor               | 2.0     | Time to half empty (mins) | 23     | Diameter (mm)  | 450      |

**Node 41 Link Surround Storage Structure**

|                             |         |                           |        |                |          |
|-----------------------------|---------|---------------------------|--------|----------------|----------|
| Base Inf Coefficient (m/hr) | 0.21960 | Porosity                  | 0.30   | Link           | 39       |
| Side Inf Coefficient (m/hr) | 0.21960 | Invert Level (m)          | 54.151 | Surround Shape | (Trench) |
| Safety Factor               | 2.0     | Time to half empty (mins) | 27     | Diameter (mm)  | 450      |

**Node 41 Link Surround Storage Structure**

|                             |         |                           |        |                |          |
|-----------------------------|---------|---------------------------|--------|----------------|----------|
| Base Inf Coefficient (m/hr) | 0.21960 | Porosity                  | 0.30   | Link           | 40       |
| Side Inf Coefficient (m/hr) | 0.21960 | Invert Level (m)          | 54.151 | Surround Shape | (Trench) |
| Safety Factor               | 2.0     | Time to half empty (mins) | 27     | Diameter (mm)  | 450      |

**Node 5 Link Surround Storage Structure**

|                             |         |                           |        |                |          |
|-----------------------------|---------|---------------------------|--------|----------------|----------|
| Base Inf Coefficient (m/hr) | 0.21960 | Porosity                  | 0.30   | Link           | 4        |
| Side Inf Coefficient (m/hr) | 0.21960 | Invert Level (m)          | 54.741 | Surround Shape | (Trench) |
| Safety Factor               | 2.0     | Time to half empty (mins) | 37     | Diameter (mm)  | 450      |

**Node 43 Link Surround Storage Structure**

|                             |         |                           |        |                |          |
|-----------------------------|---------|---------------------------|--------|----------------|----------|
| Base Inf Coefficient (m/hr) | 0.21960 | Porosity                  | 0.30   | Link           | 42       |
| Side Inf Coefficient (m/hr) | 0.21960 | Invert Level (m)          | 53.910 | Surround Shape | (Trench) |
| Safety Factor               | 2.0     | Time to half empty (mins) | 29     | Diameter (mm)  | 450      |

**Node 4 Link Surround Storage Structure**

|                             |         |                           |        |                |          |
|-----------------------------|---------|---------------------------|--------|----------------|----------|
| Base Inf Coefficient (m/hr) | 0.21960 | Porosity                  | 0.30   | Link           | 3        |
| Side Inf Coefficient (m/hr) | 0.21960 | Invert Level (m)          | 55.334 | Surround Shape | (Trench) |
| Safety Factor               | 2.0     | Time to half empty (mins) | 25     | Diameter (mm)  | 450      |

**Node 2 Link Surround Storage Structure**

|                             |         |                           |        |                |          |
|-----------------------------|---------|---------------------------|--------|----------------|----------|
| Base Inf Coefficient (m/hr) | 0.21960 | Porosity                  | 0.30   | Link           | 1        |
| Side Inf Coefficient (m/hr) | 0.21960 | Invert Level (m)          | 55.480 | Surround Shape | (Trench) |
| Safety Factor               | 2.0     | Time to half empty (mins) | 24     | Diameter (mm)  | 450      |

**Node 44 Link Surround Storage Structure**

|                             |         |                           |        |                |          |
|-----------------------------|---------|---------------------------|--------|----------------|----------|
| Base Inf Coefficient (m/hr) | 0.21960 | Porosity                  | 0.30   | Link           | 43       |
| Side Inf Coefficient (m/hr) | 0.21960 | Invert Level (m)          | 53.238 | Surround Shape | (Trench) |
| Safety Factor               | 2.0     | Time to half empty (mins) | 11     | Diameter (mm)  | 450      |

**Node 45 Link Surround Storage Structure**

|                             |         |                           |        |                |          |
|-----------------------------|---------|---------------------------|--------|----------------|----------|
| Base Inf Coefficient (m/hr) | 0.21960 | Porosity                  | 0.30   | Link           | 44       |
| Side Inf Coefficient (m/hr) | 0.21960 | Invert Level (m)          | 52.385 | Surround Shape | (Trench) |
| Safety Factor               | 2.0     | Time to half empty (mins) | 0      | Diameter (mm)  | 450      |

**Node 18 Link Surround Storage Structure**

|                             |         |                           |        |                |          |
|-----------------------------|---------|---------------------------|--------|----------------|----------|
| Base Inf Coefficient (m/hr) | 0.21960 | Porosity                  | 0.30   | Link           | 17       |
| Side Inf Coefficient (m/hr) | 0.21960 | Invert Level (m)          | 54.646 | Surround Shape | (Trench) |
| Safety Factor               | 2.0     | Time to half empty (mins) | 7      | Diameter (mm)  | 450      |

**Node 15 Link Surround Storage Structure**

|                             |         |                           |        |                |          |
|-----------------------------|---------|---------------------------|--------|----------------|----------|
| Base Inf Coefficient (m/hr) | 0.21960 | Porosity                  | 0.30   | Link           | 14       |
| Side Inf Coefficient (m/hr) | 0.21960 | Invert Level (m)          | 53.276 | Surround Shape | (Trench) |
| Safety Factor               | 2.0     | Time to half empty (mins) | 5      | Diameter (mm)  | 450      |

**Node 12 Link Surround Storage Structure**

|                             |         |                           |        |                |          |
|-----------------------------|---------|---------------------------|--------|----------------|----------|
| Base Inf Coefficient (m/hr) | 0.21960 | Porosity                  | 0.30   | Link           | 11       |
| Side Inf Coefficient (m/hr) | 0.21960 | Invert Level (m)          | 53.990 | Surround Shape | (Trench) |
| Safety Factor               | 2.0     | Time to half empty (mins) | 22     | Diameter (mm)  | 450      |

**Node 9 Link Surround Storage Structure**

|                             |         |                           |        |                |          |
|-----------------------------|---------|---------------------------|--------|----------------|----------|
| Base Inf Coefficient (m/hr) | 0.21960 | Porosity                  | 0.30   | Link           | 8        |
| Side Inf Coefficient (m/hr) | 0.21960 | Invert Level (m)          | 53.754 | Surround Shape | (Trench) |
| Safety Factor               | 2.0     | Time to half empty (mins) | 47     | Diameter (mm)  | 450      |

**Node 13 Link Surround Storage Structure**

|                             |         |                           |        |                |          |
|-----------------------------|---------|---------------------------|--------|----------------|----------|
| Base Inf Coefficient (m/hr) | 0.21960 | Porosity                  | 0.30   | Link           | 12       |
| Side Inf Coefficient (m/hr) | 0.21960 | Invert Level (m)          | 53.895 | Surround Shape | (Trench) |
| Safety Factor               | 2.0     | Time to half empty (mins) | 35     | Diameter (mm)  | 450      |

**Node 14 Link Surround Storage Structure**

|                             |         |                           |        |                |          |
|-----------------------------|---------|---------------------------|--------|----------------|----------|
| Base Inf Coefficient (m/hr) | 0.21960 | Porosity                  | 0.30   | Link           | 9        |
| Side Inf Coefficient (m/hr) | 0.21960 | Invert Level (m)          | 53.670 | Surround Shape | (Trench) |
| Safety Factor               | 2.0     | Time to half empty (mins) | 45     | Diameter (mm)  | 450      |

**Node 63 Carpark Storage Structure**

|                             |         |                           |        |               |       |
|-----------------------------|---------|---------------------------|--------|---------------|-------|
| Base Inf Coefficient (m/hr) | 0.21960 | Invert Level (m)          | 52.960 | Slope (1:X)   | 100.0 |
| Side Inf Coefficient (m/hr) | 0.21960 | Time to half empty (mins) | 0      | Depth (m)     | 0.350 |
| Safety Factor               | 2.0     | Width (m)                 | 15.000 | Inf Depth (m) |       |
| Porosity                    | 0.30    | Length (m)                | 5.000  |               |       |

**Node 61 Carpark Storage Structure**

|                             |         |                           |        |               |       |
|-----------------------------|---------|---------------------------|--------|---------------|-------|
| Base Inf Coefficient (m/hr) | 0.21960 | Invert Level (m)          | 52.908 | Slope (1:X)   | 100.0 |
| Side Inf Coefficient (m/hr) | 0.00000 | Time to half empty (mins) | 0      | Depth (m)     | 0.350 |
| Safety Factor               | 2.0     | Width (m)                 | 16.200 | Inf Depth (m) |       |
| Porosity                    | 0.30    | Length (m)                | 5.000  |               |       |

**Results for 5 year +20% CC Critical Storm Duration. Lowest mass balance: 99.33%**

| Node Event       | US Node | Peak (mins) | Level (m) | Depth (m) | Inflow (l/s) | Node Vol (m <sup>3</sup> ) | Flood (m <sup>3</sup> ) | Status     |
|------------------|---------|-------------|-----------|-----------|--------------|----------------------------|-------------------------|------------|
| 15 minute summer | 3       | 12          | 56.624    | 0.209     | 18.8         | 0.0000                     | 0.0000                  | SURCHARGED |
| 15 minute summer | 1       | 11          | 56.045    | 0.082     | 8.1          | 0.0000                     | 0.0000                  | OK         |
| 30 minute summer | 4       | 22          | 55.975    | 0.641     | 29.3         | 2.3662                     | 0.0000                  | SURCHARGED |
| 30 minute summer | 5       | 23          | 55.407    | 0.666     | 25.3         | 3.5487                     | 0.0000                  | SURCHARGED |
| 60 minute summer | 6       | 40          | 54.979    | 0.653     | 18.6         | 2.9576                     | 0.0000                  | SURCHARGED |
| 30 minute summer | 7       | 22          | 54.702    | 0.672     | 24.7         | 2.5189                     | 0.0000                  | SURCHARGED |
| 60 minute summer | 8       | 40          | 54.415    | 0.579     | 20.6         | 1.5038                     | 0.0000                  | SURCHARGED |
| 60 minute summer | 12      | 41          | 54.141    | 0.151     | 7.6          | 0.3181                     | 0.0000                  | SURCHARGED |
| 60 minute summer | 15      | 43          | 53.436    | 0.160     | 17.1         | 0.3519                     | 0.0000                  | SURCHARGED |
| 15 minute summer | 16      | 11          | 55.557    | 0.069     | 6.8          | 0.0776                     | 0.0000                  | OK         |
| 15 minute summer | 17      | 12          | 54.837    | 0.155     | 9.9          | 0.2976                     | 0.0000                  | SURCHARGED |
| 30 minute summer | 21      | 19          | 52.960    | 0.172     | 43.8         | 0.1944                     | 0.0000                  | OK         |
| 15 minute summer | 22      | 12          | 52.854    | 0.190     | 56.3         | 0.2147                     | 0.0000                  | OK         |
| 30 minute summer | 23      | 20          | 52.633    | 0.223     | 69.4         | 0.2523                     | 0.0000                  | OK         |
| 30 minute summer | 59      | 19          | 52.466    | 0.283     | 131.1        | 0.3198                     | 0.0000                  | OK         |
| 15 minute summer | 37      | 10          | 56.104    | 0.064     | 5.8          | 0.0000                     | 0.0000                  | OK         |

| Link Event (Outflow) | US Node | Link         | DS Node | Outflow (l/s) | Velocity (m/s) | Flow/Cap | Link Vol (m <sup>3</sup> ) | Discharge Vol (m <sup>3</sup> ) |
|----------------------|---------|--------------|---------|---------------|----------------|----------|----------------------------|---------------------------------|
| 15 minute summer     | 3       | 3            | 4       | 18.0          | 1.043          | 0.921    | 1.1981                     |                                 |
| 15 minute summer     | 1       | 1            | 2       | 7.8           | 0.649          | 0.578    | 0.8628                     |                                 |
| 15 minute summer     | 4       | 4            | 5       | 14.2          | 0.819          | 1.049    | 1.3582                     |                                 |
| 30 minute summer     | 4       | Infiltration |         | 1.8           |                |          |                            |                                 |
| 15 minute summer     | 5       | 5            | 6       | 14.9          | 0.855          | 1.097    | 0.9493                     |                                 |
| 30 minute summer     | 5       | Infiltration |         | 2.8           |                |          |                            |                                 |
| 15 minute summer     | 6       | 6            | 7       | 13.5          | 0.770          | 0.999    | 0.6777                     |                                 |
| 60 minute summer     | 6       | Infiltration |         | 2.2           |                |          |                            |                                 |
| 15 minute summer     | 7       | 7            | 8       | 16.8          | 0.956          | 1.240    | 0.4432                     |                                 |
| 30 minute summer     | 7       | Infiltration |         | 1.8           |                |          |                            |                                 |
| 30 minute summer     | 8       | 8            | 9       | 18.1          | 1.026          | 1.331    | 0.1871                     |                                 |
| 60 minute summer     | 8       | Infiltration |         | 1.1           |                |          |                            |                                 |
| 15 minute summer     | 12      | 12           | 13      | 9.4           | 0.815          | 0.695    | 0.1813                     |                                 |
| 60 minute summer     | 12      | Infiltration |         | 0.5           |                |          |                            |                                 |
| 60 minute summer     | 15      | 15           | 21      | 16.5          | 1.005          | 1.062    | 0.5570                     |                                 |
| 60 minute summer     | 15      | Infiltration |         | 0.5           |                |          |                            |                                 |
| 15 minute summer     | 16      | 16           | 17      | 6.6           | 0.634          | 0.424    | 1.0139                     |                                 |
| 15 minute summer     | 17      | 17           | 18      | 10.2          | 0.657          | 0.658    | 0.0639                     |                                 |
| 15 minute summer     | 17      | Infiltration |         | 0.5           |                |          |                            |                                 |
| 30 minute summer     | 21      | 21           | 22      | 43.7          | 0.832          | 0.411    | 2.2819                     |                                 |
| 15 minute summer     | 22      | 22           | 23      | 56.2          | 0.920          | 0.529    | 5.4483                     |                                 |
| 30 minute summer     | 23      | 23           | 24      | 67.4          | 1.114          | 0.634    | 4.0576                     |                                 |
| 15 minute summer     | 59      | 59           | 60      | 130.7         | 1.519          | 0.872    | 5.1946                     |                                 |
| 15 minute summer     | 37      | 37           | 38      | 5.7           | 0.475          | 0.371    | 0.4697                     |                                 |

**Results for 5 year +20% CC Critical Storm Duration. Lowest mass balance: 99.33%**

| Node Event        | US Node | Peak (mins) | Level (m) | Depth (m) | Inflow (l/s) | Node Vol (m <sup>3</sup> ) | Flood (m <sup>3</sup> ) | Status     |
|-------------------|---------|-------------|-----------|-----------|--------------|----------------------------|-------------------------|------------|
| 30 minute summer  | 38      | 21          | 56.027    | 0.367     | 19.3         | 1.2264                     | 0.0000                  | SURCHARGED |
| 30 minute summer  | 39      | 22          | 55.685    | 0.716     | 31.6         | 4.0598                     | 0.0000                  | SURCHARGED |
| 30 minute summer  | 41      | 23          | 54.758    | 0.682     | 44.2         | 4.3387                     | 0.0000                  | SURCHARGED |
| 30 minute summer  | 2       | 22          | 55.977    | 0.572     | 14.6         | 2.6356                     | 0.0000                  | SURCHARGED |
| 30 minute summer  | 46      | 20          | 52.353    | 0.115     | 20.8         | 0.1296                     | 0.0000                  | OK         |
| 15 minute summer  | 55      | 12          | 52.164    | 1.508     | 107.7        | 1.7053                     | 0.0000                  | SURCHARGED |
| 15 minute summer  | 60      | 12          | 52.100    | 1.549     | 205.3        | 1.7516                     | 0.0000                  | SURCHARGED |
| 15 minute summer  | 49      | 11          | 54.301    | 0.136     | 17.4         | 0.1538                     | 0.0000                  | OK         |
| 15 minute summer  | 50      | 12          | 53.774    | 0.122     | 30.2         | 0.1377                     | 0.0000                  | OK         |
| 15 minute summer  | 51      | 11          | 52.531    | 0.109     | 38.5         | 0.1232                     | 0.0000                  | OK         |
| 15 minute summer  | 40      | 10          | 56.057    | 0.074     | 10.7         | 0.0000                     | 0.0000                  | OK         |
| 15 minute summer  | 53      | 13          | 52.224    | 1.004     | 103.3        | 1.1355                     | 0.0000                  | SURCHARGED |
| 180 minute summer | 68      | 128         | 50.593    | 0.165     | 82.5         | 202.1219                   | 0.0000                  | OK         |
| 15 minute summer  | 54      | 12          | 52.172    | 1.478     | 79.2         | 1.6714                     | 0.0000                  | SURCHARGED |
| 15 minute summer  | 68_OUT  | 1           | 50.391    | 0.000     | 0.0          | 0.0000                     | 0.0000                  | OK         |
| 15 minute summer  | 67      | 12          | 51.605    | 1.168     | 223.8        | 1.3209                     | 0.0000                  | SURCHARGED |
| 180 minute summer | 67_OUT  | 128         | 50.606    | 0.178     | 122.7        | 0.0000                     | 0.0000                  | OK         |
| 15 minute summer  | 10      | 10          | 55.461    | 0.053     | 6.4          | 0.0596                     | 0.0000                  | OK         |
| 15 minute summer  | 11      | 11          | 54.495    | 0.089     | 10.4         | 0.1163                     | 0.0000                  | OK         |

| Link Event (Outflow) | US Node | Link         | DS Node | Outflow (l/s) | Velocity (m/s) | Flow/Cap | Link Vol (m <sup>3</sup> ) | Discharge Vol (m <sup>3</sup> ) |
|----------------------|---------|--------------|---------|---------------|----------------|----------|----------------------------|---------------------------------|
| 15 minute summer     | 38      | 38           | 39      | 14.7          | 0.848          | 0.948    | 1.2159                     |                                 |
| 30 minute summer     | 38      | Infiltration |         | 0.9           |                |          |                            |                                 |
| 60 minute summer     | 39      | 39           | 41      | 16.1          | 0.956          | 1.039    | 1.4409                     |                                 |
| 30 minute summer     | 39      | Infiltration |         | 2.5           |                |          |                            |                                 |
| 15 minute summer     | 41      | 41           | 42      | 24.3          | 0.706          | 0.696    | 0.3484                     |                                 |
| 30 minute summer     | 41      | Infiltration |         | 2.3           |                |          |                            |                                 |
| 30 minute summer     | 41      | Infiltration |         | 1.4           |                |          |                            |                                 |
| 15 minute summer     | 2       | 2            | 4       | -8.9          | -0.231         | -0.196   | 0.3656                     |                                 |
| 30 minute summer     | 2       | Infiltration |         | 1.8           |                |          |                            |                                 |
| 30 minute summer     | 46      | 46           | 55      | 20.8          | 1.075          | 0.456    | 0.2330                     |                                 |
| 15 minute summer     | 55      | 55           | 60      | 112.5         | 1.020          | 0.883    | 2.8338                     |                                 |
| 15 minute summer     | 60      | 60           | 66      | 211.9         | 1.921          | 1.844    | 1.1507                     |                                 |
| 15 minute summer     | 49      | 49           | 50      | 17.1          | 0.901          | 0.426    | 1.3871                     |                                 |
| 15 minute summer     | 50      | 50           | 51      | 28.0          | 1.286          | 0.555    | 1.9281                     |                                 |
| 15 minute summer     | 51      | 51           | 52      | 38.1          | 1.523          | 0.183    | 4.4422                     |                                 |
| 15 minute summer     | 40      | 40           | 41      | 10.4          | 0.778          | 0.488    | 1.2847                     |                                 |
| 15 minute summer     | 53      | 53           | 54      | 78.6          | 0.829          | 0.430    | 6.9602                     |                                 |
| 15 minute summer     | 68      | Pump         | 68_OUT  | 0.0           |                |          |                            | 0.0                             |
| 180 minute summer    | 68      | Infiltration |         | 40.8          |                |          |                            |                                 |
| 15 minute summer     | 54      | 54           | 55      | 86.3          | 0.782          | 0.846    | 1.1268                     |                                 |
| 15 minute summer     | 67      | 67           | 67_OUT  | 229.9         | 3.222          | 2.234    | 0.2104                     |                                 |
| 15 minute summer     | 10      | 10           | 11      | 6.3           | 0.798          | 0.261    | 0.3385                     |                                 |
| 15 minute summer     | 11      | 11           | 12      | 10.1          | 0.915          | 0.652    | 0.6112                     |                                 |

**Results for 5 year +20% CC Critical Storm Duration. Lowest mass balance: 99.33%**

| Node Event           | US Node | Peak (mins)  | Level (m) | Depth (m)     | Inflow (l/s)   | Node Vol (m <sup>3</sup> ) | Flood (m <sup>3</sup> )    | Status                          |
|----------------------|---------|--------------|-----------|---------------|----------------|----------------------------|----------------------------|---------------------------------|
| 15 minute summer     | 48      | 11           | 54.435    | 0.042         | 5.3            | 0.0479                     | 0.0000                     | OK                              |
| 15 minute summer     | 47      | 10           | 54.795    | 0.044         | 5.4            | 0.0495                     | 0.0000                     | OK                              |
| 15 minute summer     | 52      | 13           | 52.223    | 0.696         | 65.9           | 0.7874                     | 0.0000                     | SURCHARGED                      |
| 15 minute summer     | 25      | 10           | 55.028    | 0.328         | 258.5          | 0.3705                     | 0.0000                     | OK                              |
| 15 minute summer     | 26      | 11           | 54.507    | 0.321         | 255.9          | 0.3632                     | 0.0000                     | OK                              |
| 15 minute summer     | 27      | 11           | 53.832    | 0.228         | 256.7          | 0.4033                     | 0.0000                     | OK                              |
| 15 minute summer     | 30      | 11           | 53.181    | 0.106         | 56.1           | 0.1869                     | 0.0000                     | OK                              |
| 15 minute summer     | 28      | 10           | 54.922    | 0.139         | 38.1           | 0.1576                     | 0.0000                     | OK                              |
| 15 minute summer     | 29      | 11           | 54.422    | 0.138         | 56.4           | 0.1560                     | 0.0000                     | OK                              |
| 15 minute summer     | 36      | 12           | 51.523    | 0.456         | 285.9          | 0.8054                     | 0.0000                     | OK                              |
| 15 minute summer     | 36_OUT  | 12           | 51.418    | 0.363         | 286.8          | 0.0000                     | 0.0000                     | OK                              |
| 15 minute summer     | 35      | 13           | 51.804    | 0.109         | 17.1           | 0.1235                     | 0.0000                     | OK                              |
| 30 minute summer     | 42      | 23           | 54.730    | 0.706         | 24.3           | 0.7983                     | 0.0000                     | SURCHARGED                      |
| 15 minute summer     | 24      | 12           | 52.467    | 0.226         | 86.8           | 0.3994                     | 0.0000                     | OK                              |
| 15 minute summer     | 34      | 12           | 51.897    | 0.117         | 31.4           | 0.1324                     | 0.0000                     | OK                              |
| 15 minute summer     | 31      | 10           | 52.552    | 0.085         | 10.5           | 0.0962                     | 0.0000                     | OK                              |
| 15 minute summer     | 32      | 11           | 52.325    | 0.093         | 11.9           | 0.1049                     | 0.0000                     | OK                              |
| 15 minute summer     | 33      | 10           | 52.056    | 0.135         | 25.3           | 0.1530                     | 0.0000                     | OK                              |
| 15 minute summer     | 66      | 12           | 51.906    | 1.390         | 218.1          | 1.5726                     | 0.0000                     | SURCHARGED                      |
| 30 minute summer     | 44      | 27           | 53.417    | 0.179         | 20.6           | 0.1334                     | 0.0000                     | SURCHARGED                      |
| Link Event (Outflow) | US Node | Link         | DS Node   | Outflow (l/s) | Velocity (m/s) | Flow/Cap                   | Link Vol (m <sup>3</sup> ) | Discharge Vol (m <sup>3</sup> ) |
| 15 minute summer     | 11      | Infiltration |           | 0.1           |                |                            |                            |                                 |
| 15 minute summer     | 48      | 48           | 49        | 5.2           | 0.360          | 0.078                      | 0.2064                     |                                 |
| 15 minute summer     | 47      | 47           | 48        | 5.3           | 1.010          | 0.079                      | 0.1136                     |                                 |
| 15 minute summer     | 52      | 52           | 53        | 66.5          | 1.345          | 0.182                      | 1.0234                     |                                 |
| 15 minute summer     | 25      | 25           | 26        | 255.9         | 1.840          | 0.674                      | 11.6094                    |                                 |
| 15 minute summer     | 26      | 26           | 27        | 256.7         | 2.246          | 0.646                      | 9.8825                     |                                 |
| 15 minute summer     | 27      | 27           | 36        | 171.3         | 2.218          | 0.259                      | 0.4842                     |                                 |
| 15 minute summer     | 27      | 27a          | 59        | 84.6          | 1.048          | 0.401                      | 0.6759                     |                                 |
| 15 minute summer     | 30      | 30           | 36        | 23.7          | 1.157          | 0.217                      | 0.1377                     |                                 |
| 15 minute summer     | 30      | 30a          | 59        | 32.1          | 1.550          | 0.224                      | 0.2194                     |                                 |
| 15 minute summer     | 28      | 28           | 29        | 37.4          | 1.189          | 0.428                      | 2.5282                     |                                 |
| 15 minute summer     | 29      | 29           | 30        | 56.1          | 2.090          | 0.395                      | 1.9981                     |                                 |
| 15 minute summer     | 36      | 36           | 36_OUT    | 286.8         | 1.587          | 1.332                      | 1.0645                     | 138.2                           |
| 15 minute summer     | 35      | 35           | 36        | 20.5          | 0.696          | 0.484                      | 1.7237                     |                                 |
| 15 minute summer     | 42      | 42           | 43        | 23.1          | 1.313          | 1.705                      | 0.2601                     |                                 |
| 15 minute summer     | 24      | 24           | 36        | 84.1          | 1.314          | 0.557                      | 0.4285                     |                                 |
| 15 minute summer     | 24      | 24a          | 59        | 24.6          | 0.703          | 0.160                      | 0.7793                     |                                 |
| 15 minute summer     | 34      | 34           | 35        | 17.1          | 0.992          | 0.404                      | 0.2314                     |                                 |
| 15 minute summer     | 34      | 34a          | 66        | 13.4          | 1.031          | 0.258                      | 0.1680                     |                                 |
| 15 minute summer     | 31      | 31           | 32        | 10.4          | 0.972          | 0.586                      | 0.2537                     |                                 |
| 15 minute summer     | 32      | 32           | 33        | 11.8          | 1.055          | 0.663                      | 0.2636                     |                                 |
| 15 minute summer     | 33      | 33           | 34        | 25.2          | 1.301          | 0.635                      | 0.5204                     |                                 |
| 15 minute summer     | 66      | 66           | 67        | 223.8         | 2.029          | 1.948                      | 2.6176                     |                                 |
| 30 minute summer     | 44      | 44           | 45        | 19.6          | 1.190          | 1.048                      | 0.9830                     |                                 |

**Results for 5 year +20% CC Critical Storm Duration. Lowest mass balance: 99.33%**

| Node Event       | US Node | Peak (mins) | Level (m) | Depth (m) | Inflow (l/s) | Node Vol (m <sup>3</sup> ) | Flood (m <sup>3</sup> ) | Status     |
|------------------|---------|-------------|-----------|-----------|--------------|----------------------------|-------------------------|------------|
| 30 minute summer | 43      | 25          | 54.409    | 0.499     | 23.1         | 0.8026                     | 0.0000                  | SURCHARGED |
| 30 minute summer | 45      | 21          | 52.431    | 0.121     | 19.6         | 0.1443                     | 0.0000                  | OK         |
| 15 minute summer | 18      | 12          | 54.820    | 0.174     | 19.4         | 0.2538                     | 0.0000                  | SURCHARGED |
| 60 minute summer | 9       | 41          | 54.277    | 0.523     | 17.4         | 1.2267                     | 0.0000                  | SURCHARGED |
| 60 minute summer | 14      | 42          | 54.137    | 0.467     | 19.4         | 1.0957                     | 0.0000                  | SURCHARGED |
| 60 minute summer | 13      | 42          | 54.138    | 0.318     | 7.6          | 0.6186                     | 0.0000                  | SURCHARGED |
| 15 minute summer | 61      | 11          | 52.929    | 0.021     | 1.8          | 0.1108                     | 0.0000                  | OK         |
| 15 minute summer | 62      | 12          | 52.800    | 0.018     | 0.5          | 0.0029                     | 0.0000                  | OK         |
| 15 minute summer | 64      | 12          | 52.754    | 0.021     | 1.3          | 0.0238                     | 0.0000                  | OK         |
| 15 minute summer | 63      | 11          | 52.983    | 0.023     | 2.1          | 0.1286                     | 0.0000                  | OK         |

| Link Event (Outflow) | US Node | Link         | DS Node | Outflow (l/s) | Velocity (m/s) | Flow/Cap | Link Vol (m <sup>3</sup> ) | Discharge Vol (m <sup>3</sup> ) |
|----------------------|---------|--------------|---------|---------------|----------------|----------|----------------------------|---------------------------------|
| 30 minute summer     | 44      | Infiltration |         | 0.4           |                |          |                            |                                 |
| 30 minute summer     | 43      | 43           | 44      | 20.6          | 1.175          | 1.178    | 0.9296                     |                                 |
| 30 minute summer     | 43      | Infiltration |         | 0.6           |                |          |                            |                                 |
| 30 minute summer     | 45      | 45           | 46      | 19.6          | 0.954          | 0.489    | 0.1975                     |                                 |
| 30 minute summer     | 45      | Infiltration |         | 0.0           |                |          |                            |                                 |
| 15 minute summer     | 18      | 18           | 21      | 19.0          | 1.104          | 1.073    | 0.2391                     |                                 |
| 15 minute summer     | 18      | Infiltration |         | 0.1           |                |          |                            |                                 |
| 60 minute summer     | 9       | 9            | 14      | 15.7          | 0.894          | 1.160    | 0.1918                     |                                 |
| 60 minute summer     | 9       | Infiltration |         | 0.5           |                |          |                            |                                 |
| 30 minute summer     | 14      | 14           | 15      | 17.2          | 0.975          | 1.266    | 0.9015                     |                                 |
| 60 minute summer     | 14      | Infiltration |         | 0.4           |                |          |                            |                                 |
| 15 minute summer     | 13      | 13           | 14      | 6.7           | 0.277          | 0.183    | 0.9227                     |                                 |
| 60 minute summer     | 13      | Infiltration |         | 0.3           |                |          |                            |                                 |
| 15 minute summer     | 61      | 61           | 62      | 0.5           | 0.473          | 0.091    | 0.0094                     |                                 |
| 15 minute summer     | 61      | Infiltration |         | 1.0           |                |          |                            |                                 |
| 15 minute summer     | 62      | 62           | 64      | 0.6           | 0.326          | 0.014    | 0.0140                     |                                 |
| 15 minute summer     | 64      | 64           | 66      | 1.3           | 0.724          | 0.017    | 0.0159                     |                                 |
| 15 minute summer     | 63      | 63           | 64      | 0.8           | 0.569          | 0.114    | 0.0109                     |                                 |
| 15 minute summer     | 63      | Infiltration |         | 1.1           |                |          |                            |                                 |

**Results for 10 year +20% CC Critical Storm Duration. Lowest mass balance: 99.20%**

| Node Event           | US Node | Peak (mins)  | Level (m) | Depth (m)     | Inflow (l/s)   | Node Vol (m <sup>3</sup> ) | Flood (m <sup>3</sup> )    | Status                          |
|----------------------|---------|--------------|-----------|---------------|----------------|----------------------------|----------------------------|---------------------------------|
| 15 minute summer     | 3       | 12           | 56.994    | 0.579         | 21.7           | 0.0000                     | 0.0000                     | SURCHARGED                      |
| 30 minute summer     | 1       | 22           | 56.137    | 0.174         | 8.8            | 0.0000                     | 0.0000                     | SURCHARGED                      |
| 30 minute summer     | 4       | 23           | 56.106    | 0.772         | 31.4           | 3.2747                     | 0.0000                     | SURCHARGED                      |
| 30 minute summer     | 5       | 24           | 55.505    | 0.764         | 27.6           | 4.4640                     | 0.0000                     | SURCHARGED                      |
| 60 minute summer     | 6       | 41           | 55.076    | 0.750         | 19.4           | 3.6635                     | 0.0000                     | SURCHARGED                      |
| 30 minute summer     | 7       | 22           | 54.801    | 0.770         | 26.3           | 3.0307                     | 0.0000                     | SURCHARGED                      |
| 60 minute summer     | 8       | 40           | 54.499    | 0.663         | 21.8           | 1.7889                     | 0.0000                     | SURCHARGED                      |
| 60 minute summer     | 12      | 41           | 54.209    | 0.219         | 8.8            | 0.5939                     | 0.0000                     | SURCHARGED                      |
| 60 minute summer     | 15      | 44           | 53.450    | 0.174         | 17.6           | 0.4024                     | 0.0000                     | SURCHARGED                      |
| 15 minute summer     | 16      | 11           | 55.563    | 0.075         | 7.9            | 0.0845                     | 0.0000                     | OK                              |
| 15 minute summer     | 17      | 12           | 54.897    | 0.215         | 11.4           | 0.4993                     | 0.0000                     | SURCHARGED                      |
| 30 minute summer     | 21      | 19           | 52.970    | 0.182         | 48.0           | 0.2059                     | 0.0000                     | OK                              |
| 15 minute summer     | 22      | 12           | 52.866    | 0.202         | 62.4           | 0.2282                     | 0.0000                     | OK                              |
| 30 minute summer     | 23      | 20           | 52.650    | 0.240         | 77.2           | 0.2715                     | 0.0000                     | OK                              |
| 15 minute summer     | 59      | 12           | 52.497    | 0.314         | 153.5          | 0.3553                     | 0.0000                     | OK                              |
| 30 minute summer     | 37      | 21           | 56.167    | 0.127         | 6.4            | 0.0000                     | 0.0000                     | OK                              |
| Link Event (Outflow) | US Node | Link         | DS Node   | Outflow (l/s) | Velocity (m/s) | Flow/Cap                   | Link Vol (m <sup>3</sup> ) | Discharge Vol (m <sup>3</sup> ) |
| 15 minute summer     | 3       | 3            | 4         | 18.9          | 1.087          | 0.969                      | 1.1981                     |                                 |
| 15 minute summer     | 1       | 1            | 2         | 9.0           | 0.677          | 0.666                      | 0.9632                     |                                 |
| 30 minute summer     | 4       | 4            | 5         | 13.7          | 0.788          | 1.009                      | 1.3582                     |                                 |
| 30 minute summer     | 4       | Infiltration |           | 2.2           |                |                            |                            |                                 |
| 15 minute summer     | 5       | 5            | 6         | 13.8          | 0.862          | 1.019                      | 0.9493                     |                                 |
| 30 minute summer     | 5       | Infiltration |           | 3.3           |                |                            |                            |                                 |
| 15 minute summer     | 6       | 6            | 7         | 13.8          | 0.784          | 1.018                      | 0.6777                     |                                 |
| 60 minute summer     | 6       | Infiltration |           | 2.5           |                |                            |                            |                                 |
| 15 minute summer     | 7       | 7            | 8         | 17.4          | 0.988          | 1.282                      | 0.4432                     |                                 |
| 30 minute summer     | 7       | Infiltration |           | 2.0           |                |                            |                            |                                 |
| 30 minute summer     | 8       | 8            | 9         | 18.8          | 1.068          | 1.386                      | 0.1871                     |                                 |
| 60 minute summer     | 8       | Infiltration |           | 1.2           |                |                            |                            |                                 |
| 15 minute summer     | 12      | 12           | 13        | 10.9          | 0.832          | 0.805                      | 0.2159                     |                                 |
| 60 minute summer     | 12      | Infiltration |           | 0.7           |                |                            |                            |                                 |
| 60 minute summer     | 15      | 15           | 21        | 16.9          | 1.005          | 1.090                      | 0.5598                     |                                 |
| 60 minute summer     | 15      | Infiltration |           | 0.5           |                |                            |                            |                                 |
| 15 minute summer     | 16      | 16           | 17        | 7.6           | 0.634          | 0.492                      | 1.0624                     |                                 |
| 15 minute summer     | 17      | 17           | 18        | 11.3          | 0.662          | 0.729                      | 0.0639                     |                                 |
| 15 minute summer     | 17      | Infiltration |           | 0.7           |                |                            |                            |                                 |
| 30 minute summer     | 21      | 21           | 22        | 48.0          | 0.847          | 0.451                      | 2.4592                     |                                 |
| 15 minute summer     | 22      | 22           | 23        | 62.2          | 0.937          | 0.585                      | 5.9405                     |                                 |
| 30 minute summer     | 23      | 23           | 24        | 74.9          | 1.136          | 0.705                      | 4.5647                     |                                 |
| 15 minute summer     | 59      | 59           | 60        | 145.9         | 1.525          | 0.974                      | 6.3025                     |                                 |
| 15 minute summer     | 37      | 37           | 38        | 6.7           | 0.490          | 0.432                      | 0.5717                     |                                 |

**Results for 10 year +20% CC Critical Storm Duration. Lowest mass balance: 99.20%**

| Node Event        | US Node | Peak (mins) | Level (m) | Depth (m) | Inflow (l/s) | Node Vol (m <sup>3</sup> ) | Flood (m <sup>3</sup> ) | Status     |
|-------------------|---------|-------------|-----------|-----------|--------------|----------------------------|-------------------------|------------|
| 30 minute summer  | 38      | 21          | 56.150    | 0.490     | 22.4         | 1.9136                     | 0.0000                  | SURCHARGED |
| 30 minute summer  | 39      | 22          | 55.813    | 0.844     | 34.0         | 5.2409                     | 0.0000                  | SURCHARGED |
| 30 minute summer  | 41      | 23          | 54.853    | 0.777     | 49.0         | 5.6960                     | 0.0000                  | SURCHARGED |
| 30 minute summer  | 2       | 23          | 56.109    | 0.704     | 16.8         | 3.7478                     | 0.0000                  | SURCHARGED |
| 15 minute summer  | 46      | 13          | 52.356    | 0.118     | 20.9         | 0.1331                     | 0.0000                  | OK         |
| 15 minute summer  | 55      | 12          | 52.293    | 1.637     | 112.5        | 1.8511                     | 0.0000                  | SURCHARGED |
| 15 minute summer  | 60      | 12          | 52.221    | 1.670     | 234.6        | 1.8882                     | 0.0000                  | SURCHARGED |
| 15 minute summer  | 49      | 11          | 54.310    | 0.145     | 20.1         | 0.1639                     | 0.0000                  | OK         |
| 15 minute summer  | 50      | 12          | 53.786    | 0.134     | 35.2         | 0.1514                     | 0.0000                  | OK         |
| 15 minute summer  | 51      | 11          | 52.539    | 0.117     | 44.7         | 0.1328                     | 0.0000                  | OK         |
| 15 minute summer  | 40      | 10          | 56.064    | 0.081     | 12.4         | 0.0000                     | 0.0000                  | OK         |
| 15 minute summer  | 53      | 12          | 52.370    | 1.150     | 80.7         | 1.3010                     | 0.0000                  | SURCHARGED |
| 240 minute summer | 68      | 168         | 50.628    | 0.200     | 83.3         | 244.1793                   | 0.0000                  | OK         |
| 15 minute summer  | 54      | 12          | 52.308    | 1.614     | 86.9         | 1.8255                     | 0.0000                  | SURCHARGED |
| 15 minute summer  | 68_OUT  | 1           | 50.391    | 0.000     | 0.0          | 0.0000                     | 0.0000                  | OK         |
| 15 minute summer  | 67      | 11          | 51.638    | 1.201     | 250.6        | 1.3584                     | 0.0000                  | SURCHARGED |
| 240 minute summer | 67_OUT  | 164         | 50.641    | 0.213     | 135.1        | 0.0000                     | 0.0000                  | OK         |
| 15 minute summer  | 10      | 10          | 55.465    | 0.057     | 7.3          | 0.0640                     | 0.0000                  | OK         |
| 15 minute summer  | 11      | 11          | 54.503    | 0.097     | 11.9         | 0.1292                     | 0.0000                  | OK         |

| Link Event (Outflow) | US Node | Link         | DS Node | Outflow (l/s) | Velocity (m/s) | Flow/Cap | Link Vol (m <sup>3</sup> ) | Discharge Vol (m <sup>3</sup> ) |
|----------------------|---------|--------------|---------|---------------|----------------|----------|----------------------------|---------------------------------|
| 30 minute summer     | 38      | 38           | 39      | 13.3          | 0.755          | 0.858    | 1.2159                     |                                 |
| 30 minute summer     | 38      | Infiltration |         | 1.2           |                |          |                            |                                 |
| 15 minute summer     | 39      | 39           | 41      | 16.0          | 0.954          | 1.035    | 1.4409                     |                                 |
| 30 minute summer     | 39      | Infiltration |         | 3.1           |                |          |                            |                                 |
| 15 minute summer     | 41      | 41           | 42      | 25.3          | 0.701          | 0.724    | 0.3484                     |                                 |
| 30 minute summer     | 41      | Infiltration |         | 2.7           |                |          |                            |                                 |
| 30 minute summer     | 41      | Infiltration |         | 1.7           |                |          |                            |                                 |
| 15 minute summer     | 2       | 2            | 4       | -9.1          | 0.236          | -0.200   | 0.3656                     |                                 |
| 30 minute summer     | 2       | Infiltration |         | 2.3           |                |          |                            |                                 |
| 30 minute summer     | 46      | 46           | 55      | 21.2          | 1.081          | 0.465    | 0.2368                     |                                 |
| 15 minute summer     | 55      | 55           | 60      | 116.0         | 1.052          | 0.910    | 2.8338                     |                                 |
| 15 minute summer     | 60      | 60           | 66      | 237.8         | 2.156          | 2.070    | 1.1507                     |                                 |
| 15 minute summer     | 49      | 49           | 50      | 19.7          | 0.932          | 0.492    | 1.5546                     |                                 |
| 15 minute summer     | 50      | 50           | 51      | 32.5          | 1.331          | 0.644    | 2.1625                     |                                 |
| 15 minute summer     | 51      | 51           | 52      | 44.0          | 1.458          | 0.211    | 4.5412                     |                                 |
| 15 minute summer     | 40      | 40           | 41      | 12.0          | 0.777          | 0.567    | 1.3354                     |                                 |
| 15 minute summer     | 53      | 53           | 54      | 86.2          | 0.822          | 0.472    | 6.9602                     |                                 |
| 15 minute summer     | 68      | Pump         | 68_OUT  | 0.0           |                |          |                            | 0.0                             |
| 240 minute summer    | 68      | Infiltration |         | 41.1          |                |          |                            |                                 |
| 15 minute summer     | 54      | 54           | 55      | 90.3          | 0.819          | 0.886    | 1.1268                     |                                 |
| 15 minute summer     | 67      | 67           | 67_OUT  | 255.8         | 3.485          | 2.486    | 0.2148                     |                                 |
| 15 minute summer     | 10      | 10           | 11      | 7.2           | 0.824          | 0.299    | 0.3760                     |                                 |
| 15 minute summer     | 11      | 11           | 12      | 11.6          | 0.939          | 0.748    | 0.6830                     |                                 |

**Results for 10 year +20% CC Critical Storm Duration. Lowest mass balance: 99.20%**

| Node Event           | US Node | Peak (mins)  | Level (m) | Depth (m)     | Inflow (l/s)   | Node Vol (m <sup>3</sup> ) | Flood (m <sup>3</sup> )    | Status                          |
|----------------------|---------|--------------|-----------|---------------|----------------|----------------------------|----------------------------|---------------------------------|
| 15 minute summer     | 48      | 10           | 54.438    | 0.045         | 6.1            | 0.0513                     | 0.0000                     | OK                              |
| 15 minute summer     | 47      | 10           | 54.798    | 0.047         | 6.2            | 0.0531                     | 0.0000                     | OK                              |
| 15 minute summer     | 52      | 12           | 52.370    | 0.843         | 142.4          | 0.9534                     | 0.0000                     | SURCHARGED                      |
| 15 minute summer     | 25      | 10           | 55.063    | 0.363         | 298.8          | 0.4110                     | 0.0000                     | OK                              |
| 15 minute summer     | 26      | 11           | 54.539    | 0.353         | 295.5          | 0.3998                     | 0.0000                     | OK                              |
| 15 minute summer     | 27      | 11           | 53.852    | 0.248         | 296.5          | 0.4387                     | 0.0000                     | OK                              |
| 15 minute summer     | 30      | 11           | 53.190    | 0.115         | 65.0           | 0.2034                     | 0.0000                     | OK                              |
| 15 minute summer     | 28      | 10           | 54.935    | 0.152         | 44.1           | 0.1717                     | 0.0000                     | OK                              |
| 15 minute summer     | 29      | 11           | 54.434    | 0.150         | 65.3           | 0.1698                     | 0.0000                     | OK                              |
| 15 minute summer     | 36      | 12           | 51.595    | 0.528         | 351.5          | 0.9326                     | 0.0000                     | SURCHARGED                      |
| 15 minute summer     | 36_OUT  | 12           | 51.457    | 0.402         | 352.0          | 0.0000                     | 0.0000                     | OK                              |
| 15 minute summer     | 35      | 13           | 51.847    | 0.152         | 39.0           | 0.1721                     | 0.0000                     | OK                              |
| 30 minute summer     | 42      | 23           | 54.824    | 0.800         | 25.1           | 0.9043                     | 0.0000                     | SURCHARGED                      |
| 15 minute summer     | 24      | 12           | 52.498    | 0.257         | 102.7          | 0.4541                     | 0.0000                     | OK                              |
| 15 minute summer     | 34      | 12           | 51.960    | 0.180         | 41.1           | 0.2040                     | 0.0000                     | OK                              |
| 15 minute summer     | 31      | 10           | 52.561    | 0.094         | 12.2           | 0.1063                     | 0.0000                     | OK                              |
| 15 minute summer     | 32      | 11           | 52.335    | 0.103         | 13.8           | 0.1161                     | 0.0000                     | OK                              |
| 15 minute summer     | 33      | 10           | 52.069    | 0.148         | 29.2           | 0.1674                     | 0.0000                     | OK                              |
| 15 minute summer     | 66      | 12           | 51.971    | 1.455         | 239.3          | 1.6459                     | 0.0000                     | SURCHARGED                      |
| 60 minute summer     | 44      | 44           | 53.452    | 0.214         | 20.7           | 0.1981                     | 0.0000                     | SURCHARGED                      |
| Link Event (Outflow) | US Node | Link         | DS Node   | Outflow (l/s) | Velocity (m/s) | Flow/Cap                   | Link Vol (m <sup>3</sup> ) | Discharge Vol (m <sup>3</sup> ) |
| 15 minute summer     | 11      | Infiltration |           | 0.1           |                |                            |                            |                                 |
| 15 minute summer     | 48      | 48           | 49        | 6.0           | 0.381          | 0.090                      | 0.2233                     |                                 |
| 15 minute summer     | 47      | 47           | 48        | 6.1           | 1.051          | 0.091                      | 0.1256                     |                                 |
| 15 minute summer     | 52      | 52           | 53        | -95.4         | 1.392          | -0.261                     | 1.0234                     |                                 |
| 15 minute summer     | 25      | 25           | 26        | 295.5         | 1.894          | 0.778                      | 13.0234                    |                                 |
| 15 minute summer     | 26      | 26           | 27        | 296.5         | 2.318          | 0.747                      | 11.0377                    |                                 |
| 15 minute summer     | 27      | 27           | 36        | 196.9         | 2.292          | 0.298                      | 0.5382                     |                                 |
| 15 minute summer     | 27      | 27a          | 59        | 98.8          | 1.096          | 0.468                      | 0.7545                     |                                 |
| 15 minute summer     | 30      | 30           | 36        | 27.5          | 1.201          | 0.252                      | 0.1539                     |                                 |
| 15 minute summer     | 30      | 30a          | 59        | 37.2          | 1.607          | 0.259                      | 0.2450                     |                                 |
| 15 minute summer     | 28      | 28           | 29        | 43.3          | 1.230          | 0.495                      | 2.8217                     |                                 |
| 15 minute summer     | 29      | 29           | 30        | 65.0          | 2.163          | 0.457                      | 2.2340                     |                                 |
| 15 minute summer     | 36      | 36           | 36_OUT    | 352.0         | 1.740          | 1.635                      | 1.1681                     | 162.9                           |
| 15 minute summer     | 35      | 35           | 36        | 34.5          | 0.926          | 0.815                      | 2.0630                     |                                 |
| 15 minute summer     | 42      | 42           | 43        | 23.9          | 1.356          | 1.760                      | 0.2601                     |                                 |
| 15 minute summer     | 24      | 24           | 36        | 101.8         | 1.372          | 0.675                      | 0.4966                     |                                 |
| 15 minute summer     | 24      | 24a          | 59        | 26.0          | 0.707          | 0.170                      | 0.8806                     |                                 |
| 15 minute summer     | 34      | 34           | 35        | 39.0          | 1.265          | 0.922                      | 0.3895                     |                                 |
| 15 minute summer     | 34      | 34a          | 66        | 14.9          | 1.057          | 0.287                      | 0.2214                     |                                 |
| 15 minute summer     | 31      | 31           | 32        | 12.1          | 0.999          | 0.679                      | 0.2852                     |                                 |
| 15 minute summer     | 32      | 32           | 33        | 13.6          | 1.085          | 0.765                      | 0.2957                     |                                 |
| 15 minute summer     | 33      | 33           | 34        | 29.1          | 1.340          | 0.732                      | 0.7094                     |                                 |
| 15 minute summer     | 66      | 66           | 67        | 250.6         | 2.273          | 2.182                      | 2.6176                     |                                 |
| 60 minute summer     | 44      | 44           | 45        | 20.0          | 1.192          | 1.067                      | 0.9859                     |                                 |

**Results for 10 year +20% CC Critical Storm Duration. Lowest mass balance: 99.20%**

| Node Event       | US Node | Peak (mins) | Level (m) | Depth (m) | Inflow (l/s) | Node Vol (m <sup>3</sup> ) | Flood (m <sup>3</sup> ) | Status     |
|------------------|---------|-------------|-----------|-----------|--------------|----------------------------|-------------------------|------------|
| 60 minute summer | 43      | 41          | 54.488    | 0.578     | 22.8         | 0.9598                     | 0.0000                  | SURCHARGED |
| 15 minute summer | 45      | 13          | 52.432    | 0.122     | 19.7         | 0.1458                     | 0.0000                  | OK         |
| 15 minute summer | 18      | 12          | 54.876    | 0.230     | 22.0         | 0.3441                     | 0.0000                  | SURCHARGED |
| 60 minute summer | 9       | 41          | 54.353    | 0.599     | 17.9         | 1.4205                     | 0.0000                  | SURCHARGED |
| 60 minute summer | 14      | 42          | 54.204    | 0.534     | 19.8         | 1.2709                     | 0.0000                  | SURCHARGED |
| 60 minute summer | 13      | 42          | 54.205    | 0.385     | 8.6          | 0.8066                     | 0.0000                  | SURCHARGED |
| 15 minute summer | 61      | 12          | 52.931    | 0.023     | 2.1          | 0.1377                     | 0.0000                  | OK         |
| 15 minute summer | 62      | 12          | 52.803    | 0.021     | 0.7          | 0.0033                     | 0.0000                  | OK         |
| 15 minute summer | 64      | 12          | 52.756    | 0.023     | 1.6          | 0.0263                     | 0.0000                  | OK         |
| 15 minute summer | 63      | 11          | 52.986    | 0.026     | 2.4          | 0.1547                     | 0.0000                  | OK         |

| Link Event (Outflow) | US Node | Link         | DS Node | Outflow (l/s) | Velocity (m/s) | Flow/Cap | Link Vol (m <sup>3</sup> ) | Discharge Vol (m <sup>3</sup> ) |
|----------------------|---------|--------------|---------|---------------|----------------|----------|----------------------------|---------------------------------|
| 60 minute summer     | 44      | Infiltration |         | 0.5           |                |          |                            |                                 |
| 30 minute summer     | 43      | 43           | 44      | 20.8          | 1.183          | 1.192    | 0.9296                     |                                 |
| 60 minute summer     | 43      | Infiltration |         | 0.7           |                |          |                            |                                 |
| 60 minute summer     | 45      | 45           | 46      | 19.9          | 0.952          | 0.498    | 0.1990                     |                                 |
| 15 minute summer     | 45      | Infiltration |         | 0.0           |                |          |                            |                                 |
| 15 minute summer     | 18      | 18           | 21      | 21.4          | 1.218          | 1.206    | 0.2435                     |                                 |
| 15 minute summer     | 18      | Infiltration |         | 0.1           |                |          |                            |                                 |
| 60 minute summer     | 9       | 9            | 14      | 16.1          | 0.917          | 1.190    | 0.1918                     |                                 |
| 60 minute summer     | 9       | Infiltration |         | 0.5           |                |          |                            |                                 |
| 60 minute summer     | 14      | 14           | 15      | 17.6          | 0.998          | 1.296    | 0.9015                     |                                 |
| 60 minute summer     | 14      | Infiltration |         | 0.5           |                |          |                            |                                 |
| 15 minute summer     | 13      | 13           | 14      | 7.2           | 0.269          | 0.197    | 0.9227                     |                                 |
| 60 minute summer     | 13      | Infiltration |         | 0.4           |                |          |                            |                                 |
| 15 minute summer     | 61      | 61           | 62      | 0.7           | 0.505          | 0.114    | 0.0110                     |                                 |
| 15 minute summer     | 61      | Infiltration |         | 1.2           |                |          |                            |                                 |
| 15 minute summer     | 62      | 62           | 64      | 0.7           | 0.351          | 0.017    | 0.0163                     |                                 |
| 15 minute summer     | 64      | 64           | 66      | 1.6           | 0.768          | 0.021    | 0.0184                     |                                 |
| 15 minute summer     | 63      | 63           | 64      | 0.9           | 0.600          | 0.137    | 0.0125                     |                                 |
| 15 minute summer     | 63      | Infiltration |         | 1.2           |                |          |                            |                                 |

**Results for 30 year +20% CC Critical Storm Duration. Lowest mass balance: 99.17%**

| Node Event           | US Node | Peak (mins)  | Level (m) | Depth (m)     | Inflow (l/s)   | Node Vol (m <sup>3</sup> ) | Flood (m <sup>3</sup> )    | Status                          |
|----------------------|---------|--------------|-----------|---------------|----------------|----------------------------|----------------------------|---------------------------------|
| 15 minute summer     | 3       | 11           | 57.465    | 1.050         | 27.5           | 0.0000                     | 0.0000                     | FLOOD RISK                      |
| 30 minute summer     | 1       | 20           | 56.405    | 0.442         | 11.3           | 0.0000                     | 0.0000                     | SURCHARGED                      |
| 30 minute summer     | 4       | 23           | 56.343    | 1.009         | 39.2           | 5.2967                     | 0.0000                     | SURCHARGED                      |
| 60 minute summer     | 5       | 41           | 55.710    | 0.969         | 27.5           | 6.5990                     | 0.0000                     | SURCHARGED                      |
| 60 minute summer     | 6       | 41           | 55.272    | 0.946         | 21.1           | 5.0898                     | 0.0000                     | SURCHARGED                      |
| 60 minute summer     | 7       | 38           | 55.002    | 0.972         | 26.3           | 4.0795                     | 0.0000                     | SURCHARGED                      |
| 60 minute summer     | 8       | 40           | 54.665    | 0.829         | 24.0           | 2.3533                     | 0.0000                     | SURCHARGED                      |
| 60 minute summer     | 12      | 42           | 54.335    | 0.345         | 11.3           | 1.3140                     | 0.0000                     | SURCHARGED                      |
| 60 minute summer     | 15      | 44           | 53.484    | 0.208         | 18.6           | 0.5449                     | 0.0000                     | SURCHARGED                      |
| 15 minute summer     | 16      | 11           | 55.574    | 0.086         | 10.0           | 0.0976                     | 0.0000                     | OK                              |
| 15 minute summer     | 17      | 12           | 55.016    | 0.334         | 14.5           | 1.0410                     | 0.0000                     | SURCHARGED                      |
| 30 minute summer     | 21      | 19           | 52.988    | 0.200         | 55.3           | 0.2257                     | 0.0000                     | OK                              |
| 15 minute summer     | 22      | 11           | 52.889    | 0.225         | 74.2           | 0.2543                     | 0.0000                     | OK                              |
| 15 minute summer     | 23      | 13           | 52.721    | 0.311         | 93.4           | 0.3514                     | 0.0000                     | OK                              |
| 15 minute summer     | 59      | 12           | 52.643    | 0.460         | 195.8          | 0.5201                     | 0.0000                     | SURCHARGED                      |
| 30 minute summer     | 37      | 21           | 56.460    | 0.420         | 8.1            | 0.0000                     | 0.0000                     | SURCHARGED                      |
| Link Event (Outflow) | US Node | Link         | DS Node   | Outflow (l/s) | Velocity (m/s) | Flow/Cap                   | Link Vol (m <sup>3</sup> ) | Discharge Vol (m <sup>3</sup> ) |
| 15 minute summer     | 3       | 3            | 4         | 22.2          | 1.260          | 1.136                      | 1.1981                     |                                 |
| 15 minute summer     | 1       | 1            | 2         | 10.2          | 0.681          | 0.756                      | 1.1052                     |                                 |
| 15 minute summer     | 4       | 4            | 5         | 13.8          | 0.826          | 1.016                      | 1.3582                     |                                 |
| 30 minute summer     | 4       | Infiltration |           | 2.9           |                |                            |                            |                                 |
| 15 minute summer     | 5       | 5            | 6         | 14.4          | 0.868          | 1.065                      | 0.9493                     |                                 |
| 60 minute summer     | 5       | Infiltration |           | 4.2           |                |                            |                            |                                 |
| 15 minute summer     | 6       | 6            | 7         | 14.1          | 0.801          | 1.040                      | 0.6777                     |                                 |
| 60 minute summer     | 6       | Infiltration |           | 3.2           |                |                            |                            |                                 |
| 15 minute summer     | 7       | 7            | 8         | 18.3          | 1.042          | 1.352                      | 0.4432                     |                                 |
| 60 minute summer     | 7       | Infiltration |           | 2.5           |                |                            |                            |                                 |
| 30 minute summer     | 8       | 8            | 9         | 20.2          | 1.148          | 1.490                      | 0.1871                     |                                 |
| 60 minute summer     | 8       | Infiltration |           | 1.5           |                |                            |                            |                                 |
| 15 minute summer     | 12      | 12           | 13        | 12.9          | 0.842          | 0.951                      | 0.2168                     |                                 |
| 60 minute summer     | 12      | Infiltration |           | 1.2           |                |                            |                            |                                 |
| 60 minute summer     | 15      | 15           | 21        | 17.8          | 1.025          | 1.146                      | 0.5652                     |                                 |
| 60 minute summer     | 15      | Infiltration |           | 0.7           |                |                            |                            |                                 |
| 15 minute summer     | 16      | 16           | 17        | 9.7           | 0.632          | 0.624                      | 1.1323                     |                                 |
| 15 minute summer     | 17      | 17           | 18        | 14.0          | 0.795          | 0.905                      | 0.0639                     |                                 |
| 15 minute summer     | 17      | Infiltration |           | 1.2           |                |                            |                            |                                 |
| 30 minute summer     | 21      | 21           | 22        | 55.4          | 0.862          | 0.521                      | 2.7868                     |                                 |
| 30 minute summer     | 22      | 22           | 23        | 73.7          | 0.946          | 0.693                      | 7.0033                     |                                 |
| 15 minute summer     | 23      | 23           | 24        | 90.9          | 1.187          | 0.855                      | 6.0925                     |                                 |
| 30 minute summer     | 59      | 59           | 60        | 165.3         | 1.556          | 1.103                      | 6.5329                     |                                 |
| 15 minute summer     | 37      | 37           | 38        | 7.8           | 0.515          | 0.504                      | 0.6692                     |                                 |

**Results for 30 year +20% CC Critical Storm Duration. Lowest mass balance: 99.17%**

| Node Event        | US Node | Peak (mins) | Level (m) | Depth (m) | Inflow (l/s) | Node Vol (m <sup>3</sup> ) | Flood (m <sup>3</sup> ) | Status     |
|-------------------|---------|-------------|-----------|-----------|--------------|----------------------------|-------------------------|------------|
| 30 minute summer  | 38      | 22          | 56.436    | 0.776     | 27.8         | 3.6806                     | 0.0000                  | SURCHARGED |
| 30 minute summer  | 39      | 23          | 56.055    | 1.086     | 40.3         | 7.7614                     | 0.0000                  | SURCHARGED |
| 60 minute summer  | 41      | 40          | 55.038    | 0.962     | 49.3         | 8.7527                     | 0.0000                  | SURCHARGED |
| 30 minute summer  | 2       | 23          | 56.344    | 0.939     | 20.2         | 6.0034                     | 0.0000                  | SURCHARGED |
| 15 minute summer  | 46      | 12          | 52.476    | 0.238     | 23.4         | 0.2694                     | 0.0000                  | SURCHARGED |
| 15 minute summer  | 55      | 12          | 52.448    | 1.792     | 113.8        | 2.0271                     | 0.0000                  | SURCHARGED |
| 15 minute summer  | 60      | 12          | 52.351    | 1.800     | 251.0        | 2.0353                     | 0.0000                  | SURCHARGED |
| 15 minute summer  | 49      | 11          | 54.327    | 0.162     | 25.5         | 0.1835                     | 0.0000                  | OK         |
| 15 minute summer  | 50      | 12          | 53.810    | 0.158     | 44.7         | 0.1790                     | 0.0000                  | OK         |
| 15 minute summer  | 51      | 13          | 52.606    | 0.184     | 56.9         | 0.2077                     | 0.0000                  | OK         |
| 15 minute summer  | 40      | 10          | 56.078    | 0.095     | 15.7         | 0.0000                     | 0.0000                  | OK         |
| 15 minute summer  | 53      | 12          | 52.551    | 1.331     | 104.8        | 1.5058                     | 0.0000                  | SURCHARGED |
| 240 minute summer | 68      | 172         | 50.693    | 0.265     | 95.6         | 325.6345                   | 0.0000                  | SURCHARGED |
| 15 minute summer  | 54      | 12          | 52.475    | 1.781     | 92.1         | 2.0142                     | 0.0000                  | SURCHARGED |
| 15 minute summer  | 68_OUT  | 1           | 50.391    | 0.000     | 0.0          | 0.0000                     | 0.0000                  | OK         |
| 15 minute summer  | 67      | 11          | 51.694    | 1.257     | 272.5        | 1.4212                     | 0.0000                  | SURCHARGED |
| 240 minute summer | 67_OUT  | 172         | 50.708    | 0.280     | 161.8        | 0.0000                     | 0.0000                  | OK         |
| 15 minute summer  | 10      | 10          | 55.473    | 0.065     | 9.3          | 0.0731                     | 0.0000                  | OK         |
| 15 minute summer  | 11      | 11          | 54.523    | 0.117     | 15.2         | 0.1603                     | 0.0000                  | OK         |

| Link Event (Outflow) | US Node | Link         | DS Node | Outflow (l/s) | Velocity (m/s) | Flow/Cap | Link Vol (m <sup>3</sup> ) | Discharge Vol (m <sup>3</sup> ) |
|----------------------|---------|--------------|---------|---------------|----------------|----------|----------------------------|---------------------------------|
| 15 minute summer     | 38      | 38           | 39      | 14.8          | 0.852          | 0.959    | 1.2159                     |                                 |
| 30 minute summer     | 38      | Infiltration |         | 1.9           |                |          |                            |                                 |
| 30 minute summer     | 39      | 39           | 41      | 16.3          | 0.957          | 1.054    | 1.4409                     |                                 |
| 30 minute summer     | 39      | Infiltration |         | 4.1           |                |          |                            |                                 |
| 15 minute summer     | 41      | 41           | 42      | 26.9          | 0.696          | 0.770    | 0.3484                     |                                 |
| 60 minute summer     | 41      | Infiltration |         | 3.5           |                |          |                            |                                 |
| 60 minute summer     | 41      | Infiltration |         | 2.1           |                |          |                            |                                 |
| 15 minute summer     | 2       | 2            | 4       | -12.5         | -0.314         | -0.274   | 0.3656                     |                                 |
| 30 minute summer     | 2       | Infiltration |         | 3.2           |                |          |                            |                                 |
| 15 minute summer     | 46      | 46           | 55      | 26.9          | 1.074          | 0.592    | 0.4802                     |                                 |
| 15 minute summer     | 55      | 55           | 60      | 121.5         | 1.102          | 0.954    | 2.8338                     |                                 |
| 30 minute summer     | 60      | 60           | 66      | 273.2         | 2.477          | 2.378    | 1.1507                     |                                 |
| 15 minute summer     | 49      | 49           | 50      | 25.0          | 0.983          | 0.623    | 1.8783                     |                                 |
| 15 minute summer     | 50      | 50           | 51      | 41.2          | 1.394          | 0.818    | 2.6193                     |                                 |
| 30 minute summer     | 51      | 51           | 52      | 55.6          | 1.510          | 0.267    | 4.7172                     |                                 |
| 15 minute summer     | 40      | 40           | 41      | 15.3          | 0.942          | 0.719    | 1.4319                     |                                 |
| 15 minute winter     | 53      | 53           | 54      | 85.1          | 0.893          | 0.466    | 6.9602                     |                                 |
| 15 minute summer     | 68      | Pump         | 68_OUT  | 0.0           |                |          |                            | 0.0                             |
| 240 minute summer    | 68      | Infiltration |         | 41.7          |                |          |                            |                                 |
| 15 minute summer     | 54      | 54           | 55      | 91.4          | 0.829          | 0.896    | 1.1268                     |                                 |
| 30 minute summer     | 67      | 67           | 67_OUT  | 291.2         | 3.658          | 2.831    | 0.2485                     |                                 |
| 15 minute summer     | 10      | 10           | 11      | 9.2           | 0.868          | 0.381    | 0.4558                     |                                 |
| 15 minute summer     | 11      | 11           | 12      | 14.7          | 0.976          | 0.949    | 0.8491                     |                                 |

**Results for 30 year +20% CC Critical Storm Duration. Lowest mass balance: 99.17%**

| Node Event           | US Node | Peak (mins)  | Level (m) | Depth (m)     | Inflow (l/s)   | Node Vol (m <sup>3</sup> ) | Flood (m <sup>3</sup> )    | Status                          |
|----------------------|---------|--------------|-----------|---------------|----------------|----------------------------|----------------------------|---------------------------------|
| 15 minute summer     | 48      | 10           | 54.444    | 0.051         | 7.8            | 0.0579                     | 0.0000                     | OK                              |
| 15 minute summer     | 47      | 10           | 54.804    | 0.053         | 7.9            | 0.0601                     | 0.0000                     | OK                              |
| 15 minute summer     | 52      | 12           | 52.558    | 1.031         | 100.9          | 1.1657                     | 0.0000                     | SURCHARGED                      |
| 15 minute summer     | 25      | 10           | 55.148    | 0.448         | 378.0          | 0.5071                     | 0.0000                     | OK                              |
| 15 minute summer     | 26      | 11           | 54.608    | 0.422         | 371.6          | 0.4777                     | 0.0000                     | OK                              |
| 15 minute summer     | 27      | 11           | 53.888    | 0.284         | 373.1          | 0.5023                     | 0.0000                     | OK                              |
| 15 minute summer     | 30      | 11           | 53.207    | 0.132         | 82.1           | 0.2335                     | 0.0000                     | OK                              |
| 15 minute summer     | 28      | 10           | 54.959    | 0.176         | 55.7           | 0.1988                     | 0.0000                     | OK                              |
| 15 minute summer     | 29      | 11           | 54.457    | 0.173         | 82.5           | 0.1959                     | 0.0000                     | OK                              |
| 15 minute summer     | 36      | 12           | 51.724    | 0.657         | 473.2          | 1.1605                     | 0.0000                     | SURCHARGED                      |
| 15 minute summer     | 36_OUT  | 12           | 51.513    | 0.458         | 474.4          | 0.0000                     | 0.0000                     | OK                              |
| 15 minute summer     | 35      | 12           | 52.013    | 0.318         | 50.5           | 0.3598                     | 0.0000                     | SURCHARGED                      |
| 60 minute summer     | 42      | 40           | 55.005    | 0.981         | 24.9           | 1.1101                     | 0.0000                     | SURCHARGED                      |
| 15 minute summer     | 24      | 12           | 52.629    | 0.388         | 170.4          | 0.6859                     | 0.0000                     | SURCHARGED                      |
| 15 minute summer     | 34      | 12           | 52.077    | 0.297         | 50.8           | 0.3355                     | 0.0000                     | SURCHARGED                      |
| 15 minute summer     | 31      | 10           | 52.579    | 0.112         | 15.4           | 0.1272                     | 0.0000                     | OK                              |
| 15 minute summer     | 32      | 12           | 52.373    | 0.141         | 17.4           | 0.1589                     | 0.0000                     | OK                              |
| 15 minute summer     | 33      | 12           | 52.191    | 0.270         | 36.8           | 0.3050                     | 0.0000                     | SURCHARGED                      |
| 15 minute summer     | 66      | 12           | 52.077    | 1.561         | 270.1          | 1.7650                     | 0.0000                     | SURCHARGED                      |
| 60 minute summer     | 44      | 45           | 53.516    | 0.278         | 21.6           | 0.3519                     | 0.0000                     | SURCHARGED                      |
| Link Event (Outflow) | US Node | Link         | DS Node   | Outflow (l/s) | Velocity (m/s) | Flow/Cap                   | Link Vol (m <sup>3</sup> ) | Discharge Vol (m <sup>3</sup> ) |
| 15 minute summer     | 11      | Infiltration |           | 0.2           |                |                            |                            |                                 |
| 15 minute summer     | 48      | 48           | 49        | 7.7           | 0.417          | 0.115                      | 0.2553                     |                                 |
| 15 minute summer     | 47      | 47           | 48        | 7.8           | 1.124          | 0.116                      | 0.1496                     |                                 |
| 15 minute summer     | 52      | 52           | 53        | 75.5          | 1.332          | 0.207                      | 1.0234                     |                                 |
| 15 minute summer     | 25      | 25           | 26        | 371.6         | 1.958          | 0.978                      | 15.8204                    |                                 |
| 15 minute summer     | 26      | 26           | 27        | 373.1         | 2.418          | 0.940                      | 13.2194                    |                                 |
| 15 minute summer     | 27      | 27           | 36        | 245.1         | 2.412          | 0.371                      | 0.6360                     |                                 |
| 15 minute summer     | 27      | 27a          | 59        | 126.7         | 1.184          | 0.600                      | 0.8957                     |                                 |
| 15 minute summer     | 30      | 30           | 36        | 35.0          | 1.276          | 0.320                      | 0.1840                     |                                 |
| 15 minute summer     | 30      | 30a          | 59        | 47.0          | 1.700          | 0.327                      | 0.2925                     |                                 |
| 15 minute summer     | 28      | 28           | 29        | 54.7          | 1.298          | 0.626                      | 3.3828                     |                                 |
| 15 minute summer     | 29      | 29           | 30        | 82.1          | 2.279          | 0.578                      | 2.6760                     |                                 |
| 15 minute summer     | 36      | 36           | 36_OUT    | 474.4         | 2.202          | 2.203                      | 1.2354                     | 213.1                           |
| 15 minute summer     | 35      | 35           | 36        | 34.3          | 0.863          | 0.810                      | 2.4011                     |                                 |
| 15 minute summer     | 42      | 42           | 43        | 25.0          | 1.419          | 1.842                      | 0.2601                     |                                 |
| 15 minute summer     | 24      | 24           | 36        | 166.2         | 1.569          | 1.101                      | 0.6855                     |                                 |
| 15 minute summer     | 24      | 24a          | 59        | -58.7         | 0.712          | -0.384                     | 1.0846                     |                                 |
| 15 minute summer     | 34      | 34           | 35        | 50.5          | 1.280          | 1.194                      | 0.5047                     |                                 |
| 15 minute summer     | 34      | 34a          | 66        | -19.0         | 1.072          | -0.366                     | 0.2383                     |                                 |
| 15 minute summer     | 31      | 31           | 32        | 15.2          | 1.039          | 0.858                      | 0.3486                     |                                 |
| 15 minute summer     | 32      | 32           | 33        | 17.2          | 1.109          | 0.966                      | 0.4106                     |                                 |
| 15 minute summer     | 33      | 33           | 34        | 36.3          | 1.377          | 0.914                      | 0.9505                     |                                 |
| 30 minute summer     | 66      | 66           | 67        | 289.6         | 2.626          | 2.521                      | 2.6176                     |                                 |
| 60 minute summer     | 44      | 44           | 45        | 20.6          | 1.190          | 1.101                      | 0.9909                     |                                 |

**Results for 30 year +20% CC Critical Storm Duration. Lowest mass balance: 99.17%**

| Node Event       | US Node | Peak (mins) | Level (m) | Depth (m) | Inflow (l/s) | Node Vol (m <sup>3</sup> ) | Flood (m <sup>3</sup> ) | Status     |
|------------------|---------|-------------|-----------|-----------|--------------|----------------------------|-------------------------|------------|
| 60 minute summer | 43      | 42          | 54.640    | 0.730     | 23.6         | 1.2643                     | 0.0000                  | SURCHARGED |
| 15 minute summer | 45      | 12          | 52.513    | 0.203     | 20.2         | 0.2848                     | 0.0000                  | OK         |
| 15 minute summer | 18      | 12          | 54.990    | 0.344     | 25.9         | 0.5297                     | 0.0000                  | SURCHARGED |
| 60 minute summer | 9       | 41          | 54.497    | 0.743     | 19.4         | 1.7904                     | 0.0000                  | SURCHARGED |
| 60 minute summer | 14      | 42          | 54.329    | 0.659     | 20.4         | 1.5958                     | 0.0000                  | SURCHARGED |
| 60 minute summer | 13      | 42          | 54.330    | 0.510     | 8.5          | 1.1556                     | 0.0000                  | SURCHARGED |
| 15 minute summer | 61      | 12          | 52.935    | 0.027     | 2.7          | 0.1881                     | 0.0000                  | OK         |
| 15 minute summer | 62      | 12          | 52.806    | 0.024     | 0.9          | 0.0038                     | 0.0000                  | OK         |
| 15 minute summer | 64      | 12          | 52.760    | 0.027     | 2.2          | 0.0306                     | 0.0000                  | OK         |
| 15 minute summer | 63      | 11          | 52.990    | 0.030     | 3.1          | 0.2118                     | 0.0000                  | OK         |

| Link Event (Outflow) | US Node | Link         | DS Node | Outflow (l/s) | Velocity (m/s) | Flow/Cap | Link Vol (m <sup>3</sup> ) | Discharge Vol (m <sup>3</sup> ) |
|----------------------|---------|--------------|---------|---------------|----------------|----------|----------------------------|---------------------------------|
| 60 minute summer     | 44      | Infiltration |         | 0.7           |                |          |                            |                                 |
| 30 minute summer     | 43      | 43           | 44      | 21.7          | 1.230          | 1.240    | 0.9296                     |                                 |
| 60 minute summer     | 43      | Infiltration |         | 0.8           |                |          |                            |                                 |
| 15 minute summer     | 45      | 45           | 46      | 21.6          | 0.962          | 0.540    | 0.3648                     |                                 |
| 15 minute summer     | 45      | Infiltration |         | 0.3           |                |          |                            |                                 |
| 15 minute summer     | 18      | 18           | 21      | 25.2          | 1.432          | 1.419    | 0.2475                     |                                 |
| 15 minute summer     | 18      | Infiltration |         | 0.1           |                |          |                            |                                 |
| 60 minute summer     | 9       | 9            | 14      | 17.2          | 0.978          | 1.270    | 0.1918                     |                                 |
| 60 minute summer     | 9       | Infiltration |         | 0.6           |                |          |                            |                                 |
| 60 minute summer     | 14      | 14           | 15      | 18.6          | 1.058          | 1.373    | 0.9015                     |                                 |
| 60 minute summer     | 14      | Infiltration |         | 0.6           |                |          |                            |                                 |
| 15 minute winter     | 13      | 13           | 14      | 7.3           | 0.284          | 0.200    | 0.9227                     |                                 |
| 60 minute summer     | 13      | Infiltration |         | 0.5           |                |          |                            |                                 |
| 15 minute summer     | 61      | 61           | 62      | 0.9           | 0.550          | 0.155    | 0.0137                     |                                 |
| 15 minute summer     | 61      | Infiltration |         | 1.4           |                |          |                            |                                 |
| 15 minute summer     | 62      | 62           | 64      | 0.9           | 0.382          | 0.024    | 0.0204                     |                                 |
| 15 minute summer     | 64      | 64           | 66      | 2.2           | 0.841          | 0.029    | 0.0229                     |                                 |
| 15 minute summer     | 63      | 63           | 64      | 1.3           | 0.653          | 0.186    | 0.0156                     |                                 |
| 15 minute summer     | 63      | Infiltration |         | 1.4           |                |          |                            |                                 |

**Results for 100 year +20% CC Critical Storm Duration. Lowest mass balance: 99.22%**

| Node Event       | US Node | Peak (mins) | Level (m) | Depth (m) | Inflow (l/s) | Node Vol (m <sup>3</sup> ) | Flood (m <sup>3</sup> ) | Status     |
|------------------|---------|-------------|-----------|-----------|--------------|----------------------------|-------------------------|------------|
| 15 minute summer | 3       | 10          | 57.465    | 1.050     | 35.5         | 0.0000                     | 0.0000                  | FLOOD RISK |
| 30 minute summer | 1       | 20          | 56.792    | 0.829     | 14.7         | 0.0000                     | 0.0000                  | FLOOD RISK |
| 30 minute summer | 4       | 24          | 56.663    | 1.329     | 49.8         | 8.3821                     | 0.0000                  | SURCHARGED |
| 60 minute summer | 5       | 42          | 55.999    | 1.258     | 32.5         | 9.6091                     | 0.0000                  | SURCHARGED |
| 60 minute summer | 6       | 41          | 55.550    | 1.224     | 23.4         | 7.1109                     | 0.0000                  | SURCHARGED |
| 60 minute summer | 7       | 38          | 55.289    | 1.259     | 29.9         | 5.5683                     | 0.0000                  | SURCHARGED |
| 60 minute summer | 8       | 40          | 54.890    | 1.054     | 27.1         | 3.1170                     | 0.0000                  | SURCHARGED |
| 60 minute summer | 12      | 43          | 54.498    | 0.508     | 13.8         | 2.5302                     | 0.0000                  | SURCHARGED |
| 60 minute summer | 15      | 46          | 53.529    | 0.253     | 19.9         | 0.7591                     | 0.0000                  | SURCHARGED |
| 15 minute summer | 16      | 11          | 55.591    | 0.103     | 12.9         | 0.1169                     | 0.0000                  | OK         |
| 30 minute summer | 17      | 20          | 55.187    | 0.505     | 18.5         | 2.1552                     | 0.0000                  | SURCHARGED |
| 15 minute summer | 21      | 13          | 53.076    | 0.288     | 65.2         | 0.3252                     | 0.0000                  | OK         |
| 15 minute summer | 22      | 12          | 53.039    | 0.375     | 90.5         | 0.4239                     | 0.0000                  | OK         |
| 15 minute summer | 23      | 11          | 52.945    | 0.535     | 108.2        | 0.6052                     | 0.0000                  | SURCHARGED |
| 15 minute summer | 59      | 11          | 52.843    | 0.660     | 252.7        | 0.7465                     | 0.0000                  | SURCHARGED |
| 30 minute summer | 37      | 22          | 56.896    | 0.856     | 10.6         | 0.0000                     | 0.0000                  | FLOOD RISK |

| Link Event (Outflow) | US Node | Link         | DS Node | Outflow (l/s) | Velocity (m/s) | Flow/Cap | Link Vol (m <sup>3</sup> ) | Discharge Vol (m <sup>3</sup> ) |
|----------------------|---------|--------------|---------|---------------|----------------|----------|----------------------------|---------------------------------|
| 15 minute summer     | 3       | 3            | 4       | 27.7          | 1.571          | 1.417    | 1.1981                     |                                 |
| 15 minute summer     | 1       | 1            | 2       | 11.8          | 0.687          | 0.873    | 1.1052                     |                                 |
| 15 minute summer     | 4       | 4            | 5       | 14.2          | 0.833          | 1.050    | 1.3582                     |                                 |
| 30 minute summer     | 4       | Infiltration |         | 4.2           |                |          |                            |                                 |
| 15 minute summer     | 5       | 5            | 6       | 14.0          | 0.874          | 1.033    | 0.9493                     |                                 |
| 60 minute summer     | 5       | Infiltration |         | 5.6           |                |          |                            |                                 |
| 30 minute winter     | 6       | 6            | 7       | 14.5          | 0.825          | 1.070    | 0.6777                     |                                 |
| 60 minute summer     | 6       | Infiltration |         | 4.1           |                |          |                            |                                 |
| 30 minute summer     | 7       | 7            | 8       | 19.7          | 1.121          | 1.456    | 0.4432                     |                                 |
| 60 minute summer     | 7       | Infiltration |         | 3.1           |                |          |                            |                                 |
| 30 minute summer     | 8       | 8            | 9       | 22.6          | 1.284          | 1.667    | 0.1871                     |                                 |
| 60 minute summer     | 8       | Infiltration |         | 1.8           |                |          |                            |                                 |
| 15 minute summer     | 12      | 12           | 13      | 13.5          | 0.884          | 0.997    | 0.2168                     |                                 |
| 60 minute summer     | 12      | Infiltration |         | 1.7           |                |          |                            |                                 |
| 60 minute summer     | 15      | 15           | 21      | 18.9          | 1.081          | 1.214    | 0.5713                     |                                 |
| 60 minute summer     | 15      | Infiltration |         | 0.8           |                |          |                            |                                 |
| 15 minute summer     | 16      | 16           | 17      | 12.3          | 0.745          | 0.797    | 1.2310                     |                                 |
| 15 minute summer     | 17      | 17           | 18      | 17.3          | 0.981          | 1.116    | 0.0639                     |                                 |
| 30 minute summer     | 17      | Infiltration |         | 1.9           |                |          |                            |                                 |
| 15 minute summer     | 21      | 21           | 22      | 65.5          | 0.864          | 0.616    | 4.3330                     |                                 |
| 15 minute summer     | 22      | 22           | 23      | 89.9          | 0.980          | 0.845    | 9.7982                     |                                 |
| 30 minute summer     | 23      | 23           | 24      | 112.5         | 1.223          | 1.059    | 6.5116                     |                                 |
| 30 minute summer     | 59      | 59           | 60      | 169.6         | 1.564          | 1.132    | 6.6560                     |                                 |
| 15 minute summer     | 37      | 37           | 38      | 8.3           | 0.513          | 0.537    | 0.6692                     |                                 |

**Results for 100 year +20% CC Critical Storm Duration. Lowest mass balance: 99.22%**

| Node Event           | US Node | Peak (mins)  | Level (m) | Depth (m)     | Inflow (l/s)   | Node Vol (m <sup>3</sup> ) | Flood (m <sup>3</sup> )    | Status                          |
|----------------------|---------|--------------|-----------|---------------|----------------|----------------------------|----------------------------|---------------------------------|
| 30 minute summer     | 38      | 22           | 56.864    | 1.204         | 33.9           | 6.3617                     | 0.0000                     | SURCHARGED                      |
| 30 minute summer     | 39      | 23           | 56.417    | 1.448         | 49.4           | 11.5527                    | 0.0000                     | FLOOD RISK                      |
| 30 minute summer     | 41      | 24           | 55.303    | 1.227         | 70.1           | 13.7811                    | 0.0000                     | SURCHARGED                      |
| 30 minute summer     | 2       | 24           | 56.663    | 1.258         | 25.9           | 9.0733                     | 0.0000                     | SURCHARGED                      |
| 15 minute summer     | 46      | 12           | 52.700    | 0.462         | 28.3           | 0.5226                     | 0.0000                     | SURCHARGED                      |
| 15 minute summer     | 55      | 12           | 52.687    | 2.031         | 130.6          | 2.2976                     | 0.0000                     | SURCHARGED                      |
| 15 minute summer     | 60      | 12           | 52.536    | 1.985         | 268.5          | 2.2454                     | 0.0000                     | SURCHARGED                      |
| 15 minute summer     | 49      | 11           | 54.352    | 0.187         | 33.0           | 0.2111                     | 0.0000                     | OK                              |
| 15 minute summer     | 50      | 12           | 53.923    | 0.271         | 57.8           | 0.3070                     | 0.0000                     | SURCHARGED                      |
| 15 minute summer     | 51      | 12           | 53.002    | 0.580         | 72.5           | 0.6554                     | 0.0000                     | SURCHARGED                      |
| 30 minute summer     | 40      | 20           | 56.272    | 0.289         | 19.5           | 0.0000                     | 0.0000                     | SURCHARGED                      |
| 15 minute summer     | 53      | 12           | 52.875    | 1.655         | 86.6           | 1.8715                     | 0.0000                     | FLOOD RISK                      |
| 240 minute winter    | 68      | 192          | 50.790    | 0.362         | 88.2           | 448.0693                   | 0.0000                     | SURCHARGED                      |
| 15 minute summer     | 54      | 12           | 52.741    | 2.047         | 94.9           | 2.3152                     | 0.0000                     | SURCHARGED                      |
| 15 minute summer     | 68_OUT  | 1            | 50.391    | 0.000         | 0.0            | 0.0000                     | 0.0000                     | OK                              |
| 15 minute summer     | 67      | 10           | 51.762    | 1.325         | 291.0          | 1.4987                     | 0.0000                     | SURCHARGED                      |
| 240 minute winter    | 67_OUT  | 188          | 50.806    | 0.378         | 139.1          | 0.0000                     | 0.0000                     | OK                              |
| 15 minute summer     | 10      | 10           | 55.483    | 0.075         | 12.0           | 0.0847                     | 0.0000                     | OK                              |
| 30 minute summer     | 11      | 20           | 54.694    | 0.288         | 19.0           | 0.5259                     | 0.0000                     | SURCHARGED                      |
| Link Event (Outflow) | US Node | Link         | DS Node   | Outflow (l/s) | Velocity (m/s) | Flow/Cap                   | Link Vol (m <sup>3</sup> ) | Discharge Vol (m <sup>3</sup> ) |
| 15 minute winter     | 38      | 38           | 39        | 14.7          | 0.852          | 0.949                      | 1.2159                     |                                 |
| 30 minute summer     | 38      | Infiltration |           | 2.9           |                |                            |                            |                                 |
| 30 minute winter     | 39      | 39           | 41        | 17.0          | 0.965          | 1.097                      | 1.4409                     |                                 |
| 30 minute summer     | 39      | Infiltration |           | 5.6           |                |                            |                            |                                 |
| 15 minute summer     | 41      | 41           | 42        | 28.6          | 0.719          | 0.818                      | 0.3484                     |                                 |
| 30 minute summer     | 41      | Infiltration |           | 4.8           |                |                            |                            |                                 |
| 30 minute summer     | 41      | Infiltration |           | 3.1           |                |                            |                            |                                 |
| 15 minute summer     | 2       | 2            | 4         | -15.1         | -0.380         | -0.332                     | 0.3656                     |                                 |
| 30 minute summer     | 2       | Infiltration |           | 4.5           |                |                            |                            |                                 |
| 15 minute summer     | 46      | 46           | 55        | 30.7          | 1.094          | 0.674                      | 0.4802                     |                                 |
| 15 minute summer     | 55      | 55           | 60        | 133.9         | 1.214          | 1.051                      | 2.8338                     |                                 |
| 30 minute summer     | 60      | 60           | 66        | 286.5         | 2.598          | 2.494                      | 1.1507                     |                                 |
| 15 minute summer     | 49      | 49           | 50        | 32.3          | 1.025          | 0.805                      | 2.3353                     |                                 |
| 30 minute summer     | 50      | 50           | 51        | 51.7          | 1.426          | 1.026                      | 3.2455                     |                                 |
| 15 minute summer     | 51      | 51           | 52        | 72.1          | 1.504          | 0.347                      | 7.1686                     |                                 |
| 15 minute summer     | 40      | 40           | 41        | 18.8          | 1.087          | 0.885                      | 1.7179                     |                                 |
| 15 minute summer     | 53      | 53           | 54        | 89.2          | 0.850          | 0.489                      | 6.9602                     |                                 |
| 15 minute summer     | 68      | Pump         | 68_OUT    | 0.0           |                |                            |                            | 0.0                             |
| 240 minute winter    | 68      | Infiltration |           | 42.7          |                |                            |                            |                                 |
| 15 minute summer     | 54      | 54           | 55        | 95.8          | 0.869          | 0.939                      | 1.1268                     |                                 |
| 30 minute summer     | 67      | 67           | 67_OUT    | 311.6         | 3.812          | 3.028                      | 0.2761                     |                                 |
| 15 minute summer     | 10      | 10           | 11        | 11.9          | 0.907          | 0.493                      | 0.5483                     |                                 |
| 15 minute summer     | 11      | 11           | 12        | 16.5          | 1.004          | 1.064                      | 0.9525                     |                                 |

**Results for 100 year +20% CC Critical Storm Duration. Lowest mass balance: 99.22%**

| Node Event           | US Node | Peak (mins)  | Level (m) | Depth (m)     | Inflow (l/s)   | Node Vol (m <sup>3</sup> ) | Flood (m <sup>3</sup> )    | Status                          |
|----------------------|---------|--------------|-----------|---------------|----------------|----------------------------|----------------------------|---------------------------------|
| 15 minute summer     | 48      | 10           | 54.451    | 0.058         | 10.1           | 0.0660                     | 0.0000                     | OK                              |
| 15 minute summer     | 47      | 10           | 54.812    | 0.061         | 10.2           | 0.0687                     | 0.0000                     | OK                              |
| 15 minute summer     | 52      | 12           | 52.898    | 1.371         | 100.1          | 1.5506                     | 0.0000                     | FLOOD RISK                      |
| 15 minute summer     | 25      | 11           | 55.868    | 1.168         | 489.0          | 1.3211                     | 0.0000                     | SURCHARGED                      |
| 15 minute summer     | 26      | 11           | 54.982    | 0.796         | 479.8          | 0.9000                     | 0.0000                     | SURCHARGED                      |
| 15 minute summer     | 27      | 11           | 53.932    | 0.328         | 472.1          | 0.5797                     | 0.0000                     | OK                              |
| 15 minute summer     | 30      | 11           | 53.230    | 0.155         | 106.2          | 0.2731                     | 0.0000                     | OK                              |
| 15 minute summer     | 28      | 10           | 54.994    | 0.211         | 72.1           | 0.2381                     | 0.0000                     | OK                              |
| 15 minute summer     | 29      | 11           | 54.490    | 0.206         | 106.7          | 0.2335                     | 0.0000                     | OK                              |
| 15 minute summer     | 36      | 11           | 51.878    | 0.811         | 623.8          | 1.4330                     | 0.0000                     | SURCHARGED                      |
| 15 minute summer     | 36_OUT  | 11           | 51.549    | 0.494         | 621.4          | 0.0000                     | 0.0000                     | OK                              |
| 15 minute summer     | 35      | 11           | 52.163    | 0.468         | 53.4           | 0.5289                     | 0.0000                     | SURCHARGED                      |
| 30 minute summer     | 42      | 24           | 55.267    | 1.243         | 27.9           | 1.4062                     | 0.0000                     | SURCHARGED                      |
| 15 minute summer     | 24      | 11           | 52.783    | 0.542         | 242.2          | 0.9568                     | 0.0000                     | SURCHARGED                      |
| 15 minute summer     | 34      | 11           | 52.239    | 0.459         | 55.8           | 0.5195                     | 0.0000                     | SURCHARGED                      |
| 15 minute summer     | 31      | 12           | 52.939    | 0.472         | 19.9           | 0.5342                     | 0.0000                     | FLOOD RISK                      |
| 15 minute summer     | 32      | 12           | 52.707    | 0.475         | 20.4           | 0.5376                     | 0.0000                     | SURCHARGED                      |
| 15 minute summer     | 33      | 11           | 52.422    | 0.501         | 43.5           | 0.5663                     | 0.0000                     | SURCHARGED                      |
| 15 minute summer     | 66      | 11           | 52.237    | 1.721         | 288.1          | 1.9470                     | 0.0000                     | SURCHARGED                      |
| 60 minute summer     | 44      | 47           | 53.603    | 0.365         | 22.8           | 0.6314                     | 0.0000                     | SURCHARGED                      |
| Link Event (Outflow) | US Node | Link         | DS Node   | Outflow (l/s) | Velocity (m/s) | Flow/Cap                   | Link Vol (m <sup>3</sup> ) | Discharge Vol (m <sup>3</sup> ) |
| 30 minute summer     | 11      | Infiltration |           | 0.5           |                |                            |                            |                                 |
| 15 minute summer     | 48      | 48           | 49        | 10.0          | 0.455          | 0.149                      | 0.2956                     |                                 |
| 15 minute summer     | 47      | 47           | 48        | 10.1          | 1.207          | 0.150                      | 0.1801                     |                                 |
| 15 minute summer     | 52      | 52           | 53        | 78.0          | 1.374          | 0.214                      | 1.0234                     |                                 |
| 15 minute summer     | 25      | 25           | 26        | 479.8         | 2.221          | 1.263                      | 18.0307                    |                                 |
| 15 minute summer     | 26      | 26           | 27        | 472.1         | 2.495          | 1.189                      | 15.4887                    |                                 |
| 15 minute summer     | 27      | 27           | 36        | 306.6         | 2.541          | 0.464                      | 0.7538                     |                                 |
| 15 minute summer     | 27      | 27a          | 59        | 163.5         | 1.284          | 0.775                      | 1.0644                     |                                 |
| 15 minute summer     | 30      | 30           | 36        | 45.4          | 1.360          | 0.416                      | 0.2242                     |                                 |
| 15 minute summer     | 30      | 30a          | 59        | 60.6          | 1.803          | 0.422                      | 0.3554                     |                                 |
| 15 minute summer     | 28      | 28           | 29        | 70.7          | 1.365          | 0.809                      | 4.1570                     |                                 |
| 15 minute summer     | 29      | 29           | 30        | 106.2         | 2.398          | 0.748                      | 3.2803                     |                                 |
| 15 minute summer     | 36      | 36           | 36_OUT    | 621.4         | 2.877          | 2.886                      | 1.2672                     | 283.8                           |
| 15 minute winter     | 35      | 35           | 36        | 34.9          | 0.879          | 0.825                      | 2.4011                     |                                 |
| 15 minute summer     | 42      | 42           | 43        | 26.1          | 1.484          | 1.926                      | 0.2601                     |                                 |
| 15 minute summer     | 24      | 24           | 36        | 237.5         | 2.154          | 1.574                      | 0.7238                     |                                 |
| 15 minute summer     | 24      | 24a          | 59        | -114.2        | -1.036         | -0.746                     | 1.0846                     |                                 |
| 15 minute winter     | 34      | 34           | 35        | 54.1          | 1.362          | 1.278                      | 0.5047                     |                                 |
| 30 minute summer     | 34      | 34a          | 66        | 22.1          | 1.119          | 0.425                      | 0.2344                     |                                 |
| 30 minute summer     | 31      | 31           | 32        | 17.8          | 1.058          | 1.004                      | 0.4144                     |                                 |
| 15 minute summer     | 32      | 32           | 33        | 20.4          | 1.160          | 1.150                      | 0.4160                     |                                 |
| 30 minute summer     | 33      | 33           | 34        | 43.6          | 1.437          | 1.098                      | 0.9344                     |                                 |
| 30 minute summer     | 66      | 66           | 67        | 310.3         | 2.813          | 2.701                      | 2.6176                     |                                 |
| 60 minute summer     | 44      | 44           | 45        | 21.4          | 1.215          | 1.141                      | 0.9960                     |                                 |

**Results for 100 year +20% CC Critical Storm Duration. Lowest mass balance: 99.22%**

| Node Event       | US Node | Peak (mins) | Level (m) | Depth (m) | Inflow (l/s) | Node Vol (m <sup>3</sup> ) | Flood (m <sup>3</sup> ) | Status     |
|------------------|---------|-------------|-----------|-----------|--------------|----------------------------|-------------------------|------------|
| 30 minute summer | 43      | 25          | 54.849    | 0.939     | 25.9         | 1.6810                     | 0.0000                  | SURCHARGED |
| 15 minute summer | 45      | 12          | 52.709    | 0.399     | 21.2         | 0.8793                     | 0.0000                  | SURCHARGED |
| 30 minute summer | 18      | 20          | 55.147    | 0.501     | 31.1         | 0.7845                     | 0.0000                  | SURCHARGED |
| 60 minute summer | 9       | 41          | 54.687    | 0.933     | 21.5         | 2.2773                     | 0.0000                  | SURCHARGED |
| 60 minute summer | 14      | 43          | 54.491    | 0.821     | 21.4         | 2.0170                     | 0.0000                  | SURCHARGED |
| 60 minute summer | 13      | 43          | 54.492    | 0.672     | 8.2          | 1.6086                     | 0.0000                  | SURCHARGED |
| 15 minute summer | 61      | 12          | 52.941    | 0.033     | 3.5          | 0.2696                     | 0.0000                  | OK         |
| 15 minute summer | 62      | 12          | 52.810    | 0.028     | 1.3          | 0.0045                     | 0.0000                  | OK         |
| 15 minute summer | 64      | 12          | 52.765    | 0.032     | 3.1          | 0.0361                     | 0.0000                  | OK         |
| 30 minute summer | 63      | 19          | 52.996    | 0.036     | 3.8          | 0.2982                     | 0.0000                  | OK         |

| Link Event (Outflow) | US Node | Link         | DS Node | Outflow (l/s) | Velocity (m/s) | Flow/Cap | Link Vol (m <sup>3</sup> ) | Discharge Vol (m <sup>3</sup> ) |
|----------------------|---------|--------------|---------|---------------|----------------|----------|----------------------------|---------------------------------|
| 60 minute summer     | 44      | Infiltration |         | 0.9           |                |          |                            |                                 |
| 30 minute summer     | 43      | 43           | 44      | 22.9          | 1.299          | 1.309    | 0.9296                     |                                 |
| 30 minute summer     | 43      | Infiltration |         | 1.0           |                |          |                            |                                 |
| 15 minute summer     | 45      | 45           | 46      | 27.2          | 0.971          | 0.681    | 0.3742                     |                                 |
| 15 minute summer     | 45      | Infiltration |         | 0.8           |                |          |                            |                                 |
| 30 minute summer     | 18      | 18           | 21      | 30.3          | 1.723          | 1.708    | 0.2490                     |                                 |
| 30 minute summer     | 18      | Infiltration |         | 0.2           |                |          |                            |                                 |
| 30 minute summer     | 9       | 9            | 14      | 19.2          | 1.088          | 1.412    | 0.1918                     |                                 |
| 60 minute summer     | 9       | Infiltration |         | 0.7           |                |          |                            |                                 |
| 60 minute summer     | 14      | 14           | 15      | 19.9          | 1.130          | 1.466    | 0.9015                     |                                 |
| 60 minute summer     | 14      | Infiltration |         | 0.7           |                |          |                            |                                 |
| 15 minute summer     | 13      | 13           | 14      | 7.9           | 0.274          | 0.216    | 0.9227                     |                                 |
| 60 minute summer     | 13      | Infiltration |         | 0.6           |                |          |                            |                                 |
| 15 minute summer     | 61      | 61           | 62      | 1.3           | 0.604          | 0.219    | 0.0176                     |                                 |
| 15 minute summer     | 61      | Infiltration |         | 1.6           |                |          |                            |                                 |
| 15 minute summer     | 62      | 62           | 64      | 1.3           | 0.421          | 0.033    | 0.0261                     |                                 |
| 15 minute summer     | 64      | 64           | 66      | 3.1           | 0.926          | 0.041    | 0.0290                     |                                 |
| 15 minute summer     | 63      | 63           | 64      | 1.8           | 0.713          | 0.257    | 0.0197                     |                                 |
| 30 minute summer     | 63      | Infiltration |         | 1.7           |                |          |                            |                                 |

# Appendix D. Foul sewer calculations



**Design Settings**

|                                   |      |                             |               |
|-----------------------------------|------|-----------------------------|---------------|
| Frequency of use (kDU)            | 0.00 | Minimum Velocity (m/s)      | 0.75          |
| Flow per dwelling per day (l/day) | 0    | Connection Type             | Level Soffits |
| Domestic Flow (l/s/ha)            | 0.0  | Minimum Backdrop Height (m) | 0.200         |
| Industrial Flow (l/s/ha)          | 0.0  | Preferred Cover Depth (m)   | 1.200         |
| Additional Flow (%)               | 0    | Include Intermediate Ground | ✓             |

**Nodes**

| Name                       | Add Inflow (l/s) | Cover Level (m) | Diameter (mm) | Easting (m) | Northing (m) | Depth (m) |
|----------------------------|------------------|-----------------|---------------|-------------|--------------|-----------|
| FW-1                       | 0.1              | 55.570          |               | 546608.264  | 728161.994   | 1.350     |
| FW-2                       |                  | 54.590          | 1500          | 546656.914  | 728203.691   | 1.711     |
| FW-3                       |                  | 54.830          | 1200          | 546649.328  | 728210.469   | 1.669     |
| FW-4                       | 0.1              | 55.200          |               | 546621.197  | 728152.898   | 1.350     |
| FW-5                       |                  | 55.340          | 1200          | 546616.790  | 728156.642   | 1.586     |
| FW-6                       | 0.1              | 53.500          |               | 546687.406  | 728226.881   | 1.050     |
| FW-7                       |                  | 53.860          | 1800          | 546681.363  | 728232.124   | 1.555     |
| FW-10                      |                  | 54.580          | 1200          | 546663.317  | 728198.349   | 1.763     |
| FW-8 Decompression manhole |                  | 54.300          | 1200          | 546663.287  | 728210.855   | 1.350     |
| FW-9                       |                  | 54.590          | 1200          | 546658.866  | 728202.079   | 1.730     |

**Links**

| Name  | US Node                    | DS Node                    | Length (m) | ks (mm) / n | US IL (m) | DS IL (m) | Fall (m) | Slope (1:X) | Dia (mm) |
|-------|----------------------------|----------------------------|------------|-------------|-----------|-----------|----------|-------------|----------|
| 1.000 | FW-1                       | FW-3                       | 63.532     | 1.500       | 54.220    | 53.161    | 1.059    | 60.0        | 150      |
| 2.001 | FW-5                       | FW-2                       | 61.835     | 1.500       | 53.754    | 53.091    | 0.663    | 93.3        | 150      |
| 2.000 | FW-4                       | FW-5                       | 5.783      | 1.500       | 53.850    | 53.754    | 0.096    | 60.0        | 150      |
| 1.002 | FW-2                       | FW-9                       | 2.532      | 1.500       | 52.879    | 52.860    | 0.019    | 135.0       | 150      |
| 1.001 | FW-3                       | FW-2                       | 10.173     | 1.500       | 53.161    | 53.086    | 0.075    | 135.0       | 150      |
| 3.000 | FW-6                       | FW-7                       | 8.001      | 1.500       | 52.450    | 52.317    | 0.133    | 60.0        | 150      |
| 3.002 | FW-8 Decompression manhole | FW-2                       | 9.589      | 0.300       | 52.950    | 52.879    | 0.071    | 135.0       | 150      |
| 1.003 | FW-9                       | FW-10                      | 5.807      | 1.500       | 52.860    | 52.817    | 0.043    | 135.0       | 150      |
| 3.001 | FW-7                       | FW-8 Decompression manhole | 27.912     | 1.500       | 52.305    | 52.950    | -0.645   | -43.3       | 60       |

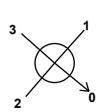
| Name  | Pro Vel @ 1/3 Q (m/s) | Vel (m/s) | Cap (l/s) | Flow (l/s) | US Depth (m) | DS Depth (m) | Σ Area (ha) | Σ Dwellings (ha) | Σ Units (ha) | Σ Add Inflow (ha) | Pro Depth (mm) | Pro Velocity (m/s) |
|-------|-----------------------|-----------|-----------|------------|--------------|--------------|-------------|------------------|--------------|-------------------|----------------|--------------------|
| 1.000 | 0.192                 | 1.132     | 20.0      | 0.1        | 1.200        | 1.519        | 0.000       | 0                | 0.0          | 0.1               | 8              | 0.274              |
| 2.001 | 0.167                 | 0.907     | 16.0      | 0.1        | 1.436        | 1.349        | 0.000       | 0                | 0.0          | 0.1               | 9              | 0.243              |
| 2.000 | 0.192                 | 1.132     | 20.0      | 0.1        | 1.200        | 1.436        | 0.000       | 0                | 0.0          | 0.1               | 8              | 0.274              |
| 1.002 | 0.212                 | 0.753     | 13.3      | 0.3        | 1.561        | 1.580        | 0.000       | 0                | 0.0          | 0.3               | 16             | 0.305              |
| 1.001 | 0.150                 | 0.753     | 13.3      | 0.1        | 1.519        | 1.354        | 0.000       | 0                | 0.0          | 0.1               | 10             | 0.211              |
| 3.000 | 0.192                 | 1.132     | 20.0      | 0.1        | 0.900        | 1.393        | 0.000       | 0                | 0.0          | 0.1               | 8              | 0.274              |
| 3.002 | 0.172                 | 0.940     | 16.6      | 0.1        | 1.200        | 1.561        | 0.000       | 0                | 0.0          | 0.1               | 8              | 0.254              |
| 1.003 | 0.211                 | 0.753     | 13.3      | 0.3        | 1.580        | 1.613        | 0.000       | 0                | 0.0          | 0.3               | 16             | 0.303              |
| 3.001 | 0.000                 | 0.750     | 2.1       | 0.1        | 1.495        | 1.290        | 0.000       | 0                | 0.0          | 0.1               | 150            | 0.000              |

**Pipeline Schedule**

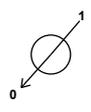
| Link  | Length (m) | Slope (1:X) | Dia (mm) | Link Type    | US CL (m) | US IL (m) | US Depth (m) | DS CL (m) | DS IL (m) | DS Depth (m) |
|-------|------------|-------------|----------|--------------|-----------|-----------|--------------|-----------|-----------|--------------|
| 1.000 | 63.532     | 60.0        | 150      | Carrierdrain | 55.570    | 54.220    | 1.200        | 54.830    | 53.161    | 1.519        |
| 2.001 | 61.835     | 93.3        | 150      | Carrierdrain | 55.340    | 53.754    | 1.436        | 54.590    | 53.091    | 1.349        |
| 2.000 | 5.783      | 60.0        | 150      | Carrierdrain | 55.200    | 53.850    | 1.200        | 55.340    | 53.754    | 1.436        |
| 1.002 | 2.532      | 135.0       | 150      | Carrierdrain | 54.590    | 52.879    | 1.561        | 54.590    | 52.860    | 1.580        |
| 1.001 | 10.173     | 135.0       | 150      | Carrierdrain | 54.830    | 53.161    | 1.519        | 54.590    | 53.086    | 1.354        |
| 3.000 | 8.001      | 60.0        | 150      | Carrierdrain | 53.500    | 52.450    | 0.900        | 53.860    | 52.317    | 1.393        |
| 3.002 | 9.589      | 135.0       | 150      | Carrierdrain | 54.300    | 52.950    | 1.200        | 54.590    | 52.879    | 1.561        |
| 1.003 | 5.807      | 135.0       | 150      | Carrierdrain | 54.590    | 52.860    | 1.580        | 54.580    | 52.817    | 1.613        |
| 3.001 | 27.912     | -43.3       | 60       | Carrierdrain | 53.860    | 52.305    | 1.495        | 54.300    | 52.950    | 1.290        |

| Link  | US Node                    | Dia (mm) | Node Type | MH Type   | DS Node                    | Dia (mm) | Node Type | MH Type   |
|-------|----------------------------|----------|-----------|-----------|----------------------------|----------|-----------|-----------|
| 1.000 | FW-1                       |          | Junction  |           | FW-3                       | 1200     | Manhole   | Adoptable |
| 2.001 | FW-5                       | 1200     | Manhole   | Adoptable | FW-2                       | 1500     | Manhole   | Adoptable |
| 2.000 | FW-4                       |          | Junction  |           | FW-5                       | 1200     | Manhole   | Adoptable |
| 1.002 | FW-2                       | 1500     | Manhole   | Adoptable | FW-9                       | 1200     | Manhole   | Adoptable |
| 1.001 | FW-3                       | 1200     | Manhole   | Adoptable | FW-2                       | 1500     | Manhole   | Adoptable |
| 3.000 | FW-6                       |          | Junction  |           | FW-7                       | 1800     | Manhole   | Adoptable |
| 3.002 | FW-8 Decompression manhole | 1200     | Manhole   | Adoptable | FW-2                       | 1500     | Manhole   | Adoptable |
| 1.003 | FW-9                       | 1200     | Manhole   | Adoptable | FW-10                      | 1200     | Manhole   | Adoptable |
| 3.001 | FW-7                       | 1800     | Manhole   | Adoptable | FW-8 Decompression manhole | 1200     | Manhole   | Adoptable |

**Manhole Schedule**

| Node | Easting (m) | Northing (m) | CL (m) | Depth (m) | Dia (mm) | Connections  | Link  | IL (m) | Dia (mm) |
|------|-------------|--------------|--------|-----------|----------|--|-------|--------|----------|
| FW-1 | 546608.264  | 728161.994   | 55.570 | 1.350     |          |  |       |        |          |
|      |             |              |        |           |          | 0  | 1.000 | 54.220 | 150      |
| FW-2 | 546656.914  | 728203.691   | 54.590 | 1.711     | 1500     |  | 1     | 3.002  | 52.879   |
|      |             |              |        |           |          | 2  | 2.001 | 53.091 | 150      |
|      |             |              |        |           |          | 3  | 1.001 | 53.086 | 150      |
|      |             |              |        |           |          | 0  | 1.002 | 52.879 | 150      |
| FW-3 | 546649.328  | 728210.469   | 54.830 | 1.669     | 1200     |  | 1     | 1.000  | 53.161   |
|      |             |              |        |           |          | 0  | 1.001 | 53.161 | 150      |
| FW-4 | 546621.197  | 728152.898   | 55.200 | 1.350     |          |   |       |        |          |
|      |             |              |        |           |          | 0  | 2.000 | 53.850 | 150      |
| FW-5 | 546616.790  | 728156.642   | 55.340 | 1.586     | 1200     |  | 1     | 2.000  | 53.754   |
|      |             |              |        |           |          | 0  | 2.001 | 53.754 | 150      |
| FW-6 | 546687.406  | 728226.881   | 53.500 | 1.050     |          |   |       |        |          |
|      |             |              |        |           |          | 0  | 3.000 | 52.450 | 150      |

**Manhole Schedule**

| Node                       | Easting<br>(m) | Northing<br>(m) | CL<br>(m) | Depth<br>(m) | Dia<br>(mm) | Connections   | Link | IL<br>(m) | Dia<br>(mm) |     |
|----------------------------|----------------|-----------------|-----------|--------------|-------------|---|------|-----------|-------------|-----|
| FW-7                       | 546681.363     | 728232.124      | 53.860    | 1.555        | 1800        |  | 1    | 3.000     | 52.317      | 150 |
| FW-10                      | 546663.317     | 728198.349      | 54.580    | 1.763        | 1200        |  | 1    | 1.003     | 52.817      | 150 |
| FW-8 Decompression manhole | 546663.287     | 728210.855      | 54.300    | 1.350        | 1200        |  | 1    | 3.001     | 52.950      | 60  |
| FW-9                       | 546658.866     | 728202.079      | 54.590    | 1.730        | 1200        |  | 1    | 1.002     | 52.860      | 150 |
|                            |                |                 |           |              |             |   | 0    | 1.003     | 52.860      | 150 |

# Appendix E. Uisce Éireann Pre-Connection Application and Confirmation of Feasibility



# Pre-connection enquiry form

## Business developments, mixed use developments, housing developments



This form is to be filled out by applicants enquiring about the feasibility of a water and/or wastewater connection to Uisce Éireann infrastructure. If completing this form by hand, please use BLOCK CAPITALS and black ink. Please note that this is a digital PDF form and can be filled in electronically

Please refer to the **Guide to completing the pre-connection enquiry form** on page 14 of this document when completing the form.

**\* Denotes mandatory/ required field. Please note, if mandatory fields are not completed the application will be returned.**

### Section A | Applicant details

#### 1 \*Applicant details:

Registered company name (if applicable):

Trading name (if applicable):

Company registration number (if applicable):

Parent company registered company name (if applicable):

Parent company registration number (if applicable):

If you are not a registered company/business, please provide the applicant's name:

\*Contact name:

\*Postal address:

\*Eircode:

Please provide either a landline or a mobile number

Landline:

\*Mobile:

\*Email:

**2 Agent details (if applicable):**

The fields marked with \* in this section are mandatory if using an agent

\*Contact name:

Company name (if applicable):

\*Postal address:

\*Eircode:

Please provide either a landline or a mobile number

Landline:

\*Mobile

\*Email: .com

**3 \*Please indicate whether it is the applicant or agent who should receive future correspondence in relation to the enquiry:**

Applicant

Agent

**Section B | Site details**

**4 \*Site address 1 (include Site name/Building name/Building number):**

\*Address 2

\*Address 3

\*City/Town

\*County  Eircode

**5 \*Irish Grid co-ordinates (proposed connection point):**

Eastings (X)  Northings (Y)

Note: Values for Eastings must be between 015,900 and 340,000. Northings, between 029,000 and 362,000  
Eg. co-ordinates of GPO, O'Connell St., Dublin: E(X) 315,878 N(Y) 234,619

**6 \*Local Authority where proposed development is located:**

**7 \*Has full planning permission been granted?** Yes  No

If 'Yes', please provide the current or previous planning reference number:





## Section D | Water connection and demand details

13 **\*Is there an existing connection to public water mains at the site?** Yes  No

13.1 If yes, is this enquiry for an additional connection to one already installed? Yes  No

13.2 If yes, is this enquiry to increase the size of an existing connection? Yes  No

14 **Approximate date water connection is required:** / /

15 **\*What diameter of water connection is required to service the development?**  mm

16 **\*Is more than one connection required to the public infrastructure to service this development?** Yes  No

If 'Yes', how many?

17 **Please indicate the business water demand (shops, offices, schools, hotels, restaurants, etc.):**

|  |  |     |
|--|--|-----|
| Post-development peak hour water demand    |  | I/s |
| Post-development average hour water demand |  | I/s |

Please include calculations on the attached sheet provided. Where there will be a daily/weekly/seasonal variation in the water demand profile, please provide all such details.

18 **Please indicate the industrial water demand (industry-specific water requirements):**

|  |  |     |
|--|--|-----|
| Post-development peak hour water demand    |  | I/s |
| Post-development average hour water demand |  | I/s |

Please include calculations on the attached sheet provided. Where there will be a daily/weekly/seasonal variation in the water demand profile, please provide all such details.

19 **What is the existing ground level at the property boundary at connection point (if known) above Malin Head Ordnance Datum?**

 m

20 **What is the highest finished floor level of the proposed development above Malin Head Ordnance Datum?**

 m

21 **Is on-site water storage being provided?** Yes  No

Please include calculations on the attached sheet provided.







Please note that if you are sending us your application form and any associated documentation by email, the maximum file size that we can receive in any one email is 35MB.

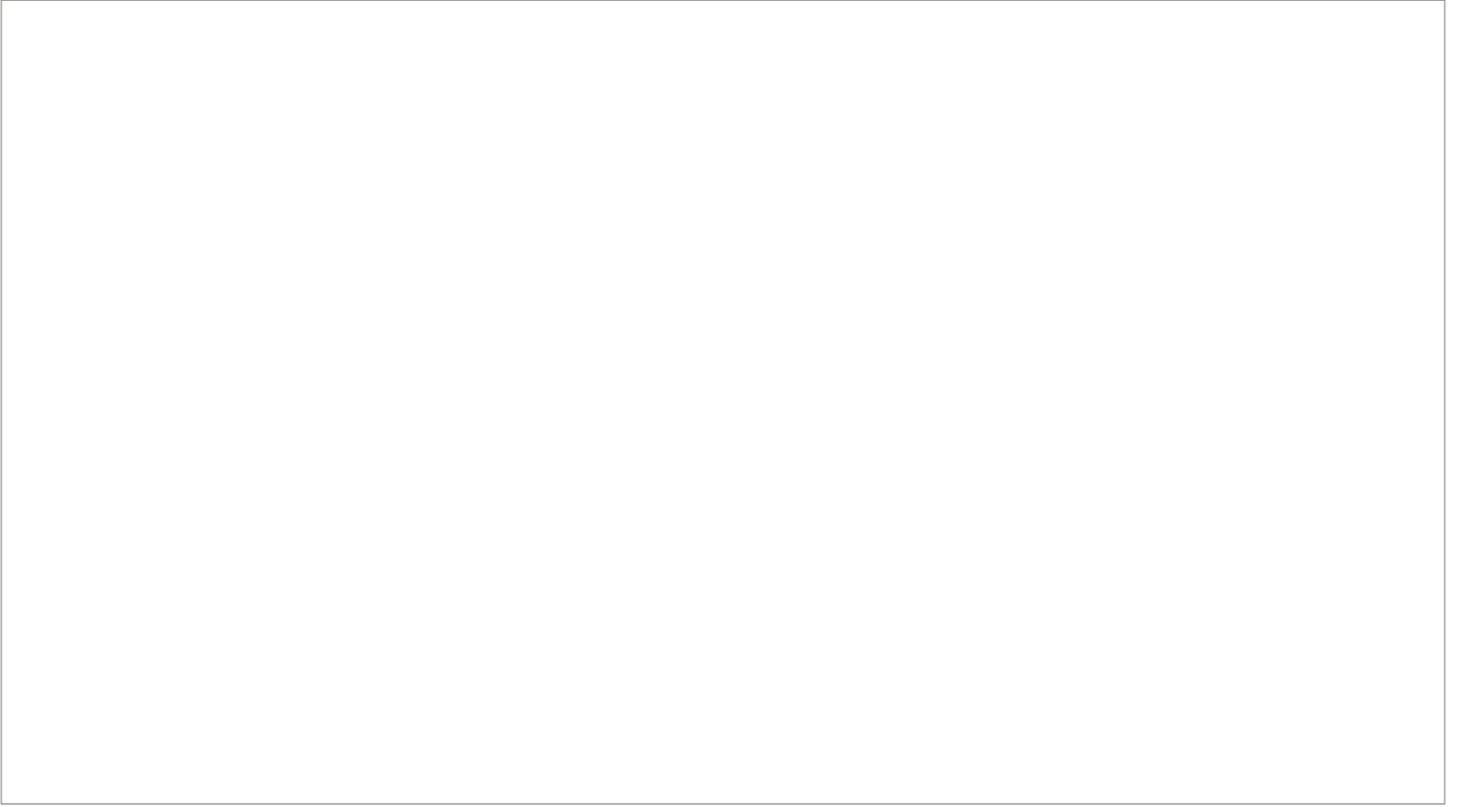
**Please note, if mandatory fields are not completed the application will be returned.**

Uisce Éireann is subject to the provisions of the Freedom of Information Act 2014 (“FOIA”) and the codes of practice issued under FOIA as may be amended, updated or replaced from time to time. The FOIA enables members of the public to obtain access to records held by public bodies subject to certain exemptions such as where the requested records may not be released, for example to protect another individual’s privacy rights or to protect commercially sensitive information. Please clearly label any document or part thereof which contains commercially sensitive information. Uisce Éireann accepts no responsibility for any loss or damage arising as a result of its processing of freedom of information requests.

## Calculations

Water demand

## On-site storage



## Fire flow requirements







## Guide to completing the pre-connection enquiry form

This form should be completed by applicants enquiring about the feasibility of a water and/or wastewater connection to Uisce Éireann infrastructure.

The Uisce Éireann Codes of Practice are available at [www.water.ie](http://www.water.ie) for reference.

### Section A | Applicant Details

- Question 1:** This question requires the applicant or company enquiring about the feasibility of a connection to identify themselves, their postal address, and to provide their contact details.
- Question 2:** If the applicant has employed a consulting engineer or an agent to manage the enquiry on their behalf, the agent's address and contact details should be recorded here.
- Question 3:** Please indicate whether it is the applicant or the agent who should receive future correspondence in relation to the enquiry.

### Section B | Site details

- Question 4:** This is the address of the site requiring the water/wastewater service connection and for which this enquiry is being made.
- Question 5:** Please provide the Irish Grid co-ordinates of the proposed site. Irish grid positions on maps are expressed in two dimensions as Eastings (E or X) and Northings (N or Y) relative to an origin. You will find these coordinates on your Ordnance Survey map which is required to be submitted with an application.
- Question 6:** Please identify the Local Authority that is or will be dealing with your planning application, for example Cork City Council.
- Question 7:** Please indicate if planning permission has been granted for this application, and if so, please provide the planning permission reference number.
- Question 8:** Please indicate if this development is affiliated with a government body/agency, and if so, specify

### Section C | Development details

- Question 9:** Please specify the number of different property/premises types by filling in the tables provided.
- Question 9.1:** Please provide additional details if your proposed business use are in the Food Processing, Industrial unit/ Manufacturing, Sports Facility or Other Categories.
- Question 9.2:** Please indicate the maximum expected occupancy in numbers of people according to the proposed development you selected.
- Question 10:** Please indicate the approximate commencement date of works on the development.
- Question 11:** Please indicate if a phased building approach is to be adopted when developing the site. If so, please provide details of the phase master-plan and the proposed variation in water demand/wastewater discharge as a result of the phasing of the development.
- Question 12:** Please indicate the type of connection required by ticking the appropriate box and proceed to complete the appropriate section or sections.

### Section D | Water connection and demand details

- Question 13:** Please indicate if a water connection already exists for this site.
- Question 13.1:** Please indicate if this enquiry concerns an additional connection to one already installed on the site.
- Question 13.2:** Please indicate if you are proposing to upgrade the water connection to facilitate an increase in water demand. Uisce Éireann will determine what impact this will have on our infrastructure.
- Question 14:** Please indicate the approximate date that the proposed connection to the water infrastructure will be required.
- Question 15:** Please indicate what diameter of water connection is required to service this development.

- Question 16:** Please indicate if more than one connection is required to service this development. Please note that the connection size provided may be used to determine the connection charge.
- Question 17:** If this connection enquiry concerns a business premises, please provide calculations for the water demand and include your calculations on the calculation sheet provided. Business premises include shops, offices, hotels, schools, etc. Demand rates (peak and average) are site specific. Average demand is the total daily volume divided by a 24-hour time period and expressed in litres per second (l/s). For design purposes, please refer to the Uisce Éireann Codes of Practice for Water Infrastructure.
- Question 18:** If this connection enquiry is for an industrial premises, please calculate the water demand and include your calculations on the calculation sheet provided. Demand rates (peak and average) are site specific. Average demand is the total daily volume divided by a 24-hour time period and expressed in litres per second (l/s). The peak demand for sizing of the pipe network will be as per the specific business production requirements. For design purposes, please refer to the Uisce Éireann Codes of Practice for Water Infrastructure.
- Question 19:** Please specify the ground level at the location where connection to the public water mains will be made. This is required in order to determine if there is sufficient pressure in the existing water infrastructure to serve your proposed development. Levels should be quoted in metres relative to Malin Head Ordnance Datum.
- Question 20:** Please specify the highest finished floor level on site. This is required in order to determine if there is sufficient pressure in the existing water infrastructure to serve your proposed development. Levels should be quoted in metres relative to Malin Head Ordnance Datum.
- Question 21:** If storage is required, water storage capacity of 24-hour water demand must usually be provided at the proposed site. In some cases, 24-hour storage capacity may not be required, for example 24-hour storage for a domestic house would be provided in an attic storage tank. Please calculate the 24-hour water storage requirements and include your calculations on the attached sheet provided. Please also confirm that on-site storage is being provided by ticking the appropriate box.
- Question 22:** The water supply system shall be designed and constructed to reliably convey the water flows that are required of the development including fire flow requirements by the Fire Authority. The Fire Authority will provide the requirement for fire flow rates that the water supply system will have to carry. Please note that while flows in excess of your required demand may be achieved in the Uisce Éireann network and could be utilised in the event of a fire, Uisce Éireann cannot guarantee a flow rate to meet your fire flow requirement. To guarantee a flow to meet the Fire Authority requirements, you should provide adequate fire storage capacity within your development. Please include your calculations on the attached sheet provided, and further provide confirmation of the Fire Authority requirements.
- Question 23:** Please identify proposed additional water supply sources, that is, do you intend to connect to the public water mains or the public mains and supplement from other sources? If supplementing public water supply with a supply from another source, please provide details as to how the potable water supply is to be protected from cross contamination at the premises.

## Section E | Wastewater connection and discharge details

- Question 24:** Please indicate if a wastewater connection to a public sewer already exists for this site.
- Question 24.1:** Please indicate if this enquiry relates to an additional wastewater connection to one already installed.
- Question 24.2:** Please indicate if you are proposing to upgrade the wastewater connection to facilitate an increased discharge. Uisce Éireann will determine what impact this will have on our infrastructure.
- Question 25:** Please specify the approximate date that the proposed connection to the wastewater infrastructure will be required.
- Question 26:** Please indicate what diameter of wastewater connection is required to service this development.
- Question 27:** Please indicate if more than one connection is required to service this development. Please indicate number required.
- Question 28:** If this enquiry relates to a business premises, please provide calculations for the wastewater discharge and include your calculations on the attached sheet provided. Business premises include shops, offices, hotels, schools, etc. Discharge rates (peak and average) are site specific. Average discharge is the total daily volume divided by a 24-hour time period and expressed in litres per second (l/s). For design purposes, please refer to the Uisce Éireann Codes of Practice for Wastewater Infrastructure.

- Question 29:** If this enquiry relates to an industrial premises, please provide calculations for the wastewater discharge and include your calculations on the calculation sheet provided. Discharge rates (peak and average) are site specific. Average discharge is the total daily volume divided by a 24-hour time period and expressed in litres per second (l/s). The peak discharge for sizing of the pipe network will be as per the specific business production requirements. For design purposes, please refer to the Uisce Éireann Codes of Practice for Wastewater Infrastructure.
- Question 30:** Please specify the maximum and average concentrations and the maximum daily load of each of the wastewater characteristics listed in the wastewater organic load table (if not domestic effluent), and also specify if any other significant concentrations are expected in the effluent. Please complete the table and provide additional supporting documentation if relevant. Note that the concentration shall be in mg/l and the load shall be in kg/day. Note that for business premises (shops, offices, schools, hotels, etc.) for which only domestic effluent will be discharged (excluding discharge from canteens/restaurants which would require a Trade Effluent Discharge licence), there is no need to complete this question.
- Question 31:** In exceptional circumstances, such as brownfield sites, where the only practical outlet for storm/surface water is to a combined sewer, Uisce Éireann will consider permitting a restricted attenuated flow to the combined sewer. Storm/surface water will only be accepted from brownfield sites that already have a storm/surface water connection to a combined sewer and the applicant must demonstrate how the storm/surface water flow from the proposed site is minimised using sustainable urban drainage system (SUDS). This type of connection will only be considered on a case by case basis. Please advise if the proposed development intends discharging surface water to the combined wastewater collection system.
- Question 32:** Please specify if the development needs to pump its wastewater discharge to gain access to Uisce Éireann infrastructure.
- Question 33:** Please specify the ground level at the location where connection to the public sewer will be made. This is required to determine if the development can be connected to the public sewer via gravity discharge. Levels should be quoted in metres relative to Malin Head Ordnance Datum.
- Question 34:** Please specify the lowest floor level of the proposed development. This is required in order to determine if the development can be connected to the public sewer via gravity discharge. Levels should be quoted in metres relative to Malin Head Ordnance Datum.
- Question 35:** Please specify the proposed invert level of the pipe exiting the property to the public road.

## Section F | Supporting documentation

Please provide additional information as listed.

## Section G | Declaration

Please review the declaration, sign, and return the completed application form to Uisce Éireann by email or by post using the contact details provided in Section G.





## CONFIRMATION OF FEASIBILITY

Nik Dewhirst

2 May 2025

**Our Ref: CDS25000940 Pre-Connection Enquiry  
Pollnagroagh, Athenry, Co.Galway**

**Uisce Éireann**  
Bosca OP 448  
Oifig Sheachadta na  
Cathrach Theas  
Cathair Chorcaí

**Uisce Éireann**  
PO Box 448  
South City  
Delivery Office  
Cork City

[www.water.ie](http://www.water.ie)

Dear Applicant/Agent,

### **We have completed the review of the Pre-Connection Enquiry.**

Uisce Éireann has reviewed the pre-connection enquiry in relation to a Water connection for a Business Connection of 1 unit(s) at Pollnagroagh, Athenry, Co.Galway, (the **Development**).

Based upon the details provided we can advise the following regarding connecting to the networks;

- **Water Connection**

- Feasible without infrastructure upgrade by Uisce Éireann
- No direct Connection is permitted to the existing 300mm Trunk Main.  
The connection is feasible, however, a water network extension will be required to be installed by Uisce Éireann and funded by the Customer in order to facilitate the proposed development. Approximately 2km of existing water mains will be required to be upsized to 150mm to satisfy the proposed demands. The main will also need to be extended on the public road to the proposed connection point (approximately 150m) Tank Filling will be limited to occur only during nighttime off peak flow times. The customer is responsible for ensuring the tanks are to be filled strictly between the

**Stiúrtóirí / Directors:** Niall Gleeson (POF / CEO), Jerry Grant (Cathaoirleach / Chairperson), Gerard Britchfield, Liz Joyce, Michael Nolan, Patricia King, Eileen Maher, Cathy Mannion, Paul Reid, Michael Walsh.

**Oifig Chláraithe / Registered Office:** Teach Colvill, 24-26 Sráid Thalbóid, Baile Átha Cliath 1, D01 NP86 / Colvill House, 24-26 Talbot Street, Dublin, Ireland D01NP86

Is cuideachta ghníomhaíochta ainmnithe atá faoi theorainn scaireanna é Uisce Éireann / Uisce Éireann is a designated activity company, limited by shares.

Cláraithe in Éirinn Uimh.: 530363 / Registered in Ireland No.: 530363.

hours of 12am and 6am by way of automated controls.

This letter does not constitute an offer, in whole or in part, to provide a connection to any Uisce Éireann infrastructure. Before the Development can be connected to our network(s) you must submit a connection application and be granted and sign a connection agreement with Uisce Éireann.

As the network capacity changes constantly, this review is only valid at the time of its completion. As soon as planning permission has been granted for the Development, a completed connection application should be submitted. The connection application is available at [www.water.ie/connections/get-connected/](http://www.water.ie/connections/get-connected/)

### Where can you find more information?

- **Section A** - What is important to know?
- **Section B** - Details of Uisce Éireann's Network(s)

**This letter is issued to provide information about the current feasibility of the proposed connection(s) to Uisce Éireann's network(s). This is not a connection offer and capacity in Uisce Éireann's network(s) may only be secured by entering into a connection agreement with Uisce Éireann.**

For any further information, visit [www.water.ie/connections](http://www.water.ie/connections), email [newconnections@water.ie](mailto:newconnections@water.ie) or contact 1800 278 278.

Yours sincerely,



**Dermot Phelan**  
**Connections Delivery Manager**

## Section A - What is important to know?

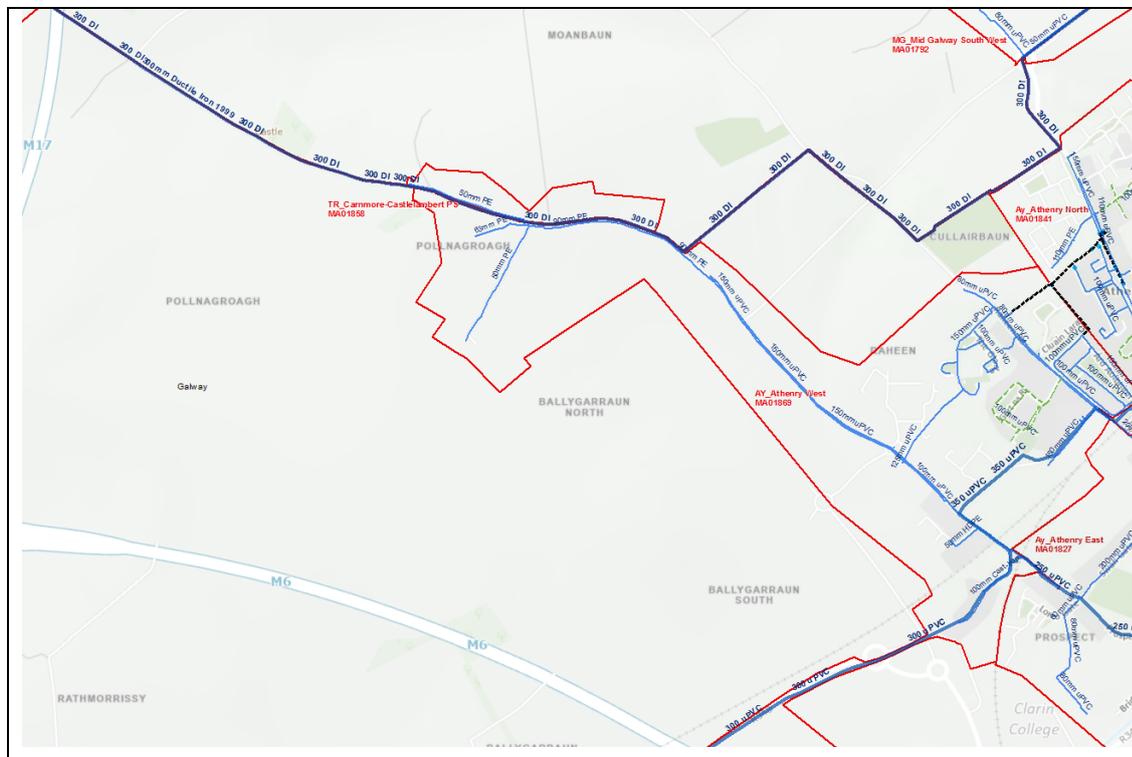
| What is important to know?   | Why is this important?  |
|--|---|
| <p><b>Do you need a contract to connect?</b></p>                     | <ul style="list-style-type: none"> <li>• Yes, a contract is required to connect. This letter does not constitute a contract or an offer in whole or in part to provide a connection to Uisce Éireann's network(s).</li> <li>• Before the Development can connect to Uisce Éireann's network(s), you must submit a connection application <u>and be granted and sign</u> a connection agreement with Uisce Éireann.</li> </ul> |
| <p><b>When should I submit a Connection Application?</b></p>         | <ul style="list-style-type: none"> <li>• A connection application should only be submitted after planning permission has been granted.</li> </ul>   |
| <p><b>Where can I find information on connection charges?</b></p>    | <ul style="list-style-type: none"> <li>• Uisce Éireann connection charges can be found at: <a href="https://www.water.ie/connections/information/charges/">https://www.water.ie/connections/information/charges/</a></li> </ul>   |
| <p><b>Who will carry out the connection work?</b></p>                | <ul style="list-style-type: none"> <li>• All works to Uisce Éireann's network(s), including works in the public space, must be carried out by Uisce Éireann*.</li> </ul> <p>*Where a Developer has been granted specific permission and has been issued a connection offer for Self-Lay in the Public Road/Area, they may complete the relevant connection works</p>  |
| <p><b>Fire flow Requirements</b></p>                                 | <ul style="list-style-type: none"> <li>• The Confirmation of Feasibility does not extend to fire flow requirements for the Development. Fire flow requirements are a matter for the Developer to determine.</li> <li>• <b>What to do?</b> - Contact the relevant Local Fire Authority</li> </ul>  |
| <p><b>Plan for disposal of storm water</b></p>                       | <ul style="list-style-type: none"> <li>• The Confirmation of Feasibility does not extend to the management or disposal of storm water or ground waters.</li> <li>• <b>What to do?</b> - Contact the relevant Local Authority to discuss the management or disposal of proposed storm water or ground water discharges.</li> </ul>   |
| <p><b>Where do I find details of Uisce Éireann's network(s)?</b></p> | <ul style="list-style-type: none"> <li>• Requests for maps showing Uisce Éireann's network(s) can be submitted to: <a href="mailto:datarequests@water.ie">datarequests@water.ie</a></li> </ul>  |

|   |   |
|---|---|
| <p><b>What are the design requirements for the connection(s)?</b></p> | <ul style="list-style-type: none"> <li>• The design and construction of the Water pipes and related infrastructure to be installed in this Development shall comply with <i>the Uisce Éireann Connections and Developer Services Standard Details and Codes of Practice</i>, available at <a href="http://www.water.ie/connections">www.water.ie/connections</a></li> </ul>   |
| <p><b>Trade Effluent Licensing</b></p>                                | <ul style="list-style-type: none"> <li>• Any person discharging trade effluent** to a sewer, must have a Trade Effluent Licence issued pursuant to section 16 of the Local Government (Water Pollution) Act, 1977 (as amended).</li> <li>• More information and an application form for a Trade Effluent License can be found at the following link:<br/><a href="https://www.water.ie/business/trade-effluent/about/">https://www.water.ie/business/trade-effluent/about/</a></li> </ul> <p>**trade effluent is defined in the Local Government (Water Pollution) Act, 1977 (as amended)</p> |

## Section B – Details of Uisce Éireann’s Network(s)

The map included below outlines the current Uisce Éireann infrastructure adjacent the Development: To access Uisce Éireann Maps email

[datarequests@water.ie](mailto:datarequests@water.ie)



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**Note:** The information provided on the included maps as to the position of Uisce Éireann’s underground network(s) is provided as a general guide only. The information is based on the best available information provided by each Local Authority in Ireland to Uisce Éireann.

Whilst every care has been taken in respect of the information on Uisce Éireann’s network(s), Uisce Éireann assumes no responsibility for and gives no guarantees, undertakings or warranties concerning the accuracy, completeness or up to date nature of the information provided, nor does it accept any liability whatsoever arising from or out of any errors or omissions. This information should not be solely relied upon in the event of excavations or any other works being carried out in the vicinity of Uisce Éireann’s underground network(s). The onus is on the parties carrying out excavations or any other works to ensure the exact location of Uisce Éireann’s underground network(s) is identified prior to excavations or any other works being carried out. Service connection pipes are not generally shown but their presence should be anticipated.

# Appendix F. BRE365 test results



P25025

Galway Peaker

27/02/2025

Test 1

SA01

E546726.444 N728214.041

52.169mOD

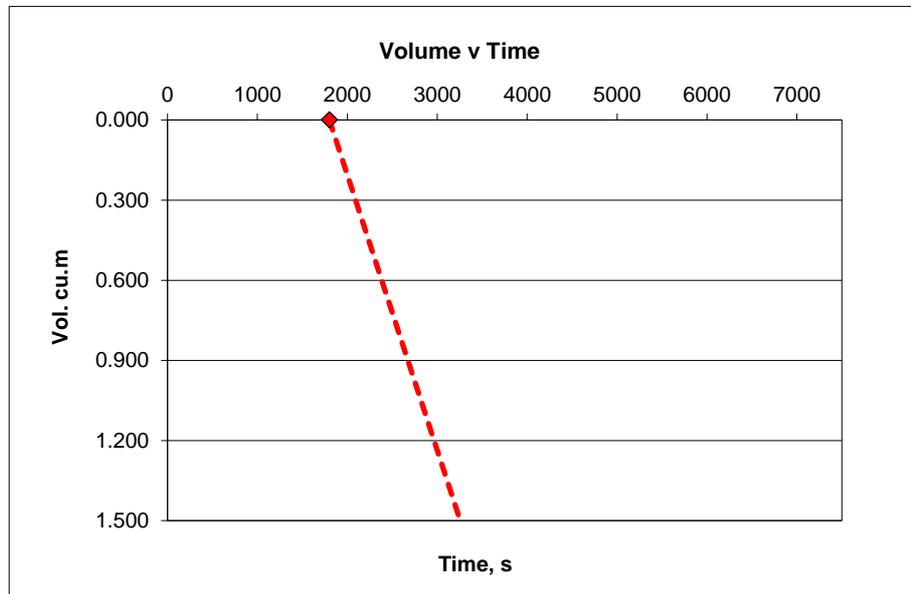
l, m 2.300 b, m 1.200 d, m 1.600  
 l\_base, m 2.300 d\_eff, m 0.560  
 l\_eff, m 2.300

empty

| Time, min | Measure, m bgl | Time, sec | Depth water, m | Fall, m | Volume |
|-----------|----------------|-----------|----------------|---------|--------|
| 30        | 1.040          | 1800      | 0.56           | 0.00    | 0.000  |
| 55        | 1.600          | 3300      | 0.00           | 0.56    | 1.546  |

Area 2.760 m<sup>2</sup>  $V_{p75-25 \text{ theory}}$  volume 0.7728 m<sup>3</sup>  
 50% Area\_eff, a<sub>p50</sub> 4.720 m<sup>2</sup>  $V_{p75-25 \text{ actual}}$  volume 0.7728 m<sup>3</sup>  
 50% Area\_act, a<sub>p50</sub> 4.720 m<sup>2</sup>  $t_{p75-25 \text{ actual}}$  time 750 s

Infiltration Coefficient *f* 2.18E-04 ms<sup>-1</sup>



**NOTES:**

Water drains as the pit is being filled.  
 Water does not rise above 1.04m bgl.

P25025

Galway Peaker

27/02/2025

Test 1

SA02 (PT01)

E546540.557 N728314.574

55.797mOD

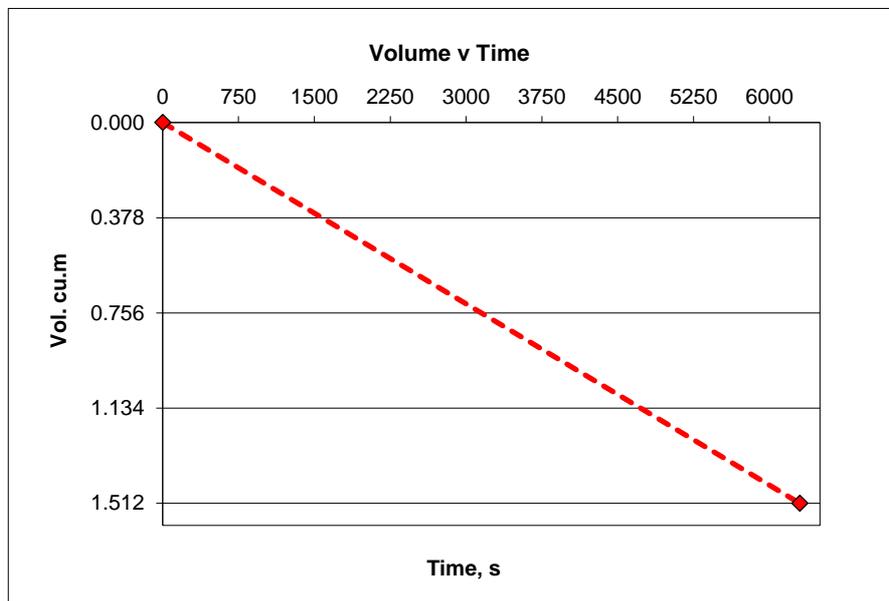
l, m 2.100 b, m 1.200 d, m 1.000  
 l\_base, m 2.100 d\_eff, m 0.600  
 l\_eff, m 2.100

empty

| Time, min | Measure, m<br>bgl | Time, sec | Depth water,<br>m | Fall, m | Volume |
|-----------|-------------------|-----------|-------------------|---------|--------|
| 0         | 0.400             | 0         | 0.60              | 0.00    | 0.000  |
| 105       | 1.000             | 6300      | 0.00              | 0.60    | 1.512  |

Area 2.520 m<sup>2</sup>  $V_{p75-25}$  theory volume 0.7560 m<sup>3</sup>  
 50% Area\_eff, a<sub>p50</sub> 4.500 m<sup>2</sup>  $V_{p75-25}$  actual volume 0.7560 m<sup>3</sup>  
 50% Area\_act, a<sub>p50</sub> 4.500 m<sup>2</sup>  $t_{p75-25}$  actual time 3150 s

Infiltration Coefficient  $f$  5.33E-05 ms<sup>-1</sup>



**NOTES:**

This was the proposed location for percolation test. Percolation test not carried out due to Soakaway test done instead.

P25025

Galway Peaker

27/02/2025

Test 2

SA02 (PT01)

E546540.557 N728314.574

55.797mOD

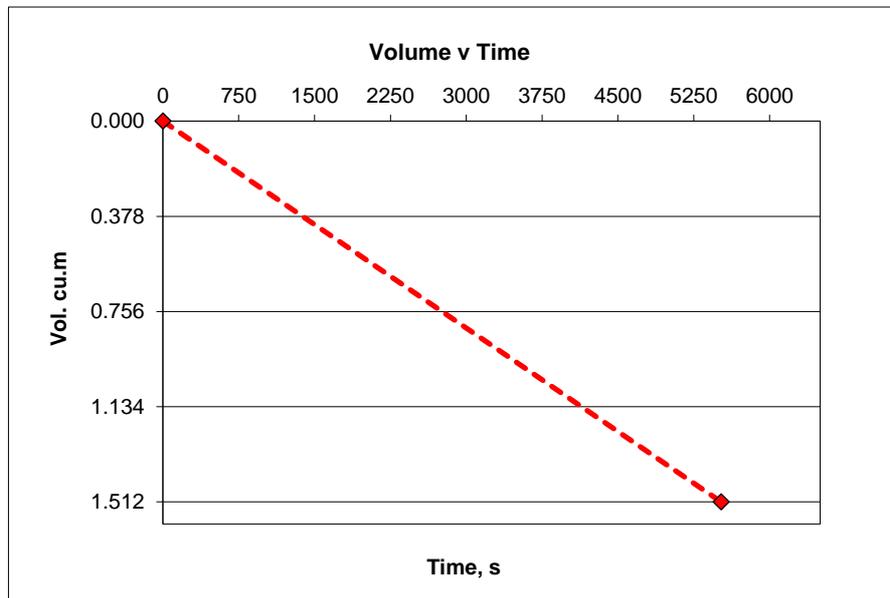
l, m 2.100 b, m 1.200 d, m 1.000  
 l\_base, m 2.100 d\_eff, m 0.600  
 l\_eff, m 2.100

empty

| Time, min | Measure, m bgl | Time, sec | Depth water, m | Fall, m | Volume |
|-----------|----------------|-----------|----------------|---------|--------|
| 0         | 0.400          | 0         | 0.60           | 0.00    | 0.000  |
| 92        | 1.000          | 5520      | 0.00           | 0.60    | 1.512  |

Area 2.520 m<sup>2</sup> V<sub>p75-25 theory</sub> volume 0.7560 m<sup>3</sup>  
 50% Area\_eff, a<sub>p50</sub> 4.500 m<sup>2</sup> V<sub>p 75 - 25 actual</sub> volume 0.7560 m<sup>3</sup>  
 50% Area\_act, a<sub>p50</sub> 4.500 m<sup>2</sup> t<sub>p 75- 25 actual</sub> time 2760 s

Infiltration Coefficient *f* 6.09E-05 ms<sup>-1</sup>



**NOTES:**

This was the proposed location for percolation test. Percolation test not carried out due to Soakaway test done instead.

P25025

Galway Peaker

27/02/2025

Test 3

SA02 (PT01)

E546540.557 N728314.574

55.797mOD

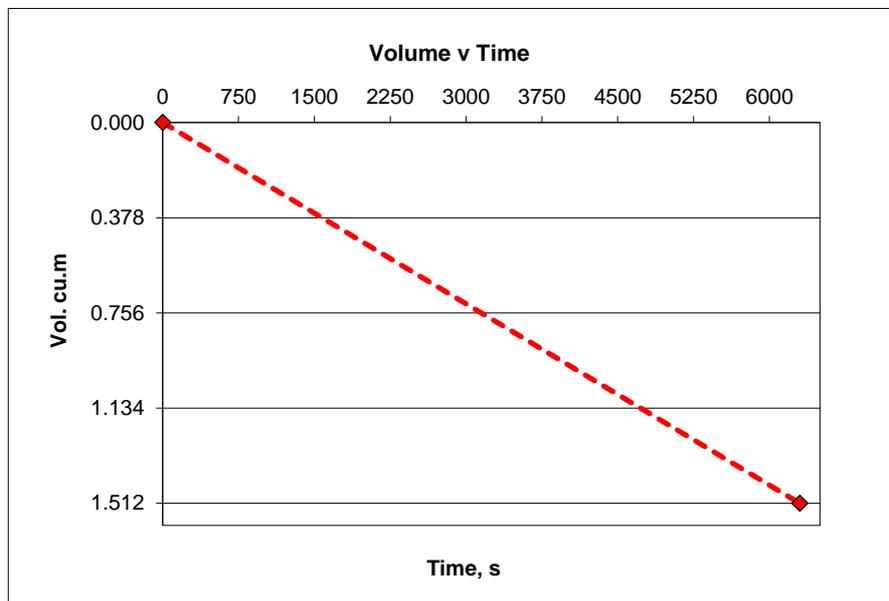
l, m 2.100 b, m 1.200 d, m 1.000  
 l\_base, m 2.100 d\_eff, m 0.600  
 l\_eff, m 2.100

empty

| Time, min | Measure, m bgl | Time, sec | Depth water, m | Fall, m | Volume |
|-----------|----------------|-----------|----------------|---------|--------|
| 0         | 0.400          | 0         | 0.60           | 0.00    | 0.000  |
| 105       | 1.000          | 6300      | 0.00           | 0.60    | 1.512  |

Area 2.520 m<sup>2</sup>  $V_{p75-25}$  theory volume 0.7560 m<sup>3</sup>  
 50% Area\_eff, a<sub>p50</sub> 4.500 m<sup>2</sup>  $V_{p75-25}$  actual volume 0.7560 m<sup>3</sup>  
 50% Area\_act, a<sub>p50</sub> 4.500 m<sup>2</sup>  $t_{p75-25}$  actual time 3150 s

Infiltration Coefficient  $f$  5.33E-05 ms<sup>-1</sup>



**NOTES:**

This was the proposed location for percolation test. Percolation test not carried out due to Soakaway test done instead.

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